# SYSTEMS DESIGN

#### **NOVEMBER-DECEMBER 1960**

#### featuring:

-

ITAR

S

EMS DES

G Controlled

pplicaur Re-

Chi-Illinois rd St.

Pacific te Mc-

Sunset

nerican

lebach onduc

Chmm. ty, Mo

Englind Ran-Lafaydanoff

ciences

n Magpred by Illurgical er, New Ir., IBM , N. Y.

For ins AssoSalmon
6, N. Y.

Joint
by IRE
r Hatel
Lanigan
0 Third

New Gyroscopes

Transducers

Processing and Updating of Magnetic Tape Files

Electronic Circuitry

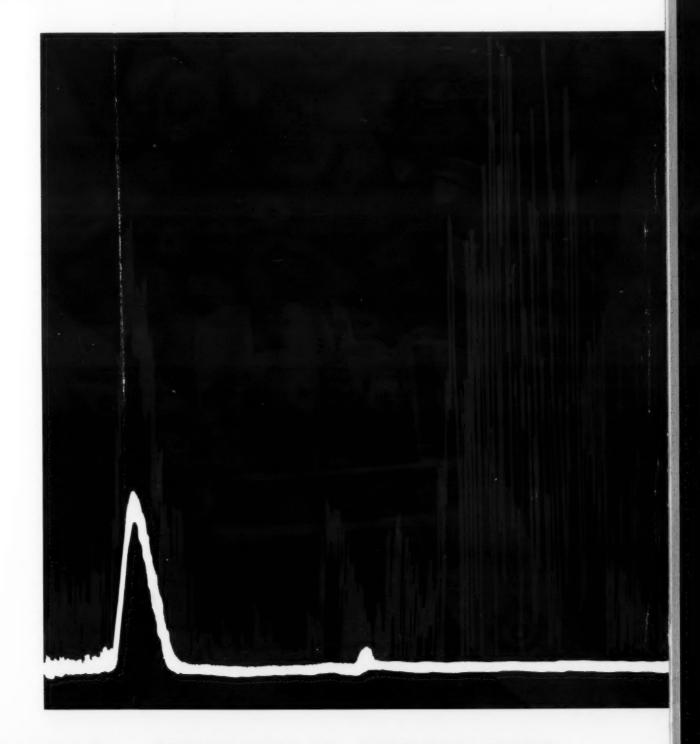
TRANSISTORIZED SCOPE DEFLECTION AMPLIFIER
TRANSISTORIZED SCOPE POWER SUPPLY
DIRECT-COUPLED AMPLIFIER FOR HIGH VOLTAGES
TWO-METER POWER SUPPLY
TRANSISTOR CIRCUITS—CURRENT FLOW AND
VOLTAGE PHASE RELATIONS

#### cover article:

First Ceramic Gyro For Space Achieves Ultra-Accuracy

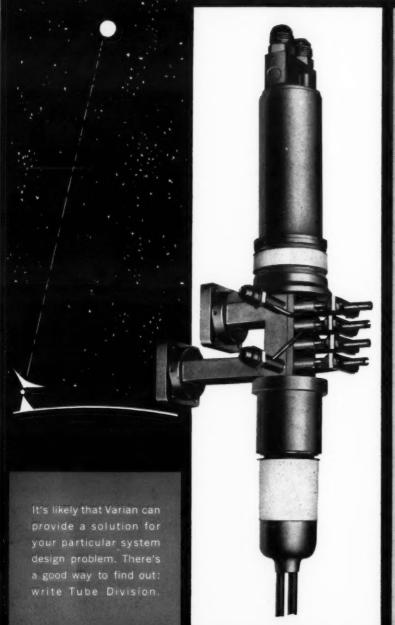
ANNUAL INDEX VOL. IV 1960

ROUTE THIS COPY TO



INSTRUMENTS PUBLISHING COMPANY . PITTSBURGH 12, PENNSYLVANIA

## space systems 20kW CW at X-band



Varian's new VA-849 amplifier klystrons are rated to deliver higher CW power at X-band than any existing tube in the world ... 20kW!

Varian's new VA-849 power klystron opens up a variety of new design approaches to space systems. Possible applications exist in communication concepts such as repeater satellites, moonbounce signalling, or in reflections from clouds of tiny orbiting needles. Radio astronomers, too, will welcome the VA-849.

Immediate applications include CW radar and illuminator service. Low incidental noise. Water cooling. Electromagnet focusing. Another significant advance In microwave components from Varian's broad experience and research in super-power tubes.

#### **FEATURES**

- 7.125 to 8.5 kMc
- 20 kW CW
- 50 db Gain.
- 30 Mc Minimum Bandwidth
- Tunable 60 Mc.



#### VARIAN associates

PALO ALTO 9, CALIFORNIA

BOMAC LABORATORIES, INC. VARIAN ASSOCIATES OF CANADA, LTD. S-F-D LABORATORIES, INC. SEMICON ASSOCIATES, INC. SEMICON OF CALIFORNIA, INC. VARIAN A.G. (SWITZERLAND)

CIRCLE 1 ON READER-SERVICE CARD



Published bimonthly by Instruments Publishing Company Inc., 845 Ridge Ave., Pittsburgh 12, Pa. Printed at 1600 N. Main St., Pontiac, III. Accepted as Controlled Circulation Publication at Pontiac, Illinois.

#### BPA

#### Richard Rimbach, Publisher

Claude O. Morrison, Editor (Commander U.S. Naval Reserve)

Milton H. Aronson Editorial Director Fred D. Marton ... Associate Editor ....Art Director Raymond C. E. Smith Main Office: 845 Ridge Ave, Pgh 12, Pa., Fairfax 1-0161

#### **Advertising Representatives**

Richard Rimbach, Jr., Vice-President, Sales, New York, Murray Hill 8-0980 Boston 16—Harold H. Short, Jr., 269 Maine St., Stoneham, Mass., Stoneham 6-3982

Chicago 6—Harold W. Haskett, Madison Terminal Bldg., 9 S. Clinton St. Central

Clearwater, Florida-Evert F. Nordstrom, 1651 Sherwood St., Clearwater 319033

Cleveland (Shaker Heights) 22—Max G. Bauer, 3310 Warrenville Center Rd. Wyoming 1-7145

Los Angeles 34-John J. Fahey, 2639 S. La Cienega Blvd., Upton 0-8442

New York 17-Richard Rimbach, Jr., Room 359, 525 Lexington Ave. Murray Hill

Pittsburgh 12, Penna—C. F. Goldcamp, 845 Ridge Ave., Fairfax 10161

Philadelphia 4-Robert V. Frey, Suite 100, 101 N. 33rd St., Evergreen 2-3878

San Francisco II-Charles Clark, 420 Market St., Douglas 2-3899

St. Louis I-Steve Wright, Room 416, 4 N. 8th St., Chestnut 1-1965

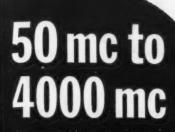
#### Subscriptions

Circulated without charge to qualified engineers and executives in organizations which develop, manufacture, purchase, install, or maintain electronic and control equipment and systems for military applications; of-ficers and engineers in the Armed Forces responsible for design specification, test, or maintenance of such equipment; scientists and engineers in development and research for the Armed Forces. Qualified individuals in the United States may request this pub-lication by providing the following informa-tion on their company letterhead: Your name and title; your job function as related to your company's products or services for the military; your company's name, address, and nature of business as related to military end products or applications. Available to others, by subscriptions, at the rate of \$10 per year.

Copyright 1960

by Instruments Publishing Company, Inc.

CIR Voven



WITH TWO TUNING HEADS



PANORAMIC SPECTRUM ANALYZER

d.

S

111

45

00.

ar-

4

or ists rch ubna-our ted

for

ary

#### WITH TWO TUNING HEADS

- Check these outstanding features:

   Low noise input, less than 0.5 micro volts across 50 ohms, for high usable sensitivity
- 10 mc maximum sweepwidth, continuously reducible to 0 mc
- Continuously variable differential markers, ±50 kc to ±5 mc

- ers, ±50 kc to ±5 mc
  Continuously variable resolution (I.F. bandwidth 9 kc to 80 kc)

  1 cps to 60 cps sweep rate, continuously variable with single control
  DC coupled video amplifier for analysis of CW signals

  Three selectable amplitude scales 40 kb log 20 kb linear and source law
- db log, 20 db linear and square law Low frequency swept oscillator pro-vides high inherent stability Excellent construction and design make the equipment unparalleled for mini-
- mum down time Optional scale lighting, flat faced CRT and camera bezel for standard scope
- Tuning Heads: RF-2 50 mc-250 mc, RF-3 220 mc-4000 mc in five ranges Inquiries invited on Panoramic Spectrum Analyzers for special problems. Write to-day for descriptive literature.

  Makers of Panadaptor • Panalyzer • Panoramic Sonic Analyzer • Panoramic Ultrasonic Analyzer



518 So. Fulton Ave. • Mount Vernon, N.Y.
Ph: OWens 9-4600 • TWX: MT-V-NY-5221
Cables: Panoramic, Mt. Vernon, N.Y. State CIRCLE 2 ON READER-SERVICE CARD

November-December, 1960



**VOLUME 4. NUMBER 6** NOV.-DEC. 1960

EDITORIAL	
Merry Christmas! And An Exciting New Year	2
In This Issue	3
ARTICLES EMPHASIZING INERTIAL GUIDANCE COMPONENTS	
Electrostatic Gyro is Space Reference	3
First Ceramic Gyro for Space Guidance Achieves Ultra-Accuracy	
Gyro Applications in Ballastic Missiles and Space Vehicles	
The Magnetohydrodynamic Gyroscope	
Gimbal Angle Transducers Require Increased Accuracy & Speed	15
PAUL KAESTNER	20
Gyro Characteristics Vary to Meet Job Requirements	41
Unique Vertical Gyro for Target Drones	50
ARTICLES EMPHASIZING OTHER TRANSDUCERS	
The Thermistor—a Versatile Thermal Transducer	28
Tip-Sensitive Heat Switch	29
New Linear Pots are Standardized	
Bondable Semiconductor Strain Gage	44
Multirange Digital Voltmeter Reads Missile Transducers	
Electrodynamic Shakers Calibrate Transducers	52
Far Infrared Filters Have Sharp Cut-On	54
Underwater Transducers	56
OTHER ARTICLES IN THE FIELD OF SYSTEMS COMPONENTS	
Manned Space Vehicles Monitoring Systems	4
Electronic Specialties Feature Teflon Characteristics	11
Energy Absorber Cushions Pilot in Barrier Crashes	14
Processing and Updating Magnetic Tape Files	
Modern Permanent Magnets	30
Digital Variable Increment Computer Solves Weapons Systems Problems	36
Fault Monitor Scans Thirty Remote Stations	4!
A Pocket Laboratory Scope	4
Toroid Applications Chart	5
ELECTRONIC CIRCUITRY	
Transistorized-Scope Deflection Amplifier	1
Transistorized-Scope Power Supply	
Direct Coupled Amplifier for High Voltages	1
Two-Meter Power Supply	1
Transistor Circuits—Current Flow and Voltage Phase Relations	1
Annual Index, All 1960 MSD Issues	5

COVER: Significant reduction of bearing noise achieved in new ceramic gas-bearing gyro is shown by oscillo-scope comparison with bearing noise of standard MIG gyro. Noise is evi-dence of ball friction, a major cause of gyro drift. Miniature size of gyro rotor is also dramatically shown. (See page 4).

#### REGULAR FEATURES

New Products		32
New Literature		52
Advertisers' IndexInside	Back	Cover
Events	Back	Cover
Book Reviews		23-49

Noise spectrum analysis using internal video smoothing filter. Noise envelope average vs. fre-quency seen in readily inter-preted plot. In-ternal marker pips are 500kc apart.



### more applications maximum economy



PANORAMIC'S **SPA-3/25** SPECTRUM ANALYZER 1kc-25mc

One compact, low-cost unit for all these uses . . . and MORE:

Video Band Analysis
Broadband Noise Studies
Communications Channel Analysis
Telemetry Subcarrier Channel Analysis
Frequency Response Plotting of filters,
video networks etc., to 15mc (with companion sweep generator Model G-6)

Combining the most desirable features of a whole series of equipments, Panoramic's "workhorse" Model SPA-3/25 (usable to 200 cps) features:

• 0-3mc sweep width continuously call-brated • Variable center frequency con-trol calibrated from 0 to 23.5 mc • Ad-justable resolution; selectivity, 200cps to 30kc • Variable sweep rate Icps to 60 cps • Lin, 40db log and square law amplitude scales • High sensitivity: 20µv full scale • Calibrated 100 db input at-tenuators

Also available: Model SPA-3, 1kc-15mc. Same as SPA-3/25, except variable center frequency control is calibrated 0 to 13.5mc.

Write, wire, phone NOW for detailed specification bulletin . . . NEW Catalog Digest . . . and regular mailing of "THE PANORAMIC ANALYZER," featuring application data.



518 So. Fulton Ave. • Mount Vernon, N.Y.
Ph: OWens 9-4600 • TWX: MT-V-NY-5229
Cables: Panoramic, Mt. Vernon, N.Y. State CIRCLE 3 ON READER-SERVICE CARD



## A COMPLETELY NEW SERIES OF STATIC FREQUENCY CHANGERS

New, because of its exclusive use of solid state components in sophisticated circuitry designed and produced with Tomorrow in mind. These units provide exceptionally stable 400-CPS, single- or 3-phase, A-C outputs from 60-CPS, single- or 3-phase, A-C inputs. This equipment is designed for use in applications where critical voltages and frequencies are required...laboratories, ground support systems and production testing facilities.

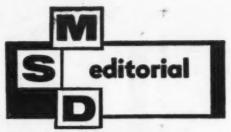
ADVANTAGES

Because of its solid state design, this system offers ■ An 80% Reduction in Weight ■ A 40% Reduction in Size ■ An Exceptionally Low Acoustical Noise Level ■ Extreme Flexibility ■ Improved Efficiency ■ Virtually No Maintenance ■ Instant Starting ■ Pushbutton Control ■ Portability ■ and a Cost Equal to or Lower Than That of Comparable Rotary or Vacuum Tube Systems ■ If yours is a power conversion problem, please write or call for further information.

**ELECTROSOLIDS CORPORATION** 

13745 Saticoy Street, Panorama City, California TRiangle 7-5587 ■ TRiangle 3-3172

CIRCLE 4 ON READER-SERVICE CARD



#### Merry Christmas!

With this issue, MILITARY SYSTEMS DESIGN completes its fourth year. In these four years intensive activity in the design of electronic and electromechanical systems has made possible the manufacture and control of missiles of tremendous striking power. In this time the ICBM has come of age. With the launching of the USS GEORGE WASHINGTON the Western World attains a missile capability which is independent of bases in foreign lands and which does not offer a target for a "preventive" attack by the enemy. Capsule recovery from satellites now brings manned exploration of space only a short step away.

President Eisenhower was undoubtedly correct when he stated in the recent election campaign that the United States is the strongest nation in the world. Many of the readers of MILITARY SYSTEMS DESIGN can personally take credit for important contributions toward this strength.

Well Done!

#### —And An Exciting New Year!

However, important as is the maintenance of a strong military position vis-a-vis the Russian Bloc, this is not enough. President-elect Kennedy recognizes this and has promised aggressive leadership in other important areas. His suggestion of a foreign-service corps of young technically trained men to serve in lieu of military service has great possibilities. Such service should be granted only to young persons highly qualified in every respect, and who would be good-will ambassadors for democracy.

We believe that a crop of developments resulting from space technologies is just beginning to flower. In the coming few years many methods of communication and control will be revolutionized. Business accounting and sales will be increasingly automated as will many of the more tedious chores associated with education. Electronics systems and component designers will find increasing employment in these areas.

More important than the making of better and smaller hardware, however, may be the application of broad techniques of system development and design to the problems of economic growth and management. Some possibilities of this nature are suggested by the use of computers in "War Gaming" and "Management Gaming" exercises.

We are confident that electronics and systems

We are confident that electronics and systems engineers will find 1961 exciting. We also hope that a year from now our progress measured toward a more peaceful world will tell us that it has truly been a Happy Year!

## HIKE Flow Sheet

HOKE REPORTS ON FLUID CONTROL (3

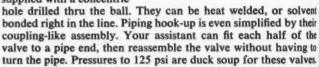
#### WE'VE TOSSED A NEW BALL INTO AN OLD GAME

The technique of molding polyvinyl chloride into ball valve parts is old hat. Even the unplasticized compounds of type I PVC have been kicked around for a while (with minor successes). But until now, no one has booted the ball for a goal.

Perseverance, determination, and the pursuit of economic reward have prompted us to offer a line of ball valves molded of the toughest grade of type I, unplasticized PVC. There are no foreign agents to contribute to a corrosive demise, even in most caustic services. It even meets the proposed new ASTM specification and has a tensile strength of 8500 psi. Those who have had PVC piping problems will profit from the new molding process that

gives these Hokes dimensional stability and very high impact strength. Sensitive systems, human and otherwise, are safe from contamination — they're absolutely non-toxic. We've set 140°F. as the operating temperature limit, but occasional excursions to 160°F. won't do any harm.

All standard models are supplied with a concentric



A maintenance man's delight, they can be cleaned and have their seats changed without leaving the pipe. Their light weight makes them ideal for use on long, unsupported spans of pipe. Size-wise, we're offering them in ½, ¾, 1, 1½, 2, and 3 inch sizes, all NPT female connections.

10

me

ne

in

vel

frie

ver

isti

vid

gra

ma

req

drif

can

cati

ing

You will command the eternal admiration of your colleagues when you install these valves. Be the first to show your rightful status by ordering a shiny new Hoke polyvinyl chloride ball valve. If pride of ownership hasn't motivated you at this point, the mere fact that you are behind the scientific times should move you to find out more.

It isn't necessary to tell us why you want the additional information. Just check the coupon below. We'll forward the facts in a plain, brown envelope.

Hoke's Performance Guarantee — Every Valve Leak-Tested!

HOKE INCORPORATI 13 Piermont Road, C	
☐ PVC Ball Valves	n on the Hoke products checked below:    FREE Corrosion Slide Rule   Complete Catalog GC 960
NAME	TITLE
COMPANY	
ADDRESS	
CITY	STATE

CIRCLE 5 ON READER-SERVICE CARD

MILITARY SYSTEMS DESIGN Nover

#### Scanning This Issue

The close dependency between new techniques and new materials is vividly illustrated in our cover article on ceramic gyros by Jack Lower, Chief Engineer in the Gyro Design Section, Aeronautical Division for Minneapolis-Honeywell. High reliability and long life for gas-bearing gyros were achieved only after development of a new ceramic for vital gyro parts. Other interesting gyro articles include a survey of their use in ballistic missiles and space vehicles by Paul Ott, Nortronics Div., Northrop Corporation, an exposition of the Magneto-hydrodynamic Gyro by R. V. Monopoli, Speidel Corporation, and a brief news item on the General Electric electrostatic gyro, which is still under security wraps insofar as detailed descriptions or illustrations are concerned. (see below)

(3)

L

valve

type

goal.

of the

oreign

caustic on and

PVC

ss that

solven

by their

f of the

aving to

e valves

nd have

t weigh

of pipe

d 3 inch

olleague

rightfu

ride ball

nis point,

uld mov

informa

facts in

k-Tested

Test tables for determining gyro characteristics are described by Paul Kaestner, Chief Engineer of J. W. Fecker, Inc., while two shorter articles describe a sturdy vertical gyro for target drone applications and a versatile miniature rate gyro in which angular momentum rates and gimbal deflection can be controlled to meet job requirements.

In addition to articles on inertial sensors manufacturer's literature on other types of transducers, including angle transducers, thermistors, heat-limit switches, linear and rotary pots, strain gages resolvers and underwater transducers, are briefed in this issue. The advantage of this treatment is that the interested reader can obtain this literature free on request through the MSD reader Service Card.

Other important articles cover the updating of magnetic tape information, by J. C. Hammerton, and a new mechanical energy absorber which promises to save the lives of many navy jet pilots.

#### Electrostatic Gyro is Space Reference

Utica, N. Y.-An electrostatic gyro developed by General Electric's Light Military Electronics Department has successfully operated in tests for 100 continuous hours, according to an announcement made here.

Developed for the Air Force by LMED engineers, the new gyro is being investigated for use in inertial subsystems aboard satellites and space vehicles. Electrostatic suspension eliminates the friction and wear problems associated with conventional rotor spin bearings, and shows promise of considerable reduction in gyro-drift characteristics.

To be practical, electrostatic gyros must provide rotor suspension in the presence of the earth's gravitational field and in other accelerations that may be encountered. In operation, precise control requires keeping the rotor at a constant potential, preferably zero. This suggests that the known lowdrift potential of earth-bound electrostatic gyros can be further reduced in space or satellite applications where gravity fields and acceleration loading are at or near zero for long time periods.



#### DU MONT CHARACTER DISPLAY TUBES ARE USED IN SUCH APPLICATIONS AS:

- Target display and identification
- Air traffic control
- Reproduction of info from coded magnetic tape
- Harbor traffic control
- · and many others

Write for complete technical details Industrial Tubes Sales

enhance any system requiring versatility of rapidly formed characters for readout. A unique Du Mont CRT gun design enables alpha-numeric characters to be formed electrostatically in any size from %" to over 1", and positioned electromagnetically anywhere on the screen - on any size screen from 5" to 19". Other background information, such as a separate radar display for target tracking, can be shown simultaneously through time sharing devices.

Du Mont tubes short-cut expensive system maintenance problems by permitting replacement of the display portion of a system alone - eliminating the necessity of replacing expensive integrated tube and character generator. For versatility, clarity and economy look to Du Mont for character readout.

Available now at attractive prices!

ALLEN B. DU MONT LABORATORIES, Clifton, N. J.



CIRCLE 6 ON READER-SERVICE CARD



Input: 0 to 5 volts, or ±2.5 volts.

Output: 0 to 4 volts RMS (adjustable).

Power Requirements: Less than 70 milliwatts (+20 volts and -20 volts). Specify model PS-20 power supply for

Impedance: Output, 10 K. Input, 1 megohm.

Stability: Temperature, 2% flw change in center frequency or band width for any 50°C change between —55°C and +125°C.

No more than ±1% fbw shift

No more than ±1% fbw shift in center frequency or deviation sensitivity under 50 G linear acceleration; 20 G vibration, 55-2000 cps; or following a 100 G, 11 millisecond shock.

Size: 2.25" x 1.875" x .875".

Weight: Less than 4 ounces.

Holddown: Special captive

screws.
Controls: Output. Centering.
Deviation Sensitivity.

#### **SPECIFICATIONS**

28 volt systems

Linearity: Less than .5% deviation from best straight

Harmonic Distortion: Less



#### DORSETT ELECTRONICS

Typical packaging of Model 0-20 VCO and of other Dorsett "20" series components soon to be an

LABORATORIES, INC.

119 WEST BOYD STREET . NORMAN, OKLAHOMA . JE 4-3750

CIRCLE 7 ON READER-SERVICE CARD

#### Manned Space VehicleMor

requ

Edw

year.

equi

MER

son-S

phon

cons

switc

and

orbit

plays

neces

layin

contr

forde

flight

astro

A

In

MANNED SPACE vehicle pilots in X-15 or succeed. ing high-performance rocket planes will be as closely watched by monitoring teams as their highly-tuned planes. All experimental flights will be scrutinized over a space display unit being designed for the Air Force Flight Test Center, Edwards AFB, California, by the International Telephone and Telegraph Laboratories, San Fernando, Calif.

Separated into vehicular and physiological units, and console will display on the vehicular unit stability and aerodynamic parameters, structural strains, flutter, power plant behavior and various operational fault warnings which will be monitored by an experienced test flight engineer (Fig. 1). The physiological unit displays the pilot's heart rate, blood pressure, temperature, breathing rate and volume, oxygen supply, acceleration and radiation count for the consideration of the monitoring flight surgeon. The console-watching experts exercise only remote control through advice radioed to the pilot.

Because the monitored factors are displayed to show "safe/unsafe" type indications or to trace recent

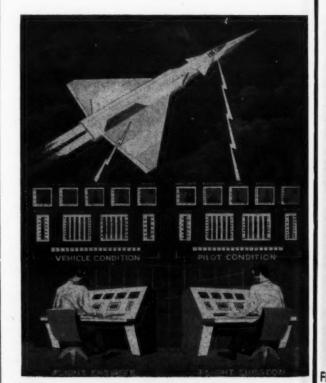


FIG. I. MONITOR SYSTEM for X-15 Type "Inne Space" craft will be built for Edwards AFB by ITTLaboratories. Vehicle and pilot condition indica-MERC Carlso tions are displayed in real time on consoles. are pr

MILITARY SYSTEMS DESIGN Nove

#### icl Monitoring Systems

ceed-

osely

Force

y the

ories,

units,

bility

flut-

fault

enced

l unit

tem-

upply,

ration

tching

advice

ed to

recent

AFB by

history to show dangerous trends, no computers are required and all indications are in "real time." The Edwards AFB monitor will be in operation early next year.

In a similar, although entirely separate project, equipment for the Flight Controller Team of Project MERCURY has been completed by Stromberg-Carlson-San Diego under subcontract from the Bell Telephone Laboratories (Fig. 2). Installed at Cape Canaveral and at the Bermuda Range Station, the display consoles will contain charts and meters to display data, switches to activate systems which control the flight and telephone intercommunications systems.

A large global map will show the manned capsule's orbiting path, location of the remote stations and displays giving critical data about each remote station. The room will contain other electronic equipment necessary for receiving and displaying data and relaying flight controller team's commands. Some direct control of rockets, aborting mechanisms, etc., is afforded by the console team in the case of the Mercury flight, to parallel or supersede those available to the astronaut.

FOR MORE INFORMATION ON: (1) IT&T MONITOR CIRCLE 95
(2) STROMBERG CARLSON MONITOR CIRCLE 96
ON READER-SERVICE CARD



FIG. 2. MANNED SPACE CAPSULE monitor equipment for use at Cape Canaveral by NASA's Project MERCURY is shown nearing completion at Stromberg-Carlson-San Diego plant. Bell Telephone Laboratories are prime contractors for this phase.

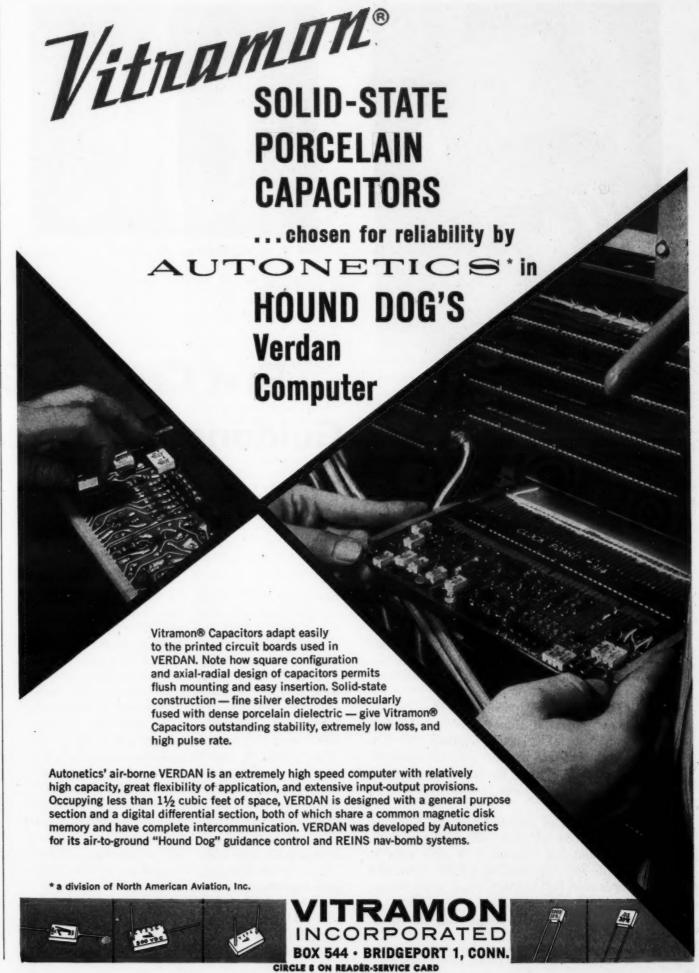




FIG. I. CERAMIC spin motor of new gas-bearing space guidance gyro is being encased in ceramic gimbal. Reduction of bearing noise by 30-to-1 ratio is claimed for new bearing. Rotor is balanced by drilling out metal from band clamped between rotor end-bells.

THE AEROSPACE industry's first ceramic gyroscope, representing significant improvements in gyro accuracy, has been developed by the Aeronautical Division of Minneapolis-Honeywell Regulator Company. Designed for missile and space uses, it incorporates gas lubricated spin motor bearings.

The new gyro marks the greatest improvement in production gyros in a decade. Its development, the result of four and a half years of research, has far-reaching significance in the field of missile and space vehicle guidance.

The gyro was made possible by two major achievements: One was Honeywell's development of a ceramic material as hard as sapphire that can be diamond-honed into the tiny and ultra-precise shapes of critical gyro parts; the other, the development of a miniature ceramic self-generating gas bearing (Fig. 1).

The combination of ceramics and gas bearings has sharply reduced the prime causes of gyro drift inaccuracies, and has resulted in a gyro with a theoretical life span approaching infinity. Previously gyroscopes used ball bearings which are relatively unstable and subject to wear (Fig. 2a), as evidenced by random noise frequencies shown in oscilloscope bearing tests.

The ceramic bearings in the new gyro are lub-

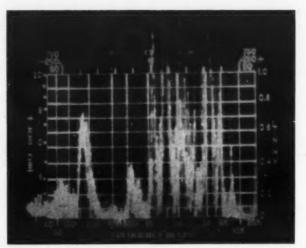
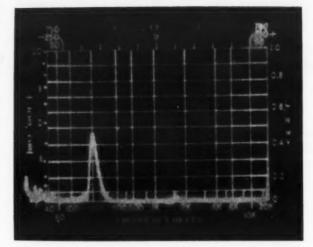


FIG. 2. NOISE-FREE quality of ceramic gas bearing is illustrated by oscilloscope comparison between (a) decibel reading from ball-bearing MIG



gyro, and (b) same readings from gas bearing gyro. Peak at 200 cps is due to fundamental of rotation frequency at 12,000 rpm.

## First Ceramic Gyro For Space Guidance Achieves Ultra-Accuracy

JACK W. LOWER, Chief Eng., Gyro Design, Aero Div., Minneapolis-Honeywell

ricated by a film of gas less than 50 millionths of an inch thick. The film of gas provides a bearing that is stiffer than the steel ball bearings it replaces. At the same time vibration, or bearing noise, is decreased by a ratio of 30 to 1 (Fig 2b).

Although the principle of the gas bearing is not new, previous models without ceramics have been severely limited due to size and bearing wear caused by starting and stopping. The new gyro is only 2.817" long and 2.0" in diameter and weighs only half a pound. In tests its super-hard ceramic bearings have undergone many thousands of starts and stops without detectible wear. In addition to nearly eliminating the drift caused by the ball bearings, drift caused by the instability of other critical gyro parts has been reduced considerably by using ceramics in the spin motor and gimbal constructions.

Even such exotic gyro materials as beryllium have undesirable characteristics that can cause gyro drift. In stability tests of its new ceramics, Honeywell subjected the material to temperatures ranging from -85°F to 1500°F and the material retained its original dimensions within measurement

accuracy. The ceramic material is so inert that Honeywell cleans it in hydrochloric acid to remove sub-microscopic foreign particles that could affect gyro performance. The acid dissolves everything but the ceramic, permitting cleaning and assembly techniques in production substantially advanced beyond the conventional use of cleaning solvents and ultrasonic scrubbing.

Ceramic gyro parts are rough cast in powdered form. The material can be worked easily in the half-fired "green"state. After final firing at above 3000°F the material becomes as hard as sapphire.

Although the ceramic is harder than ordinary grinding wheel materials, it can be finished with diamond compounds to extreme accuracy and excellent surface finish. Tolerances on some parts of the new gyro are being held to less than three millionths of an inch.

Honeywell has been conducting research in the field of close tolerance ceramics for several years and recently began full-scale commercial production of precision ceramic components for military and industrial applications.

Pre flotat weigl tion t bearing trosta this a It i that t

Th tion i ture in mi the M reduc gratin by t

fluid off d A princ moto

port

front that : torqu

bility

that

is err

On forma the to conve contro errors Un

ly im

balan torque supply compl puts. The

torque peatal straint types Hoy

cause

unwar

#### Floated Gimbal Suspension

The ceramic gas bearing unit is the next generation in a family of gyros that began with the miniature integrating gyroscope (MIG), presently used in missile and space vehicle guidance systems. Like the MIG, the gimbal of the new gyro is floated to reduce gimbal friction torque. In a floated integrating gyro the input turning rates are converted by the gyroscopic element into gimbal torques. These torques are time integrated through a viscous fluid into gimbal displacements which may be read off directly by a displacement type pickoff.

A practical mechanization of the floated gyro principle results in a gyroscopic element (spin-motor) sealed within a cylindrical gimbal supported by a viscous fluid to obtain near friction-free support (Fig. 3).

#### **Unwanted Gyro Torques**

Two categories of unwanted gimbal torques confront the gyro designer. The first is a friction-torque that tends to mask off some lower level gyroscopic torques to limit the angular rate threshold capability of the gyro. Second is an unbalance torque that comes from other than gyroscopic action and is erroneously measured as an angular motion.

Present production floated gyros with gimbal flotation suspension reduce greatly the first category—friction torque. Flotation of the gimbal weight to better than 99 per cent has reduced friction to the order of a million times less than ball bearings. Advanced developments in hydrostatic fluid gimbal supports, magnetic suspension or electrostatic suspensions are within reach to improve this area several orders of magnitude further.

rell

hat

ove

fect

ing

bly

ced

ents

ered

the

ove

nire.

nary

with

ex-

s of

mil-

the

ears

duc-

tary

It is the second category of unbalance torques that the ceramic gas bearing spin motor significantly improve.

One of the most significant measurements of performance for a gyro is its drift uncertainty. Because the turning rate inputs to the gyro element are converted to gimbal torque, any unwanted, uncontrolled, torques applied to the gimbal cause errors to be introduced in the output response.

Unwanted torques may come from gimbal unbalance, electromagnetic reactions of pickoffs and torque generators, elastic restraint of the flex leads supplying power for the spin motor, or from the complex responses of the gyro under vibration inputs.

There is usually a fixed amount of unwanted torque in any one gyro that is consistent and repeatable and this error can be balanced out by trim adjustment with little difficulty. Magnetic restraint and flex lead elastic restraint are typical types of this fixed torque.

However, the gyro designer is still left with some unwanted torques that cannot be compensated because they are inconsistent. These inconsistent

#### HOW THE GAS BEARING OPERATES

The gas bearing functions as a passive device capable of supporting a load on a thin film of gas without any external aids such as pressure lines or gas supplies. The basic principle of the gas bearing may be illustrated as follows. Consider a single journal bearing consisting of a shaft rotating in a concentric bearing shell as shown in Fig. 4.

As the shaft rotates, the gas within the clearance space is set into motion by the viscous shear forces of the gaseous lubricant. Pressure builds up in the direction of rotation until the minimum film thickness (h<sub>o</sub>) is reached. At this point, throttling begins and the pressure drops off rapidly. Within the "wedge" area approaching the point of minimum film thickness, the viscous shear forces must be balanced by the pressure forces. Now, the basic mechanism for load support utilizes the principle of constant mass flow. For the journal bearing without end flow, the mass rate of flow must be constant along the axial length of the bearing. Expressed symbolically:

 $\rho vh = constant$ 

where  $\rho =$  density of the gas, v = average gas velocity, and  $h_0 =$  film thickness.

When the bearing is loaded, it takes an eccentric position and the film thickness varies sinusoidally around the journal. Accordingly, either the density of the gas, the velocity of the gas, or both, must vary inversely to satisfy the continuity equation above. These velocity and density variations require the existence of pressure gradients with the integrated effect being sufficient to provide load support. The pressure profile shown in the diagram will vary with load, axial position, bearing geometry, etc. Although the profile shown is not necessarily typical of all journal bearings, it is adequate for a qualitative discussion.

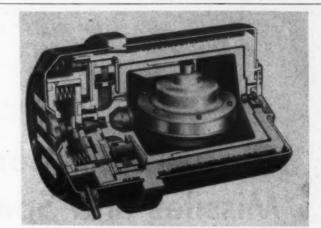


FIG. 3. CUTAWAY VIEW of gas bearing gyroscope shows spin-motor supported in a cylindrical gimbal supported by a viscous fluid to achieve near friction-free support.

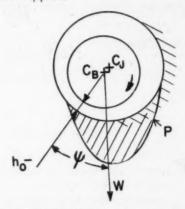


FIG. 4. GAS BEARING Principle depends on load-bearing strength of film of helium gas. Built up by shaft rotating in a concentric bearing shell. W is load on bearing;  $\psi$  is attitude angle; ho, minimum film thickness; P is pressure profile providing support.

torques establish the true uncertainty level of the gyro and set performance limits for gyro drift.

Control of these inconsistent torques is where the ceramic gas bearing gyro has shown significant results. It has proved to be the solution to torques resulting from movement of the ball retainers and shifts of the balls in the race way, mechanical hysteresis effects due to material damping and ball slippage, the stress and strain of the balls under angular motions of the gyro which cause deformations that change the balance of the gyro, and mechanical rectification of the vibration set up by the ball bearings of the spin motor.

In the ceramic gas bearing gyro the troublesome balls and retainers are eliminated, viscous damping is substituted for hysteresis damping and deformations due to thermal expansion disappear. Vibration or bearing noise is decreased by a ratio of 30 to 1.

Gas such as air or helium has been found to be an effective bearing lubricant so long as the bearing geometry is proper. While the gas lubricated bearing is in operation its elements are separated by a thin film of gas (Fig. 4). Consequently there is no contact between the bearing elements and wear is negligible.

Careful choice of material for the gas bearing is necessary to provide high reliability for a number of starts and stops. Surface finish, cleanability, hardness, and stability over time and temperature cycling are extremely important factors. Application of the new ceramic material to miniature gas bearing development was a major breakthrough. Ceramics have a high modulus of elasticity and exhibit very good thermal stability and low long-term creep. These characteristics are extremely important when dimensional control and stability are essential.

The stability advantages of ceramics also make this material more attractive than metals, including beryllium, for use in other parts of the gyro such as the gimbal, coil cup, and encapsulation of the spin motor stator.

FOR MORE INFORMATION CIRCLE 97 ON READER-SERVICE CARD

## Gyro Applications in Ballistic Missiles and Space Vehicles

By PAUL W. OTT,

Nortronics Div., Northrop Corporation

GYROSCOPES are used in ballistic missile and space applications as sensors for both guidance and control systems. They are used as angular position sensors in both systems and as angular rate sensors in control systems. The angular position gyros may be either of the single-degree-offreedom integrating type or of the two-degree-offreedom type, both of which have been used extensively in ballistic missile and space applications to date. Angular rate is measured with singledegree-of-freedom spring restrained instruments. The state-of-the-art of angular position gyroscopes has advanced considerably over the last decade resulting in the present day performance which has made inertial guidance for ICBM's feasible.

#### Missile Guidance System

A gyro stabilized inertial platform, containing in addition to the gyros three accelerometers, is the sensing element for an inertial guidance system. Since the gyros stabilize the platform in inertial space, the acceleration, velocity and position of the missile as calculated by the computer may be compared with a stored reference (Fig. 1). Any errors in the trajectory are corrected by applying the appropriate guidance signals to the control system.

The gyros used on the platform may be three single-degree-of-freedom integrating gyros or two two-degree-of-freedom gyros depending on the system being used. These gyros are quite different in construction and operating principles but both supply an angular position reference to inertial space.

The single-degree-of-freedom integrating gyros presently being used are an outgrowth of the work of Dr. C. S. Draper and his staff at M.I.T. Instruments of this type are widely used on present day intercontinental ballistic missiles. The fluid flotation technique used permits these gyros to perform well under the environmental conditions of vibration, acceleration, and shock experienced in the missile.

The two-degree-of-freedom gyros are of various configurations as developed by several different groups. The devices are gimbaled rotor structures with angular error sensors on the gimbals. A redundant axis results from the use of two of these units on a platform.

Presently under development are so-called strapdown guidance systems which do not have an inertial space referenced gimbaled platform, but consist of three single-degree-of-freedom gyros and three accelerometers mounted directly on the missile. Since the sensors are not stabilized in space, the computer must be capable of considerably more complex computations. In addition the gyros must have larger memory angles than when used on platforms since the missile response to perturbations is much slower than the gimbaled platform's response and, therefore, error angles of several degrees may result before proper correction is made. This requirement has resulted in the development of very low drift gyros with memory angles of ±5 degrees or more (Fig. 2). This gyro application is similar to that of the control system application to be discussed below except that the required drift performance is much more stringent.

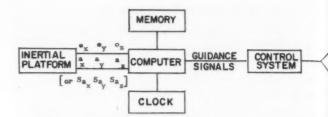


FIG. 1. MISSILE GUIDANCE system using three single-degree-of-freedom gyros and three accelerometers on a gimbaled inertial platform provide error angle and acceleration data to a computer where they are compared to a stored reference. Guidance signals resulting cause the control system to actuate guidance rockets, etc.

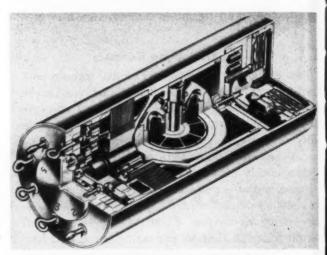


FIG. 2. SINGLE-DEGREE-OF-FREEDOM Gyro is sectioned to show construction. Present gyros attain very low drift with memory angles of ±5° or more and are frequently used "strapped down" to missile instead of in a gimbaled platform.

mal

than

are

resp

requ

freq

frec

reas

wel

hav

suc

Der

the

tion

que

gyr

rate

Cus

the

#### Missile Control System

Since ballistic missiles are large non-rigid bodies which are aerodynamically unstable, a control system is required to stabilize them. The control system will detect and counteract the instabilities such as bending, fuel sloshing, displacement of center-of-pressure and center-of-gravity, winds, etc. The control system consists of angular position and angular rate sensors, appropriate amplifiers, and thrust control devices (Fig. 3).

Many of the control systems now being used have as position sensors three single-degree-of-freedom integrating gyros. These gyros must have memory angles of  $\pm 5^{\circ}$  or more to accept the angular error perturbations. It is also necessary to program these gyros to the nominal trajectory with guidance corrections being supplied by the guidance system.

Angular rate information is required by the control system to provide a stable system. Mechanically restrained rate gyros are presently used for this

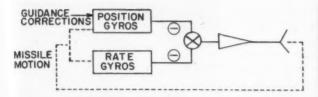


FIG. 3. CONTROL SYSTEM consists of angular position and angular rate sensors both acting to provide inputs to the amplifiers and thrust control devices.

ee

ro

er-

at-

or to

odies

l sys-

l sys-

such

enter-

The

and

and

have edom emory

error

these

e cor-

stem.

e con-

ically

r this

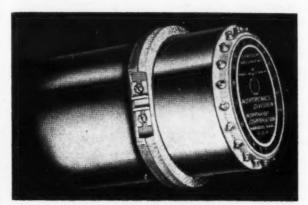


FIG. 4. SUBMINIATURE RATE GYRO with controlled damping is used at specific points on missile to measure missile motion.

purpose on most missile programs. These rate gyros are located at specific positions on the missile to make sure the gyros measure missile motion rather than local bending.

The performance requirements for the rate gyros are not too stringent except that their frequency response must be adequate to meet control system requirements. This usually means that their resonant frequency be well above the control system response frequency and that their damping be controlled to reasonable limits. From these considerations, as well as those of minimum size, weight and power, have evolved subminiature gyros with controlled damping requiring no heaters. Fig. 4 illustrates one such unit manufactured by the Precision Products Department of Nortronics.

For some control system applications such as the second stage Able vehicles, rate information is obtained by proper "shaping" of the angular position signal. This is possible only if the bending frequencies are relatively high and/or the position gyros are located so as to be free of bending mode rates.

#### Initial Control in Space Missions

The space vehicle usually consists of several stages of launch vehicle plus the final payload containing experimental equipment. The above discussion of ballistic missiles describes, in general, the launch vehicle.

Various sensors have been proposed for attitude

## BREEZE

## flexible shielding conduit and fittings

#### TO MEET YOUR REQUIREMENTS

Manufactured to meet government specifications, industrial and commercial requirements, the complete line of Breeze flexible metal shielding conduit and fittings for suppression of electrical interference and mechanical protection is described in a comprehensive catalog just off the press.

The line includes specific types of conduit designed to provide:

- FIRE PROTECTION
- ABRASION RESISTANCE
- LIGHT WEIGHT
- EXTRA FLEXIBILITY
- RESISTANCE TO SALT WATER CORROSION
- WEATHERPROOFING

Conduit can be supplied in random mill lengths or cut to order. In addition, complete assemblies consisting of conduit and fittings (ferrules couplings, nuts, connectors, adapters, collars, inserts) can be provided. Hardware can be furnished separately as can flexible wire braid covering. For special orders on conduit, hardware or braid, consult the





#### BREEZE CORPORATIONS, INC. 700 Liberty Avenue, Union, New Jersey · Telephone: MUrdock 6-4000

Manufacturers of electrical, electro-mechanical and hydro-mechanical components and systems and fabricated metal products.

CIRCLE 9 ON READER-SERVICE CARD

### **Why You Get More Stable Reference Junction Compensation**

with an AUTOREF



You get less total reference temperature variation in an "AutoRef" because all system variables are held to an absolute minimum. Temperature stability, for example, is = 1/5°F. And the thermocouple wire in all "AutoRef" systems is specially selected from our own wire mill to surpass I.S.A. premium grade accuracy. Total "AutoRef" system accuracy is further insured by proper distribution of individual thermocouple junctions, balanced electrical heat input and heat transfer, and sensitive primary control elements. This system accuracy is held to # 1°F. over ambient temperatures of 75°F., = 25°F. Such total system accuracy makes the "AutoRef" ideal for measuring temperatures together with other DC signals as on multipoint recorders and other data reduction systems. Minimum No. of points, 12-no maximum.

Write for Bulletin 81-9



In Canada: THERMO ELECTRIC (Canada) LTD.

CIRCLE 10 ON READER-SERVICE GARD

#### REC's 800 SERIES, PRESSURE TRANSDUCERS



Sensor utilizes a free-edged, circular diaphragm of Ni-Span C. Full scale ranges are from 1 to 100 psi and differential or absolute pressure measure

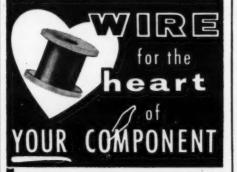
The 15 psi range features 100 percent overpressure, no resonances less than 2500 cps, and a pneumatic greater than .004 seconds. Maximum excitation voltage is 110 V rms and the capacity ratio change is such as to directly produce an output equal to 25 percent of

Write for Bulletin No. 36010



ROSEMOUNT

CIRCLE 11 ON READER-SERVICE CARD



Wire drawn to your specifications (down to .00025") in base and precious metals and alloys . . . supplied bare, enameled, ceramic insulated for use at 1000° F., or electroplated . . . to close tolerances.

Our research and development staff is available to solve YOUR wire problems.

Write for data on your specific needs.

SECON METALS CORP. SECON White Plains 9-4757

CIRCLE 12 ON READER-SERVICE CARD

stabilized payload applications. Among these are sun sensors, earth seekers, moon seekers, star trackers and gyros. The limitation of gyros as sensors is that of gyro drift. Since most space missions (lunar or planetary) involve several days travel at the very least, even a small amount of drift is unacceptable. On the other hand, gyros are very desirable as control system sensors for detecting missile body rates. Therefore, for many applications, a system consisting of gyros as rate sensors for the control system and celestial body sensors for guidance will no doubt be used.

The necessity of the payload control system operating during the long period from launch to landing (or orbiting) presents some gyro considerations different from those of the ballistic missile application. Of special concern is gyro life expectancy and probability of proper operation during extended midcourse operating periods. The fact that the gyro is operating in a zero-G, essentially vibrationless environment for most of this time means that the gyro is operating under very nearly ideal conditions since such degradations as mass unbalance, mass unbalance shifts and anisoelastic coefficients are no

longer of any concern.

Almost all of the thrust control devices proposed for space vehicles involve gas jets. Dual control systems consisting of on-off gas jets and some proportional control, such as servo-motor-flywheel systems, may be employed. The gas jets serve as a means of "dumping" the flywheel angular momen-tum when the full speed of the servo motor is reached. Proportional gas jets are now being developed to obviate the need for dual control systems. In either of these systems it is necessary to keep the body angular rates as low as possible to reduce the total gas consumption, and to do this it is necessary to detect extremely low angular rates. The single-degree-of-freedom integrating gyro used as an electrically restrained rate gyro is capable of detecting rates as low as a few degrees per hour.

Angular rate sensing is also required to reduce the perturbations which may occur at separation of the payload from the rest of the missile. These rates will probably be large enough so that they may be detected with spring-restrained rate gyros. This rate information would then be appropriately processed by the control system to reduce the perturbations to an acceptable level.

An interesting application of gyros for space missions is that of a second stage coast phase. With the advent of restartable engines (such as Able Star, Agenda B) it is necessary that the missile attitude be controlled during rather long coast periods. This means that the missile will probably exceed the normal radio guidance range before the engine is restarted and, therefore, the control system (or strap-down guidance system) gyros must control the attitude. To maximize the probability of the correct attitude for second stage restart, the gyro drift should be as small as possible. Therefore, normal control system gyros may be required to operate satisfactorily in a zero-G vibrationless environment as well as during powered flight.

FOR MORE INFORMATION CIRCLE 98 ON READER-SERVICE CARD

In telemetry and data retrieval, in s-loop guidance systems and entation, failure-proof splicne of tapes to precise lengths, with

iten

visi

sist

rad

into

Fire

hole

Fin

wid

whi

thos

bon

spec

cati

The

ness

accurate lateral end-alignment and minimum ridge thickness is a prime requirement. It is a fact that there is no tape splicer in the world today the PRESTO-SPLICER, that meets all of these requirements with



digital tapes t first-order toler ances, producing weld which i actually the strong

or further information, write:



address: PRESTOSEAL, Long Island City, N. 1 CIRCLE 13 ON READER-SERVICE CARD MILITARY SYSTEMS DESIGN Nove

#### Electronic Specialties Feature Teflon Characteristics

Subminiature Teflon® terminals, O-rings, mechanical limit stops and instrument clamps are among the items featured in a new 24-page pocket-size catalog by the Sterling Precision Corporation, Component Division, 5 Sintsink Drive East, Port Washington, L. I., N. Y.

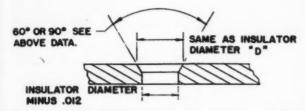


FIG. I. PREPARATION of hole in chassis for insertion of TEFLON terminals is simple.

Specially developed 100% virgin Teflon with consistently low dielectric constant, low power factor over a frequency range from 60 cps to 30 mc, and low capacitance is used in a wide range of standoffs, feedthrus, jacks and plugs for HF, VHF, UHF, Microwave, radar and other high class electronic circuitry. These are installed permanently in 4 seconds, in metallic or non-metallic chassis, with a simple "corking" motion into punched or drilled holes.

Preparation of the hole for installation is simple. First the hole is drilled to the insulation body diameter "D" minus 0.012" (Fig. 1). When the material is over 0.040" thick, countersink the insertion side of the hole 60°. When the material is less than 0.040" thick, countersink with a 90° included angle countersink. Finally press the terminal into place. The resiliency of virgin Teflon seals and holds permanently without extra hardware—no nuts, washer, staking or soldering.

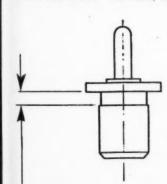
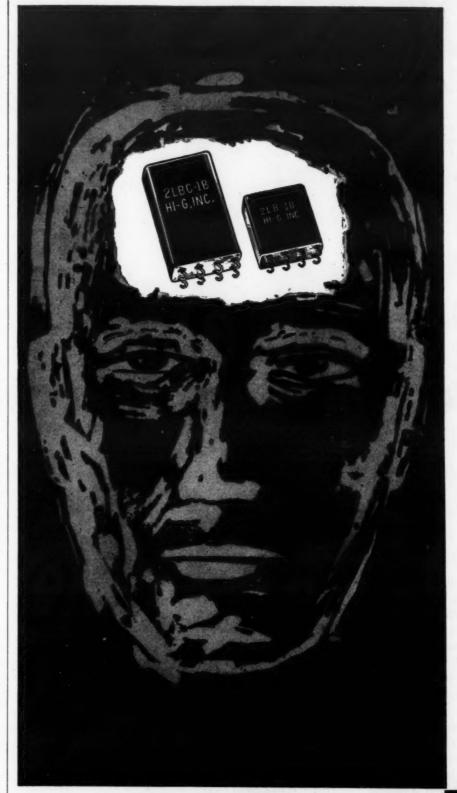


FIG. 2. INCREASED Pullout resistance can be provided to customer specification by groove "G" supplied to fit chassis thickness.

Insulators, terminals and jacks are available in a wide number of styles in white or eight RETMA colors which are applied to the insulation in such a manner as to leave the dielectric properties unchanged from those of natural Teflon. When increased mechanical bond and pullout resistance is considered advisable, special terminals will be furnished to customer specification with a groove in the Teflon bushing (Fig. 2). The customer must advise as to exact chassis thickness

® Registered trademark of the Du Pont Co.

FOR THIS LITERATURE CIRCLE 99 ON READER-SERVICE CARD



## NEW LB SERIES LATCH RELAY

## the relay with a memory!

The new LB Relay has the ability to remember its last input and will maintain the latched or unlatched position without continuous power drain, resulting in lower power dissipation. An effective magnetic latch system has been incorporated to provide greater stability and longer life. The LB Series features balanced armature construction, with extreme mechanical ruggedness as found on all Hi-G relays.

pe: DC Microminiature Latch Relay Style No. 2LB-1B and 2LBC-1B

2LB-1B: .400 x .800 x .875" max.

2LBC-1B: .400 x .800 x 1.275" max.

Contacts: 1PDT and 2PDT dry circuit to 2

amps resistive at 32 VDC

Life: 100,000 cycles, standard

Sensitivity: 2LB-1B: 2PDT-Standard DC sensitivity to latch and unlatch. 300MW or better at 25°C. 1PDT-150 mw or better.

2LBC-1B: 2PDT-Standard DC sensitivity to latch and unlatch, 40MW or better at

25°C. 1PDT-25 mw or better.

Temperature: -65°C to +125°C

Dielectric

Strength: 1000 VRMS at sea level

Insulation

Resistance: 1000 megohms min.

Optional

Terminals: Long or short leads for printed circuit application or hook type for standard

wiring.

Mounting
Provisions: Brackets, studs or straps available.

Send your relay requirements for prompt

engineering evaluation — today.







THE ONLY COMPLETE LINE OF BALANCED ROTARY RELAYS

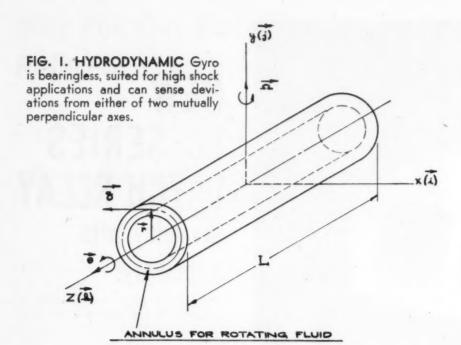
BRADLEY FIELD, WINDSOR LOCKS, CONN.

CIRCLE 14 ON READER-SERVICE CARD

N.Y

y. N. 1

ARD



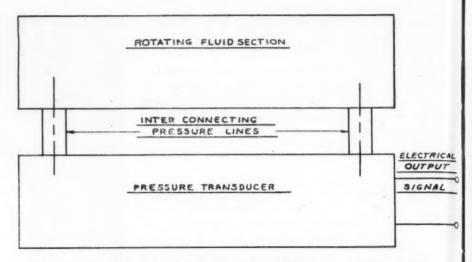


FIG. 2. TRANSDUCER SECTION is connected with pressure lines to rotate fluid section of hydrodynamic gyro.

### The Magnetohydrodynamic Gyroscope

R. V. MONOPOLI, Industrial Division, Speidel Corporation, Providence, Rhode Island

THE MAGNETOHYDRODYNAMIC gyroscope is a device in which a conducting fluid, e. g. mercury, is driven by a rotating magnetic field around a closed annular path formed between the inner surface of a magnetic sleeve and the outer surface of a magnetic cylinder placed inside the sleeve and concentric with it. When the device experiences rotation about any axis other than the fluid spin axis, a Coriolis force acts on the spinning fluid creating a pressure gradient along the spin axis. The magnitude and direction of the pressure differential developed from one end of the fluid annulus to the other are functions of the magnitude and direction of the input angular velocity. A suitable transducer can sense this pressure signal and convert it to an electrical output signal.

The analysis of the operation of this type of gyroscope must be approached through principles which are different from those applicable to the common gyroscope.

Represented in Fig. 1 is a cylinder concentrically located inside a sleeve. Both cylinder and sleeve are

made from a high permeability magnetic material. The space between them forms an annulus which is filled with mercury and closed at the ends with copper rings. These rings conduct current passing through the mercury and are the counterparts of the shorting rings in a squirrel cage induction motor. Each ring has a small pressure port at the upper half of the y, z plane.

Not indicated in the figure, but actually present, are longitudinal slots in the outer circumference of the cylinder containing copper wires wound in a manner standard for stator windings of a three phase induction motor. Three phase currents in these stator windings cause a rotating magnetic field to be directed radially across the annulus. The field induces eddy currents in the mercury. Interaction between the eddy currents and the rotating magnetic field causes the mercury to be driven in the annular path.

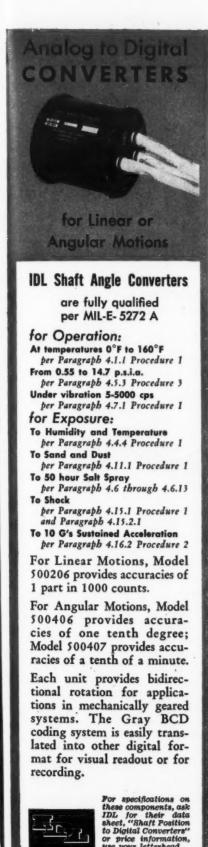
When the device experiences rotation about any axis other than the fluid spin axis, a Coriolis force acts on the spinning fluid creating a pressure gradient along the spin axis. Thus a pressure differential, p, is developed between the pressure

ports at opposite ends of the fluid annulus which is given by the vector equation

$$p = 2 \delta \vec{Lk} \cdot [\vec{\Omega} \times (\vec{\theta} \times \vec{r})]$$
 (1)

where  $\delta$  is mercury density,  $\overrightarrow{\theta}$  is the angular velocity of mercury,  $\overrightarrow{q}$  its linear velocity where it passes the pressure ports,  $\overrightarrow{r}$  the mean radius of the annulus,  $\overrightarrow{\Omega}$  angular velocity of the device (here shown to be completely around the y axis), L its length, and  $\overrightarrow{\theta}$  x  $\overrightarrow{r}$  =  $\overrightarrow{q}$ .

Because the linear velocity vector reverses direction each 180°, this same pressure differential is developed between two points at one end of the annulus separated by that amount. Therefore, an alternate location for the pressure ports is at the same end of the annulus, one in the upper half and one in the lower half of the y, z plane. For the case depicted in Fig. 1 where the orientation is such that all vectors are normal to each other, equa-



ch is

(1)

ocity

s the

ulus,

to be

and

direc-

ial is

of the

e, an

it the

If and

or the

ion is

equa-

these components, ask IDL for their data sheet, "Shaft Position to Digital Converters" or price information, use your letterhead.

INSTRUMENT DEVELOPMENT LABORATORIES INCORPORATED

54 MECHANIC STREET, ATTLEBORO, MASS.

CIRCLE 15 ON READER-SERVICE CARD DESIGN November-December, 1960 tion (1) reduces to the scalar equation

 $p=2 \delta L \Omega q$ 

A unique advantage of this type gyroscope is that rotation about either of two mutually perpendicular axes can be sensed by a single unit. This is accomplished by having a second pair of pressure ports displaced 90° from the pair previously mentioned.

Conversion of the pressure signal to an electrical output signal can be accomplished using transducers such as the following (See Fig. 2):

1. Mercury cut-off switch-in which the tip of a metallic contact placed in mercury is either covered or uncovered by an insulating diaphragm actuated by the differential pressure, thereby opening or closing an electrical circuit.

2. Differential transformer-in which the differential pressure acting on a diaphragm or piston causes linear motion of a magnetic core within standard differential transformer windings.

The first of these transducers allows operation of the device as a rate switch which will actuate at some predetermined rate of turn. With a differential transformer type transducer, the device operates as a rate gyro, giving a continuous output signal with amplitude and phase proportional to rate and direction of turn respectively.

In both transducers the mercury in the annulus and in the transducer forms a closed fluid loop interrupted only by the diaphragm or piston. These moving elements are inertia compensated, i.e. the average density of the materials used in their construction is equal to the density of the mercury. The transducer is thus rendered insensitive to inertia forces.

Results from the development test program undertaken by the Industrial Division, Speidel Corporation, 88 Ship St., Providence 2, R. I., have demonstrated the practicality of a gyroscopic instrument based on the principles proposed by Dr. P. F. Malder of Brown University, holder of a patent on the device. The obvious advantages which this device has over the conventional gyro are:

1. Construction is greatly simplified since no bearings are required.

The rugged construction makes it well suited for operation under extreme conditions of shock and vibration.

Sensing can be accomplished about either of two mutually perpendicular axes with a single unit.

With input powers of less than five watts, the sensitivity is one degree per second when operated in the form of the simple rate switch previously described. Greater sensitivities result from the use of a higher input power in a larger device, in cases where space, weight, and power are not limiting factors. The damping and natural frequency are adjustable within limits.

FOR MORE INFORMATION CIRCLE 100 ON READER-SERVICE CARD

## 100,000 VOLT

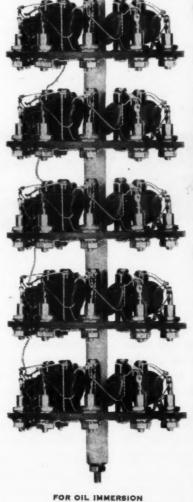
SILICON RECTIFIER IN 0.15 CUBIC FEET

CLIPPING
CHARGING
DIODES
RåDAR
MODULATOR
CIRCUITS

combinations
replacing tubes in power supplies for: Klystron, Travelling
Wave and Cathode Ray Tubes
... Infra-Red and Atomic Instrumentation . . . FM and Single
Side Band Transmitters.

OTHER HIGH VOLTAGE

The advanced technology which produced the single unit 2,000 PIV silicon rectifiers, making possible the most reliable and compact very high KV combinations, is evident throughout Columbus Semiconductors® extensive line of silicon rectifiers. Over 350 JEDEC types from 50 to 2,000 PIV and from 200 mA to 25 Amps, as well as all seven JAN power types are available.



FOR OIL IMMERSION IN SERVICEABLE, SEALED METAL CASE.



#### COLUMBUS ELECTRONICS CORP.

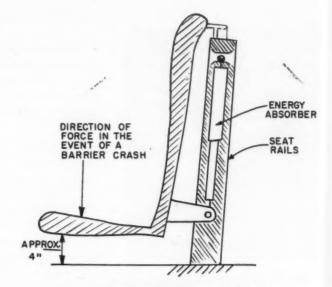
1000 Saw Mill River Road, Yonkers, New York
Tel: YOnkers 8-1221 • TWX: Yonkers, NY-1369

CIRCLE 16 ON READER-SERVICE CARD

## **Energy Absorber Cushions Pilot** in Barrier Crashes

CHAS. N. HOOD II, Director of Engineering,

Airborne Accessories Corporation, Hillside 5, New Jersey



fit

in in

tra

(6

du

sta

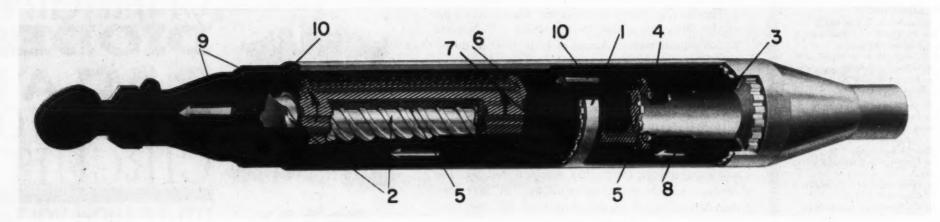
for

ter

the

Nove

FIG. 1. NEW ABSORBER is Link in normal seat-adjusting Mechanism.



DESPITE modern angled-deck carrier designs, jet pilots are still occasionally injured when barrier crashes or hard landings occur. In barrier crashes a deceleration force of up to 30 G for approximately 0.033 second can develop, usually resulting in vertebrae injury. A load of 18 G, on the other hand, can be safely experienced when the pilot is positioned and secured in the typical aircraft seat.

This device, developed by Airborne Accessories Corporation, safely absorbs 12 G above the endurable shock limit of 18 G. The weight of the pilot, seat and personal flight equipment total just over 300 lbs, which must be decelerated by 5 G in only 5" of cockpit space.

Naval Air criteria met are: Action of the device is relatively independent of environmental conditions; at loadings below 18 G, the device acts as a rigid member; it acts without rebound; is highly predictable in its action; it is re-useable, directly calibratable and testable. These criteria eliminated techniques dependent on crushing, elongation or shearing of material. Also, hydraulic mechanisms

were considered unpredictable over the expected temperature range, as were several potentially interesting clutching arrangements involving powdered metals. The approach selected uses controlled friction clutches incorporating a provision for their calibration and adjustment. The device translates the linear impact motion into rotary motion for actuation of the clutch discs. The mechanism is a member of the normal power-operated seat-adjusting mechanism (Fig. 1).

The purpose of the *Energy Absorber* is to carry all tension loads up to 18 G without physical change. Any further load causes the unit to elongate, absorbing the excess energy and thus limiting the maximum force transmitted to the "protected" load.

The plain colored portions of Fig. 2. show the members which move axially under a tension exceeding 18 G. The cross-hatched colored members also rotate during elongation in addition to moving axially, and are driven by the worm threads on the inner-surface of cylinder (5) and externally on part (2). Note that some of the clutch discs rotate with the cylinder because they are splined to its exterior, while alternate discs are kept from rotating by the

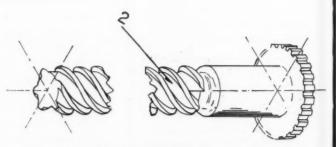


FIG. 2. ENERGY ABSORBER is independent of environmental conditions; operates only on forces exceeding safe deceleration.

inner splines in member No. 10. Friction between the two sets of discs dissipates the energy, raising the temperature approximately 15°F in a single operation in which the device absorbs 12 G under a 302-lb load.

#### **Detailed Operation**

The elegance of the design is shown by the manner in which a breakaway peak load is avoided. Actually if the applied load approaches an impact, a momentary negative peak occurs. Also, after use the device may be collapsed and reset for a second operation without disturbing its calibration.

Referring again to Fig. 2, the center member, No. 2, is helically splined externally but terminates in a flange with longitudinal splines. These splines mate with the internal longitudinal splines of the outer sleeve (1), which extend throughout its length. After assembly, part No. 2 is securely fastened in Part No. 1 so that it cannot turn or slide under tension.

No. 10 is a cylinder with external straight splines which slide easily into the internal splines of member No. 1. No. 10 also contains internal straight splines. One end of No. 10 is threaded internally to fit stop No. 3, which has external splines to fit internal splines in No. 1. These prevent rotation of No. 3, but permit free axial translation of No. 3.

No. 3 bears against a spring pack No. 8 consisting of a number of Belleville disc springs. Following the spring pack is a thrust bearing No. 4, which transmits its thrust to a friction pack consisting of alternately stacked outer discs (7) and inner discs (6). The outer discs are externally splined to mate with member No. 10, while the inner discs are internally splined to mate with external splines on part No. 5.

Part No. 5 has internal helical splines that mate

with the external helical splines of part No. 2, while the right end of No. 5 rests against thrust bearing No. 4. The friction pack, thrust bearing and disc spring pack are held under compression by the pressure adjusting nut No. 9 which screws into internal threads in the end of part No. 10.

At rest, the pressure of spring pack (8) forces discs (6) and (7) of the friction pack together, preventing rotation of the assembly. The maximum force necessary to overcome this friction is determined by the setting of the pressure adjusting screw No. 9.

Applying an impact tension load in excess of this maximum value through parts (9), (10) and (3) compresses the spring pack (8) and forces the thrust bearing (4) against the splined cylinder, No. 5. This momentarily relieves some of the pressure on the friction discs, providing a momentary "negative peak" during breakaway. The disc pressure and full friction loading is quickly restored as part No. 5 rotates with a rotary screw motion toward the left end of part No. 2. Friction between the discs retards this rotary motion and converts the thrust energy into heat.

Once elongated, the device is removed from the

seat adjusting linkage, the lock between members 1 and 2 disengaged, part No. 1 slipped off the inner assembly and part 2 is screwed back into its retracted position in sleeve No. 5. The inner assembly is then inserted into sleeve No. 1, and members 1 and 2 re-locked together. This returns the device to its ready state, no change in the spring loading adjustment being necessary.

During tests of aircraft barrier crashes when the pilot seat is equipped with the shock absorber, the aircraft has been found to travel 6.3" after the impact. The pilot in his absorber equipped seat moves 10.5", with the absorber extending 4.2". This lengthens the man's period of deceleration from the .033 seconds in which the aircraft is arrested to .055 seconds, and reduces his peak deceleration from 30 G to a safe 18 G.

Other possible uses of the new absorber principle may include automobile safety belt arresters, and landing gear shock absorbers. The Energy Absorption Device was designed by Louis Fuchs, Senior Development Engineer, and is the subject matter of a pending patent application assigned to Airborne Accessories Corporation, 1414 Chestnut Ave., Hillside 5, New Jersey.

FOR MORE INFORMATION CIRCLE 101 ON READER-SERVICE CARD

#### Gimbal Angle Transducers Require Increased Accuracy and Speed

Missile stable platform pickoffs, operating to ever higher limits of precision and speed, are demanding more thoughtful consideration from the designers of guidance system transducers. Single and dual-speed synchro and resolver pickoffs are giving way to Inductosyn¹ and optical encoder techniques utilizing standard and pancake configurations for those applications requiring the highest precision. Both the Inductosyn and optical techniques are available in coaxial pancake configurations—permitting straightforward adaptions to presently available gimbal systems—in precision devices now being produced by the Dychro Corporation, Wellesley 81, Mass.

For analog systems and particularly those that must

<sup>1</sup> Inductosyn is the registered trademark of Farrand Controls, Inc., New York 70, N. Y.

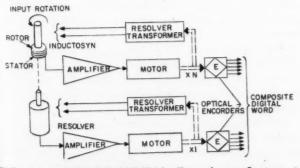


FIG. I. ANALOG-DIGITAL Transducer System is provided by combination of Inductosyn and optical encoders.

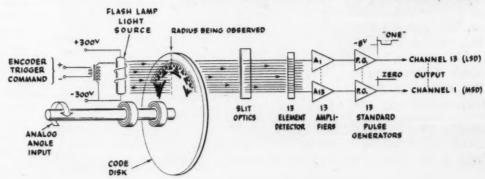
be compatible with two-speed pickoff systems, the Inductosyn is unsurpassed for ruggedness and simplicity of application. For digital pickoff requirements, direct encoding is available with accuracies to one minute of arc in systems allowing a 3" to 5" diameter instrument. The system shown in Fig. 1 combines these two techniques to provide both analog and digital information with great resolution and accuracy, Both optical encoding and Inductosyn techniques can be used in the accuracy range from a few seconds of arc to a tenth of a degree or more; realization of these accuracies being dependent upon dynamic performance requirements and other parameters.

The system (Fig. 1) uses a resolver as a coarse pickoff and an Inductosyn co-axial arrangement as a fine pickoff for a single gimbal axis. The Inductosyn output is equivalent to that of a resolver geared up N times where N may be any value between 50 and 250. These outputs operate servo repeater positioned shafts so that the information may be distributed in analog and digital form as required. These repeaters are generally designed so as to be especially compact and reliable. The accuracy of this system is dependent upon the size of the pickoff Inductosyn and the dynamic performance required in the servo repeater.

When a digital readout is required in the simplest and most direct manner, an optical encoder is mounted directly on the gimbal. Fig. 2 shows the principles of operation of such an encoder. Strobotron lamp illumination sources are commonly employed in military applications of optical encoders because they permit very high light levels and a pulsed signal system. A number of output configurations are available to reduce the number of slip rings required.

FOR MORE INFORMATION CIRCLE 102 ON READER-SERVICE CARD

FIG. 2. OPTICAL ENCODER with strobotron lamp illumination provides pulsed coded outputs with accuracies to one minute of arc in 3" to 5" diameter instruments.



veen

sing

op-

nder

nan-

ded.

pact,

use

cond

ESIGN

## **Electronic Circuitry**

A continuing MILITARY SYSTEMS DESIGN feature, these circuits are selected because they represent good design. Significant characteristics which are not self-evident from the diagram are explained in the printed commentary.

#### TRANSISTORIZED-SCOPE DEFLECTION AMPLIFIER

A 2-v sweep from the trigger and sweep generator circuit is direct-coupled into the horizontal-deflection amplifier (Fig. 1) to maintain a high amplitude stability. This is first fed into Q21, an emitter follower, and is attenuated through resistor R76 and mixed with the positioning voltage from R72. With the degeneration due to the emitter resistor (R60) in Q15, the voltage gain of the string of PNP transistors (O15, O17 and O19) is approximately 100. This signal is connected to the first horizontal-deflection plate (Terminal 5). A small amount of this sweep voltage is picked off across R74 and coupled into Q20, where it is amplified by the NPN string of Q16, Q18 and Q20. This string has a voltage gain of about 30 and provides the opposite-phase signal to the other horizontaldeflection plate of the CRT. (Terminal 4).

The biasing for the PNP string of transistors can be arranged to give equal voltage drops at any given d-c output with the resistors, R64, R67, R70 and R74 (top). However, using only these resistors, sufficient drive to the bases cannot be obtained when the transistors are near full conduction. R66 and R73 (top) provide this increased base current for Q17 and Q19 when the string is in full conduction. The same ar-

rangement is used for the NPN string.

In a triggered type of sweep, the period between sweeps is longer than the duration of the sweep. It is, therefore, permissible to use a deflection amplifier having good response during the forward trace time and reduced performance during retrace time. This is accomplished in the model 150 by utilizing the com-

plementary characteristics of P-N-P and N-P-N transistors. The P-N-P string, Q15, Q17 and Q19 is driven into higher conduction during the forward trace time and produces the positive-going deflection waveform. The complementary N-P-N string produces the negative going deflection waveform.

The effective bandwidth of either amplifier string is determined primarily by the deflection plate and stray capacities combined with the driving impedance of the amplifier string. Since the driving impedance of each string is 50K shunted by the impedance of the transistor string during the forward trace and the full 50K during retrace, the forward trace bandwidth is significantly higher than the retrace bandwidth. Bandwidth is further enhanced by the small high frequency by-pass capacitors C24 and C25. One of the benefits gained by this technique is the reduced power supply drain derived from the use of the 51K load resistors.

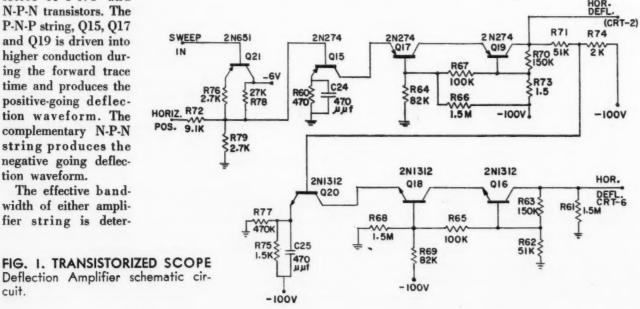
Display: 1" CRT (NU P-122P1) with 6 div by 10 div graticule.

Sweep range: 5 calibrated steps-1 µsec/div, 10 μsec/div, 100 μsec/div, 1000 μsec/div, 10,000 μsec/

Triggering: Synchronized from plus or minus slope or free-runing. Signal amplitude of ½ div or more will provide stable sweep. Trigger point is continuously adjustable from any point of the display on either positive or negative slope.

#### TRANSISTORIZED-SCOPE POWER SUPPLY

The source power for a small oscilloscope<sup>1</sup> can be an external nominal 6-v source or an internal 6-v rechargeable battery. The 6-v supply feeds a conventional square-wave dc-to-dc converter that has 3 output windings. One of the output windings (8-7-9), is a 16-v center-tapped winding. It is connected to two fullwave rectifying circuits and provides ±8-volt output (Fig. 2.).



630 TCRI5 C29 OUT Q23 LC32 +84 ± €34

FIG. 2. TRANSISTORIZED SCOPE Power Supply schematic circuit.

The second output winding (10-11) is a 100-v winding, full-wave rectified to give -100 volts to the deflection amplifier.

The third output winding is also a 100-v winding (10-12) connected to one terminal of the first 100-v winding. The fact that the first 100-v winding is feeding a full-wave bridge rectifier gives a 200-v peak-topeak square wave on the otuput end of the second 100-v winding, which is fed into a half-wave voltagedoubler circuit (CR14, CR15, CR16 and CR17) to provide a theoretical output of -700 volts. The actual output voltage (after losses in the coupling capacitors and due to loading effects) is a nominal -600 volts.

Source: EI Labs Div. of Electro Instruments, Inc., 1165 Morena Blvd., San Diego 10, Calif.

1Note: The Deflection Amplifier and Power Supply circuits given above are components of the Electro Instruments Model 150 Transistorized Oscilloscope further described on page 48 of this issue. For more information on this instrument circle 103 on reader service card

#### DIRECT-COUPLED AMPLIFIER FOR HIGH VOLTAGES

Where large voltage swings are required in excess of the maximum collector voltage rating of transistors available, the circuit shown in Fig. 3 may be used. In this circuit, the arrangement of Q1, Q2, Q3 and Q4 permits the use of a -100 v supply for Vcc which is divided among the resistors so that the collector voltage of each transistor is within the rated value of -30v for each Type 2N384 transistor. Since a single transistor does not permit a voltage swing in excess of its rated maximum collector voltage, the high instantaneous output voltage across R1 must be shared at all times by the transistors connected in series. The transistors do not require matching for identical characteristics, and any number, in addition to the input transistor, may be used.

The voltage swing for each transistor appears across the 18K resistor connected in its base circuit, and the overall voltage swing appearing across the load resistor RL is the sum of the voltage swings of the individual stages.

The current gain of the overall circuit is the same as that of the input stage Q1, where the connection can be either grounded-base or grounded-emitter. When large current gains are desired, the grounded emitter connection, as shown, should be used.

Data for the 2N384 transistor are as follows: It is a

cuit.

the industry's pioneer & complete line of

CUSTOMIZE EFFICIENCY & ACCURACY WITH TRIO LABS' BUILD-IN INSTRUMENTS



-600V

OUT

31

32

ly

nd-

de-

ling

00-v

eed-

c-to-

ond

age-

to

tual

tors

lts. Inc.,

pply In-

furmore

ader

ss of

stors

d. In

ch is

volt-

e of

ingle

xcess

h in-

ed at

The

tical

the

cross

d the

resis-

indi-

same

n can

When

nitter

t is a

+8V



instruments were used to measure AC and DC volt-ages . . . cluttered, tedi-ous, wasteful, subject to error.

AFTER . . . 3 trie lebs' miniature VTVMs inte-grally built-in new are always on hund to meas-ure just the parameters you designate.

By building-in trio labs' panel-mounting instruments you . . . customize test systems, set-ups and instruments; save space (average model is 4" x 4" x 4"); save time with at-a-glance monitoring; save money; make monitoring foolproof (go no go"); improve system reliability; increase overall design freedom. Choose from many "standard" or "special" models-or consult us for new designs for your needs. Write for free "how to" Engineering Guide to Dept. MSD-12

MILITARY for MIL-E-5400A & MIL-T-945A applications





COMMERCIAL



D Series-ruggedized Multi-range AC VTVMs \$272.



low-level multi-range AC VTVM \$199.





pc vrvms \$84.50







Model 110-1 low-level multi-runge DC VTVM \$285.



CIRCLE 17 ON READER-SERVICE CARD ESIGN November-December, 1960

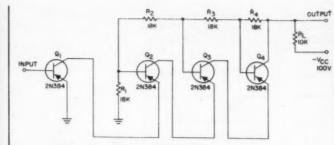


FIG. 3. HIGH VOLTAGE d-c amplifier.

PNP germanium drift type transistor with 120 mw max dissipation at 25°C, having a Vce of 40 v max, h<sub>fe</sub> of 60, maximum cutoff frequency of 100 kc, and Icbo of 12 amp at 25°C.

Source: Contributed by J. B. Angell, Philco Corp., Circuit 2-7 in Selected Semiconductor Circuits, Navships 93484, Government Printing Office, Washington, D. C.

#### TWO-METER POWER SUPPLY

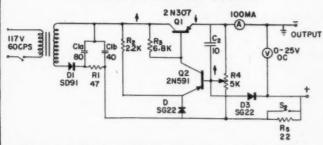
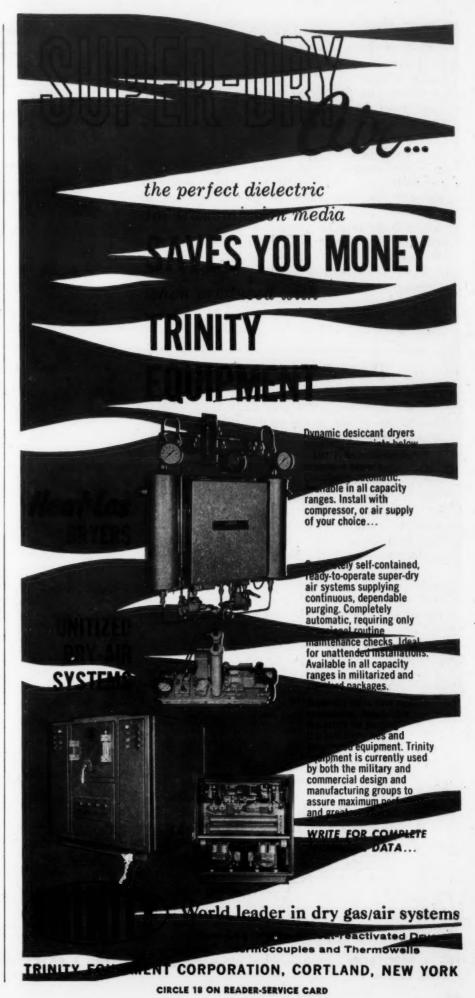


FIG. 4. POWER SUPPLY has guard circuit to protect transistors from shorted output. Output voltage is adjustable from 0 to 20v. DI is Silicon rectifier, DC and D3 are Stabistor (Transitron) reference diodes. Arrows indicate voltage-change phase.

The power supply for breadboard transistor circuits or experimental work shown in Fig. 4 features regulated output and a guard circuit to prevent damage to power supply components in the event of a shorted output.

A 117/24v transformer provides isolation of the power supply from commercial power lines, and the half-wave output of diode D1 is filtered by the network R1 C1. Transistor Q1 operates as a series voltage regulator with its base potential determined by the collector voltage on control transistor Q2. Potentiometer R4 is the output voltage control.

Q2 acts as a common emitter amplifier with its emitter-base potential stabilized by diode D2. Any sudden surge in line voltage or decrease in load causing an increase in the potential across R4 will result in an increase in the base-emitter voltage; this signal will be amplified by Q2 but with a phase reversal, which means that there will be a decrease in the Q2 collector potential. Q1 is acting as a common-collector amplifier, which makes it act much the same as a cathode follower. This means that its output voltage waveform will have the same phase as the input signal waveform, but that it will have negative voltage amplification. The decrease in potential applied to the base of Q1 is then transmitted to the Q1 emitter as a decrease in output potential.



#### ELECTRONIC CIRCUITRY

Continued from page 17.

Regulation of the circuit, using a 2N307 transistor as Q1, is shown in Fig. 5. For greater voltage stability, a higher gain 2N176 can be used instead. Voltage stability of the circuit is a function of the product of the gains of both transistors.

The guard circuit R5 and D3, limits the output current whenever an overload occurs. If the output terminals are shorted across, output voltage builds up across R5 and at 1.7 volts D3 conducts, removing the forward base-emitter bias on Q2 and reducing the emitter collector current. This in turn removes the forward bias from Q1, cutting its output to the minimum. At the same time, C2 is harmlessly discharged through D3.

Input: 110-125v 60 cps. Output: 1-20 v dc, 100 ma. Maximum load current 100 ma.

Regulation: 100 ma increase in load current produces less than 2 v change in output voltage.

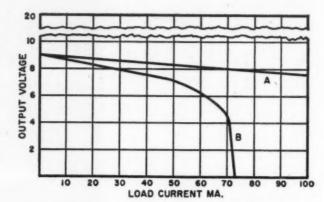


FIG. 5. REGULATION Characteristic, (A) Guard Circuit out, (B) Guard Circuit in.

Output impedance: With Guard Circuit out, 20 ohms.

Source: "Dual Meter Power Supply" Popular Electronics, November 1960.

#### In Fig. 1, th

### TRANSISTOR CIRCUITS—CURRENT FLOW AND VOLTAGE PHASE RELATIONS (Second article in a continuing MSD Series)

In the following NPN circuits (Fig. 1), electron current flow is indicated by the direction of the arrows, with the flow of the minority carriers being ignored to simplify the circuit explanation. In this discussion it is assumed that with normal bias and no signal input, 95% of the emitter current reaches the collector, and 5% flows to the base. In each case if the NPN transistor were replaced by a PNP transistor, the polarity of the batteries and the direction of electron flow would be reversed, however, the voltage phase relationship would be the same.

CB Amplifier. The wave form at the left of Fig. 1-a represents the input signal wave. Consider an instant B at which the polarity AB opposes the forward bias of the base emitter battery. The forward bias is thereby reduced, reducing the total current I flowing through

the emitter. The collector and base currents are correspondingly reduced, and the voltage drop in R<sub>1</sub> is also reduced. This causes the output voltage (to the right of coupling capacitor C) to rise accordingly. By similar action, when the forward emitter-base bias is increased, the emitter-collector current rises, causing a larger voltage drop through R<sub>1</sub>, and causing the output voltage CD to swing negative. The output signal is in phase with the input signal in a CB amplifier.

CE Amplifier. The response of the Common Emitter circuit to a similar input signal is shown in Fig. 1-b. Here a positive swing in bias aids the emitter-base bias, increasing the emitter-collector current, increasing the voltage drop through the load resistor, and causing a negative excursion of the output voltage. In

-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051
-.051

FIG. I. ELECTRON current—voltage phase relationships in NPN circuits.

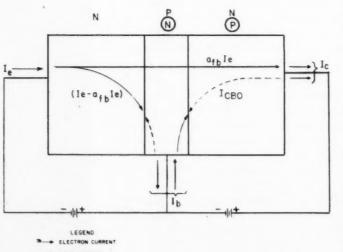


FIG. 2. BASE LEAD current direction and magnitude depends on relative strength of reverse bias current.

similar fashion, a negative input signal swing diminishes the emitter-collector current and causes a positive swing in the output voltage. In short, the output of the CE amplifier is 180° out of phase with the input.

CC Amplifier. The response of the Common Collector circuit is shown in Fig. 1-c. Here an increase in positive signal polarity aids the emitter-base bias, increasing the emitter-collector current. This causes a larger voltage drop across the load resistor R<sub>1</sub>, which in this case means that the emitter output lead becomes more positive. As the input voltage swings negative, the emitter-collector current diminishes, causing the voltage drop through R<sub>1</sub> to diminish, which swings the output lead more negative. The result is that the output wave is in phase with the input signal; however, since the voltage of the collector battery is divided between the emitter-collector resistance and R1, the output voltage amplitude is always less than that of the input signal.

#### Effect of Reverse Current

In Fig. 1, the reverse current flow between the base and the collector was neglected. In an actual case, the direction of electron current flow in the base region depends on the percentage of emitter current that flows from the base lead and the magnitude of the reverse bias collector-base current that enters the base lead. In Fig. 2 an NPN transistor is shown with normal biases applied. To the minority carrier electrons in the base region, the base region acts as N-type material, as indicated by the circled N. To the minority carriers (holes) in the collector region, the collector region acts as P-type material.

The emitter current  $I_e$  consists of electrons. Assuming the current gain of the common base amplifier is designated by the symbol  $\alpha_{fb}$  (and defined as the ratio  $I_c/I_e$  in the forward biased common base amplifer), the collector current will be  $\alpha_{fb}I_e$ , which will account for 92% to 99% of the emitter electrons. From 1% to 8% of the emitter electrons ( $I_e-\alpha_{fb}I_e$ ) combine with holes in the base region, generated near the base lead. Generation of the holes causes an electron current to flow in the base lead away from the base.

In addition, reverse-bias collector current,  $I_{\rm cbo}$  flows between b as and c ollector.  $I_{\rm cbo}$  consists of a flow of electrons in the base region that combine with holes from the collector region at the base collector junction. The reverse bias current causes a flow of electrons in the base lead and  $toward\ the\ base$ .

The direction of the resultant electron flow will be seen to depend on the relative magnitudes of ( $I_e$ – $\alpha_{fb}I_e$ ) and  $I_{cbo}$ . If  $I_e=1$  ma;  $I_{cbo}=0.01$  ma; and  $\alpha_{fb}=0.92$ , the resultant base lead current would be 0.07 ma flowing away from the base. If  $I_{cbo}=0.02$  ma, and  $\alpha_{fb}=0.99$ , the base lead current will be 0.01 ma, flowing toward the base.

In a PNP transistor, the roles of the internal electron and hole currents, also the bias potentials and directions of electron flow externally, are reversed. (Some hybrid parameters of the common emitter transistor circuit will be developed in the Circuitry Section of the January-February 1961 issue).

<sup>1</sup>Note. Material in this series is adapted in part from U. S. Army Technical Manual TM 11-690.

to pr

of Ja

The

miles

than

The

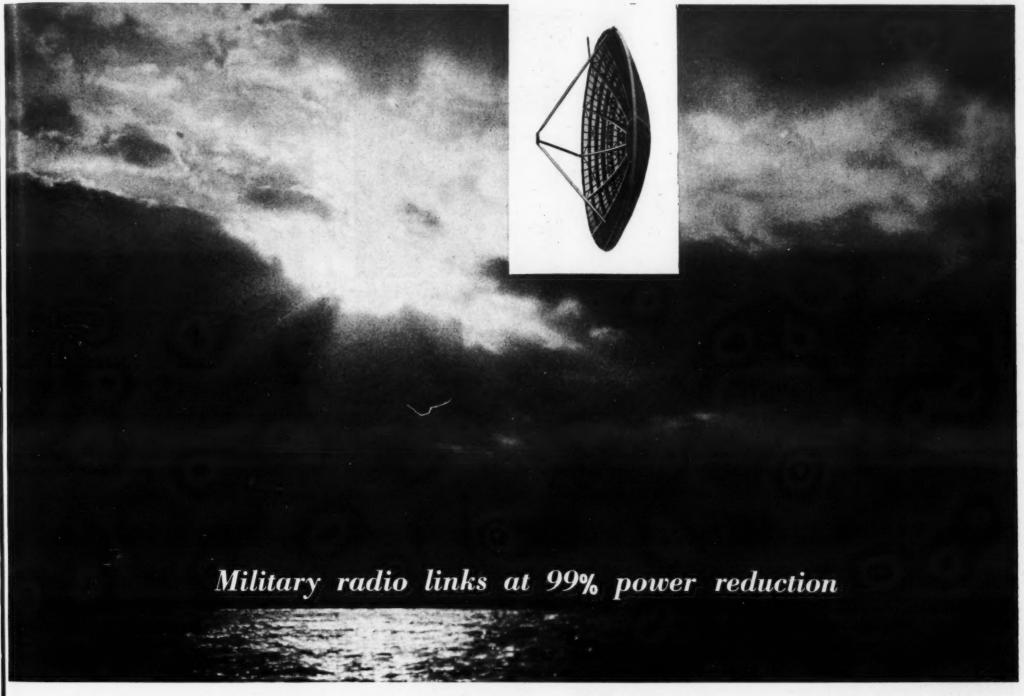
feede

S/N I

for c

The

the-h



The United States Air Force has picked NEC's High Sensitivity Reception System to provide over-the-horizon radio links for radar sites on the three main islands of Japan.

The 17-station system contains no active repeater stations. Longest hop is 145 miles at  $100\,\mathrm{W}$  output. Guaranteed reliability is a character error of no more than 1:10,000 for 99.9% of a year's hours.

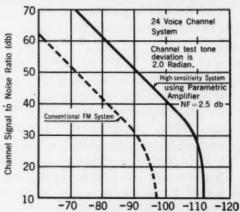
The NEC system combines high sensitivity reception, parametric amplifier, low feeder loss design, and the high antenna gain possible at 2000 mc. to improve S/N ratio by more than 20 db. This permits hops at 1/100 of the power required for conventional links.

The OH-2000 is drastically reducing installation and maintenance costs of over-the-horizon links in capacities up to 60 voice channels. A descriptive brochure is available on request.



#### OH-2000

With quadruple diversity, this compact 100 W transmitter requires a radio room of only 100 sq. ft. Final stage uses economical planar tubes. NEC also supplies completely transistorized carrier equipment.



Receiver Input Power (db below 1 milliwatt)

NEC Components / Systems

Nippon Electric Company Ltd.

CIRCLE 19 ON READER-SERVICE CARD

ESIGN November-December, 1960

siut ut. ecin ina ich nes the oltthe put nce een oltput

the cion ows erse. In ases base inciers acts

er is ratio fer),

1% bine base cur-

lows w of holes tion.

ns in

ill be

 $(I_e -$ 

and

ld be

0.02

0.01

ctron

direc-

Some

sistor

on of

from

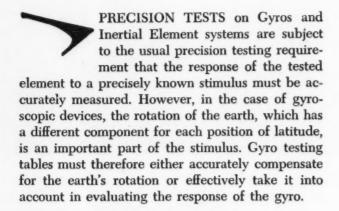
Tokyo, Japan

19



## Gyro Test Tables

PAUL KAESTNER, Chief Engineer, J. W. Fecker, Inc., Pittsburgh 6, Pa.



#### Types of Gyro Tests

Gyro testing equipments fall into two general types, depending on the philosophy governing the test. In one method a very accurately known regular rate input (compensated for earth's rotation) is applied to the gyro. The error output of the gyro is then plotted or recorded automatically for comparison with the known input. (Fig. 1). The test instrument is known as a variable rate table, and both rate and displacement gyros may be tested. Several gyros may simultaneously be tested on a single rate table if the error output from each gyro is used to drive a separate recorder.

In the second type of test, the gyro is used in a closed-loop system, with the table acting in its normal function as a null-seeking device. In this case, the gyro responds to the earth's rotation by sending an error signal to the torque servo of the test table on which the gyro is mounted. Its accuracy should ideally keep the servo table axis aligned on a fixed star. A step function test is also possible with the servo table. This determines how quickly the gyro or system settles down to a steady state after a severe disorientation.

#### Rate Tester Tables

Rate tables employ precision drives and, where the accuracy demands, frequency-regulated power supplies for their synchronous drive motors. Various types of variable speed drives may also be employed to permit operation of the rate tables over a continuous range of rates through zero speed. These include mechanical variable-speed control devices as well as rate speed controls. In use, the rate tables provide a known input to the gyro under test and the gyro performance is evaluated by measuring its response to the rate.

One type of variable rate test turntable provides a synchronous motor combined with a servo motor

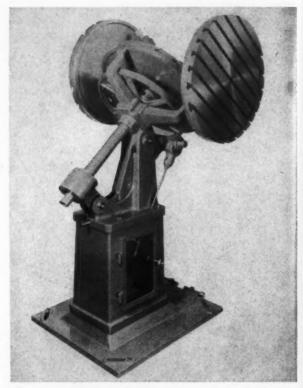


FIG. 2. SIDEREAL TEST Turntable, Model 063, when adjusted for the correct latitude and driven at sidereal speed, points the gyro axis continually at a fixed point in space. Any variation in gyro output is therefore due to drift.

tilt ma

cas for

tio

Th

the

ada

gra

lica

Fli

ele

tab

axi

mo

turi

drive through a mechanical differential to produce continuously variable speeds through zero and to maximum speed in the reverse direction. Temperature compensation in the servo motor feedback tachometer may be used to improve accuracy. Where the desired rates are not too high, a worm gear mesh is usually employed for the final table drive gear mesh. This type of gearing provides smoother rates, less subject to the high-frequency tooth-profile rate errors which are found in spur gear drives. At higher rates, above 750°/minute, worm gear surface speeds become excessive and other types of drives must be used.

A special configuration of the rate table is the sidereal rate table (Fig. 2). This unit provides a position output within 5 seconds of arc of its theoretical position with respect to the fixed stars, throughout its rotation. The axis of rotation of the test platform is set parallel to the earth's axis by either precision surveying techniques or by direct astronomical observation using a special telescope. The table is driven by a synchronous motor from a crystal-controlled frequency source at sidereal speed and multiples thereof. The sidereal day is almost 4 minutes shorter than the solar day, due to the earth's motion about the sun.

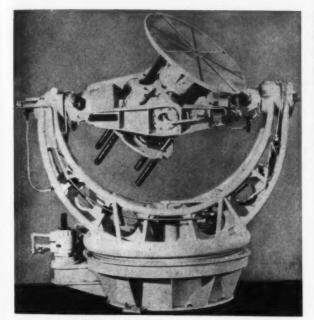


FIG. 3. THREE AXIS Scorsby Flight Simulator is hydraulically-driven unit for testing stable-element units weighing up to 200 lbs.

063

n at

at a

tput

duce

d to

era-

back

racy.

orm

able

vides

ency

spur

nute,

and

the

les a

theo-

stars,

f the

is by

lirect

cope.

peed

lmost

o the

Rate tables are frequently mounted on yokes for tilting in one plane or on gimbals and yokes for tilting in two planes. The tilting means may be manually operated to provide the desired angles and may be provided with precision optical read outs for accurately determining the angles. In other cases, the tilt operation only requires a capability for restoring the equipment to its original orientation at the conclusion of the test. One of the angles of extreme interest for gyro testing is that which corresponds to the latitude of the test site. This allows the gyro to be completely isolated from the effects of precession caused by the earth's rotation.

Two- and three-axis tables are frequently power driven in all axes, generally through limited ranges. These drives may provide harmonic motions with continuous rotation available on one axis. Since these multiple axis tables are usually servo driven to follow some form of program they are readily adaptable as flight simulators to follow any program within their performance ranges. A hydraulically driven unit of this type is the 3-axis Scorsby Flight simulator (Fig. 3), which can test stable-element units weighing up to 200 lbs. Test turntables employing servo drives on a single tiltable axis are also widely used.

#### Servo Test Tables

One type of servo table (Fig. 4) is driven by a dc torquer mounted directly on the table drive shaft to eliminate the gearing usually associated with servo drives. The table may be used in a slave mode with the gyro under test mounted on the turntable surface with its input axis parallel to the



## P-30 COMPUTER ABSTRACTS

(Application Report #10, from which the following is abstracted, is free upon request from Royal McBee Corporation, Data Processing Division, Port Chester, N.Y.)

### Subject: Design / User: Brown Fintube Company, Elyria, Ohio

THE PROBLEM: rush quotation for heat exchanger to potential customer. Determine best heat exchanger vs. cost combination. Perform necessary computations to obtain values for total surface area; total number of exchangers; area/exchanger; velocity and pressure drop—shell and tube; film coefficient; log mean temperature difference; overall transfer rate; clean rate; overall fouled rate; surface actually required; duty; price.

**METHOD:** the compact, low-cost Royal Precision LGP-30 Electronic Computer.

INPUT DATA: except for special specifications which are handled by design engineers, non-technical personnel fill in data directly from customer inquiry sheets. This information is then punched

on tape.

Solution: the engineer reads the above data into storage in specifically assigned memory lo-

cations on the computer's magnetic drum. The set of program instructions—also stored on the drum—then directs the computer where to find the input data and what mathematical operations to perform in the proper sequential order. The program then further directs the computer to store the various answers in specifically assigned memory locations.

Of notable interest is the incorporated test feature which allows any type and arrangement of sections to be tested by the computer. The program not only compares calculated values, but provides a corrective computation and recomputes all conditions until satisfactory values are obtained. The engineer need only type in the exact arrangement desired to have the computer calculate his proposed arrangement — assuring complete versatility and control over the program.

OUTPUT: all numbers required for the final specification sheet, including price, are provided—as

well as key intermediate answers
to enable the engineer to exercise judgment.
The computer
automatically
controls the typewriter so that



all answers are printed out in the desired format.

Conclusions: with the LGP-30, Brown Fintube has reduced total time on typical heat exchanger designs from one or two hours to approximately 3 minutes. Better design vs. cost combinations have been obtained—with a resulting increase in contract awards and the elimination of under-bidding. According to company officials, "perhaps the most significant contribution of the LGP-30 has been the release of engineering manpower for more basic and profound studies."



#### **Royal Precision Corporation**

Royal Precision is jointly owned by the Royal McBee and General Precision Equipment Corporations. LGP-30 sales and service are available coast-to-coast, in Canada and abroad through Royal McBee Data Processing offices. For your free copy of Application Report #10, as well as full specifications on the compact, mobile LGP-30, write today to

ROYAL MCBEE CORPORATION, data processing division, Port Chester, N.Y

CIRCLE 20 ON READER-SERVICE CARD

## PRECISE A.C. VOLTAGE DIVISION ACCURATE TO 10 P.P.M.





Precision Decade Ratio Transformers that feature high input impedance, low output impedance and negligible phase shift. Fine Instrument Switches incorporated for long term accuracy. Models shown packaged in Smartly Styled Hardwood Cabinets and priced from \$210 to \$305. Other models available.

- RESOLUTION: 0.001 to Infinite
- INPUT VOLTAGE: 0.35 f (500 Volts Maximum)
- . ACCURACY: 0.001%
- . OUTPUT IMPEDANCE: 1.5 Ohms Maximum
- . FREQUENCY: 50 to 10,000 CPS

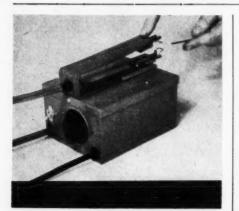
G. L. COLLINS



CORPORATION

2820 EAST HULLETT STREET LONG BEACH 5 CALIFORNIA

CIRCLE 21 ON READER-SERVICE CARD



#### **NEW MODEL G THERMAL WIRE STRIPPER**

Strips both Teflon and low-melting plastics.

No blades to cut or nick wire.

Has continuously-variable heat control.

Strips any size wire without adjustment.

Use either as bench or hand tool.

Designed for production-line use.

Price \$69.50 FOB Altadena, Calif.

Always available from stock.

Western Electronic Products Co. 2420 North Lake Avenue, Altadena, Calif.

CIRCLE 22 ON READER-SERVICE CARD

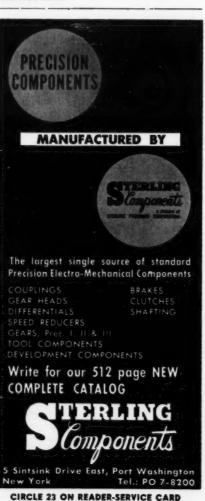


table axis. The table then rotates to reduce the error signal produced by the gyro. An optical electronic readout is provided which provides a pulse with each 6 minutes of arc table travel. With the addition of auxiliary timing, amplifiers, counters and printer, it is possible to print the elapsed time between consecutive pulses. In this mode of operation with the table set at the sidereal or latitude angle at the test site, a perfect gyro would drive the table at sidereal rate. Any departure from this condition would represent gyro errors. At other angles the component of the earth's rate will differ



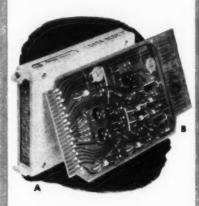
FIG. 4. MULTIMODE TEST TURNTABLE, Model 052, has DC Torquer mounted directly on drive shaft. If set accurately for the sidereal angle at the test site, a perfect gyro will drive the table at sidereal rate, with any departure from this condition representing gyro errors.

from the sidereal rate by amounts which depend on the actual angles involved.

The servo table shown in Fig. 4 is also provided with a microsyn, the stator of which is rotated with the turntable shaft. Its rotor is driven by an accurate synchronous motor drive which provides one or more rates. The microsyn output may be used to provide the error signal to the torquer motor. In this mode of operation, the unit is actually used as a rate table although it is not quite as accurate as the direct drive rate tables. To provide greater accuracy for rate operation, special direct gear at-

## THESE TWO FLIP-FLOPS

Identical!



#### DIFFERENT PACKAGES, YES

TRAK

Conne

triode from mediu availa

plate

in 196

TRAK T

TRAK T

TRAK TY

TRAK Ty

TRAK Ty

TRAK Ty

TRAK Ty

new T

Nover

— but the two high-speed flip-flop modules shown here are electrically exactly the same . . . just two more of the wide selection of Harvey-Wells Data-Bloc and Data-Pac logical building block matched pairs that make possible an entirely new way to design digital systems.

Here's why: Harvey-Wells high speed Data Blocs feature logic diagram front panels for rapid breadboarding of any digital system configuration — the compatible, easy-to-use Data Blocs are jumpered together until the new system design is thoroughly checked out. With the breadboard complete, the basic design kit Data Blocs are replaced with their Data-Pac compact electrical equivalents. The result — a working, rugged prototype or final system.

Write today for your copy of a technical brochure that gives full details about this new way to design digital systems.

A. Data Bloc Flip-Flop 1011

B. Data Pac Flip-Flop 2011 Speed ... 5 mc

Inputs . . . Set, Clear, Complement Internal Delay . . . 0.1 usec.



CIRCLE 24 ON READER-SERVICE CARD
MILITARY SYSTEMS DESIGN



### **Miniature MICROWAVE OSCILLATOR** CAVITIES

now available

TRAK Electronics Company, Wilton, Connecticut, announces the formation of TRAK MICROWAVE CORPORATION to increase its developmental facilities for triode cavities in r-f signal generation from 500 Mc upwards. Present low, medium and high power cavities are available for application in grid pulse, plate pulse, and CW service.

TRAK expanded its Microwave Cavity line, which started in 1949, by adding the following 7 NEW miniature Cavities

TRAK Type 9127-L

At 1090 Mc, tuneable ±25 Mc, available from 900—1200 Mc.

TRAK Type 2958

YES

ally

two of

ata-

ched

irely ems.

high logic

apid

sys-

com-

are new

cked

com-Data

)ata

ents

full

o de-

ement

LS

MASS

TRAK Type 2959

TRAK Type 9127-SL At 2 KMc, tuneable ±100 Mc, available from 800—7000 Mc.

TRAK Type 9127-S

Available in 3 segments of S-Band: 2700—3000 Mc, 3000—3300 Mc, 3300—3600 Mc.

TRAK Type C-3136 Tuneable 2700-3400 Mc.

TRAK Type 9127-C Tuneable 5400-5900 Mc.

ALSO, OSCILLATORS ENGINEERED to your specifications!

We invite you to write for new TRAK MICROWAVE CAVITY BULLETIN.

Cavity oscillator ENGINEERS WANTED.

TRAK

TRAK MICROWAVE CORPORATION

Subsidiary of TRAK Electronics Company

5006 N. Coolidge Avenue Tampa 3, Florida REdwood 6-6422

CIRCLE 25 ON READER-SERVICE CARD ESIGN November-December, 1960

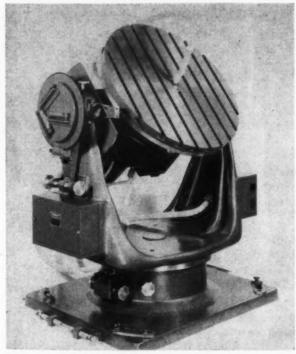


FIG. 5. SERVO MOTOR driven table, Model 066, using precision gear drive can be used for simultaneous rate mode testing of a number of gyro units or for servo mode testing of a single unit or system.

tachments have been provided on this type of table.

Servo tables using conventional servo motor drives with precision spur gearing are also used. Fig. 5 shows such a unit which provides both servo and rate modes of operation, and which can therefore be used for simultaneous rate mode testing of a number of gyro units, or for servo mode testing of a single unit or system.

FOR MORE INFORMATION CIRCLE 104 ON READER-SERVICE CARD

#### **BOOK REVIEWS**

ELECTROMAGNETIC ENERGY TRANSMISSION AND RADIATION, by Richard B. Adler, Lan Jen Chu and Robert M. Fano (1960) John Wiley & Sons, Inc., 440 Fourth Ave., New York 16, N. Y., 621 p., 6" x9", \$14.50. M.I.T. "Core Curriculum" text treating electromagnetic waves in one, two and three space dimen-

FOR MORE INFORMATION CIRCLE 105 ON READER-SERVICE CARD

COUPLED MODE AND PARAMETRIC ELEC-TRONICS, by William H. Louisell, (1960), John Wiley & Sons, Inc., 440 Park Ave. South, New York 16, N. Y. 268 p., 6" x 9", \$11.50. Theory of coupled modes is applied to TWT, backward wave tubes and parametric

FOR MORE INFORMATION CIRCLE 106 ON READER-SERVICE CARD

CIRCUIT THEORY OF LINEAR NOISY NET-WORKS, by Hermann A. Haus and Richard B. Adler, (1959), Technology Press of MIT and John Wiley & Sons, 440 Fourth Ave., New York 16, N. Y., 79 p., \$4.50. Rational approach to characterization of amplifier spot-noise performance and noise-performance

FOR MORE INFORMATION CIRCLE 107 ON READER-SERVICE CARD

## LET'S PLUG

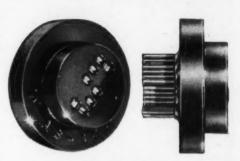
#### FOR BETTER TESTING WITH EECO'S TEST SOCK

Now all header-terminal components automatically become plug-in devices for test and evaluation, when you test solder-terminal relays, transformers, crystal cans, etc., with the new EECo universal test socket series.

Dual, isolated contacts for each terminal on header eliminates solder joints or clip leads.

Many standard configurations available, immediate delivery. New techniques make special sockets available at standard socket prices.

**Automation Division** 



**AS-Series Test Seckets** 



EECo RT-905 RELAY TESTER for faster, more accurate testing. Measures voltage and current simultaneously, both pull-in and drop-out time, contact bounce. Automatic relay driving circuitry. Oscilloscope connections and circuitry.

SEND FOR DATA SHEETS AS-101 AND RT-905.



Electronic Engineering Company of California 1601 East Chestnut Avenue . Santa Ana, Calif. . Kimberly 7-5501 . TWX: S Ana 5263

CIRCLE 24 ON READER-SERVICE CARD

EE 0-13



Repetitive symbols . . . in fact any drafting, blueprint or specification detail items . . . can be applied in seconds, rather than drawn in hours. If your engineers or draftsmen haven't yet discovered the speed and economy of STANPAT, they are wasting valuable hours . . . and valuable money.

STANPAT tri-acetate sheets are quickly and easily adhered to your tracings without special equipment. Reproductions are crisp and clean . . . Won't dry out, come off or wrinkle. Mail the coupon today and see for yourself.



CIRCLE 27 ON READER-SERVICE CARD

## Processing & Updating Magnetic Tape Files

J. C. HAMMERTON\*

This analysis evaluates the effectiveness of four systems for maintaining magnetic tape files in relation to (1) the activity of the files, and (2) the efficiency of using magnetic tape.

ILE MAINTENANCE is a problem common to all business systems and many instrumentation systems. In general terms, the problem is to modify existing records in accordance with new data received. Conventional procedures involve the location of the relevant records in a filing cabinet, modification of the record by manual entry, and re-insertion of the record in its right place in the filing cabinet.

When the basic records are stored in a reference file consisting of many reels of magnetic tape, the procedure is fundamentally the same. The existing records have to be located and altered in accordance with new data which has been consolidated on a separate transaction tape.

The new data may consist of additions, modifications and deletions. For example, the reference file of an insurance company may be changed by addition of a new policy, by recording the latest premium payment on a current policy, or by deletion of a matured policy.

If the number of unit records undergoing alteration at any one time is a large percentage of the total number of records in the file, the "activity" of the file is said to be high. Conversely if only a relatively few records are changed, the activity is low.

#### Tape Records

Customarily a unit record is recorded on magnetic tape with gaps of unrecorded tape separating it from the adjacent records. The gaps enable the tape-handling mechanism to stop the tape after one record has been read, and some time later to restart the tape and get it up to running speed before reaching the next record. The gaps, therefore, are necessary; they do, however, constitute a wastage of the storage medium. If the unit record is long (600-700 characters), the wastage is small; if short (35-70 characters), the wastage is significant. Tape utilization—i.e., the ratio of the length of recorded tape to the total length of tape, is included in the analysis as a parameter.

#### **Updating Techniques**

There are many different methods of updating magnetic tape files. Five methods are described in this section and four are analyzed.

#### System I-Computer ("read" after "write")

The most elementary method of updating a reference file is to use a simple computer which can only perform one instruction at a time (Fig. 1).

The reference file and the transaction tape are connected to input trunks of the computer. In both of them, the records are ordered by the same identifying criterion—e.g., policy number.

Having lodged the first transaction in the computer, the records on the reference tape are read-in until a match is found.

In the case of a record which does not match a transaction record, the process time is equal to the read-in time  $(T_r)$  plus the time to compare the identifying criteria, thus ascertaining that no match exists, plus the write-out time  $(T_w)$ . For practical purposes this time is equal to  $(T_r + T_w)$ .

If a match is found, the process time is increased by the compute time (T<sub>c</sub>) necessary to produce an updated record.

After using the first transaction record to update an inventory record, the second transaction record is read in to the computer and the search of the reference file repeated.

The fundamental objection to this method is that, since file-searching is a relatively simple task for the computer, the computer is used uneconomically.

#### System 2—Computer ("read" while "writing")

One method of alleviating this problem is to use a computer which has the ability to read into and write out of its memory simultaneously. This feature enables the  $n^{th}$  record to be transcribed to the output tape while the  $(n+1)^{th}$  record is being read in.

Consequently the process time per record is equal to the read-in time (T<sub>r</sub>) if no match is found, and to the read-in time plus the compute time if a match is found.

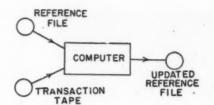


FIG. 1. SIMPLEST updating technique uses sequential read and write operations.

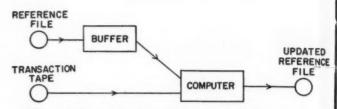


FIG. 2. USE of a buffer reduces read time.

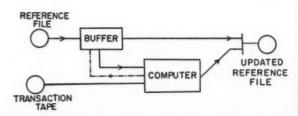


FIG. 3. BUFFER transfers record to computer only if a "match" is found.

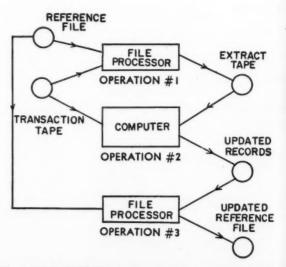


FIG. 4. FILE PROCESSOR technique prepares a tape holding only records that will be changed. Operation I is to prepare extract tape; operation 2 is to update active records; operation 3 is to replace old records by updated records.

MODE

<sup>\*</sup>Author was with Radio Corporation of America when article was written.



ntial

only if

ED

a tape

eration

update records Gears • Shafts • Differentials

Transmission • Speed Reducers & Gearheads



CIRCLE 28 ON READER-SERVICE CARD



Now—Automation Control You Can Depend On!

SCAMMIT STATIC-SWITCHING

MONITORING SYSTEMS



Self-Contained • Lower Cost
• Range of Models and Sizes

Get greater reliability for all kinds of process and automation control with SCAMMIT MONITORING SYSTEMS. Permanent components and static switching reduce operational failure. Investigate dependable, economical SCAMMIT before you invest in any monitoring system.

ODEL ST-EM SEND FOR complete information and literature.

COMPLETE MONITORING SYSTEMS FOR INDUSTRY

INSTRUMENT CORP.

Dept. H, 3101 N. Lowell Ave., Chicago 41, III. • Avenue 2-6930
REPRESENTATIVES IN ALL PRINCIPAL CITIES

CIRCLE 29 ON READER-SERVICE CARD

DESIGN November-December, 1960

#### System 3-Buffer Storage Device

The performance of a computer which does not have the ability to read while writing can be improved by the use of a buffer storage device (Fig. 2). Essentially this is an extension of the computer's memory with its own addressing matrix. Information can be transferred from buffer to computer or computer to buffer at a much higher rate than information is transferred to or from tapes. Typically the latter takes place at 30 kc/s while the transfers between memories can be effected at 300 kc/s.

One method of using a buffer storage device is to route all the reference records through it. The records are then available to the computer on demand. Immediately the  $n^{th}$  record has been transferred to the computer, the  $(n+1)^{th}$  record can be read in to the buffer storage and held until the computer has processed the  $n^{th}$  record. The transaction records are read into the computer directly since all the information contained in them is relevant to the updating operation.

If no match is found, the process time per record is equal to the read-in time plus the buffer-to-computer transfer time. (The time required to compare criteria is small.)

If a match is found, a further time must be added equal to the compute time plus the write-out time minus the read-in time (providing this quantity is positive).

An alternative method is to transfer a record from buffer to computer only if a match is found (Fig. 3). If no match occurs, the record is transferred directly to the output tape from the buffer while the next record is read in.

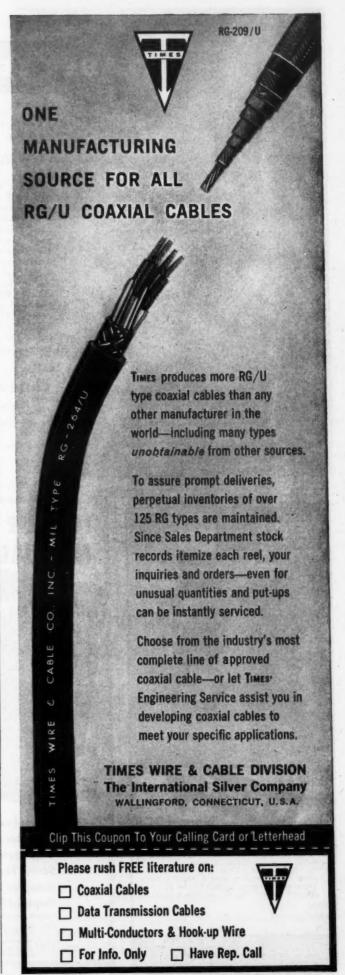
This method necessitates a buffer storage device which can (a) read while writing and (b) compare an identifying criterion in it with an identifying criterion in the computer.

#### System 4—File Processor and Computer

A different approach to the problem is found in the use of a special-purpose machine commonly referred to as a *file processor* (Fig. 4).

The purpose of this machine is two-fold. It extracts from the reference file copies of those records which have to be updated in accordance with the data consolidated on the transaction tape. Consequently, only active data are presented to the computer and the computer can complete its task in the minimum time. The second operation performed by the file processor is to return the updated records to the reference file in place of the out-of-date information.

The updating of the reference file is, therefore, accomplished in three basic operations (Fig. 4). However, if the updating operation is performed regularly and frequently, the first and third operations can be combined. For example, on a daily cycle the transaction tape resulting from Tuesday's work can be used to extract the relevant records from the reference file while the updated records from Monday's work are returned to the file. As the two operations are performed simultaneously, the total processing time is reduced.



CIRCLE 30 ON READER-SERVICE CARD



TABER TELEFLIGHT goes with the "BIRD"

## The PRESSURE TRANSDUCER that dissipates HEAT to its CASE to defeat zero gravity heat build-up

There is a whole family of Teledyne and Teleflight Pressure Transducers available for airborne or ground support application. Naturally, our star in the missile and rocket field is our tiny 9½ oz. Teleflight at the left. This Teleflight precisely measures liquid or gas pressures at 0.25% over a wide 0 to 2,000 PSIG or PSIA temperature range. Bonded strain gage construction assures low sensitivity to shock and vibration. When the Teleflight is subjected to zero gravity conditions (as in space flight where convection cooling is non-existent) the Ni-Span proving ring acts as a heat sink and conducts heat AWAY from the resistance gages to the instrument case. Handles corrosive media including fuming NITRIC ACID. With slight factory modifications, can also handle Fluorine. 200% overload protection built in at no extra cost. Infinite resolution, Linearity 0.25%, Hysteresis 0.25%, Temperature —150° to +275° F., Repeatability within 0.1%. Taber also produces a complete line of miniature transistor amplifiers or will build complete Electronic Systems to your specifications.

Write for Illustrated Literature

#### TABER INSTRUMENT CORPORATION

Where the Accent is on Accuracy & Reliability

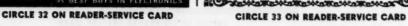
n 242 North Tongwanda, N. Y.

Telephone: NX 3-8900 ● TWX-TON 277

Taber

CIRCLE 31 ON READER-SERVICE CARD







CIRCLE 34 ON READER-SERVICE CARD

#### TERMINOLOGY

- Tr = read-in time from tape to computer, file processor or buffer
  - = Ts, time to start the tape and reach the first character; + time to transfer the record

25

bu

cu

tiv

tin

ed

file

a

ma

- = T<sub>s</sub> + h/v where h is the average length of a record in inches and v is the tape speed in inches/sec.
- = length of gap of blank tape between records in inches
- = fraction of a tape which stores useful data = h/(h + d)
- T<sub>c</sub> = time to perform the necessary computation on an active record
- Tw = time to transcribe a record to a tape from the computer, the file processor or the buffer storage device
- T<sub>bd</sub> = time to transfer a record from buffer to computer er computer to buffer = h/kv
- k = ratio of information handling rate in computer and buffer to information handling rate to and from tape.
- L = length of a reel of tape in inches
- N = number of records per reel of tape = L/(h + d)
- y = fraction of the records in the reference file which require servicing during a particular cycle of operation

The analysis which follows assumes that the file processor can simultaneously extract from and return to the reference file in this manner.

It further assumes that the machine is designed so that the time taken to process a reel of tape is approximately equal to the running time of the tape. In low-activity applications, this assumption is justified if the reference tapes are only stopped when a match occurs with either a record on the transaction tape or a record on the updated tape. By implication the file processor must be able to read, perform its limited computation and write simultaneously.

#### **Comparison of Processing Times**

In the following sections, the four systems described are analyzed with respect to processing time and machine cost.

The analysis is made with reference to two different operations. In one the records have an average length equal to the gaps of unrecorded tape between records (tape utilization factor x = 0.5). In the other, the records have an average length equal to nine times the length of the gap (x = 0.9).

The time to introduce the transaction records is excluded from the analysis because it affects all the systems equally with the exception of System #4. Since the latter is used only in low activity applications the exception is unimportant.

The method of analysis is valid for other systems but the results must be applied with caution if any of the typical values are altered.

#### System I-Computer ("read" after "write")

The processing time (T<sub>1</sub>) is the sum of the time to read and write the inactive records and the time to read, compute and write the active records.

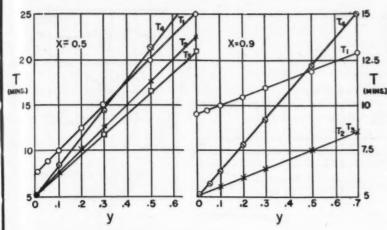
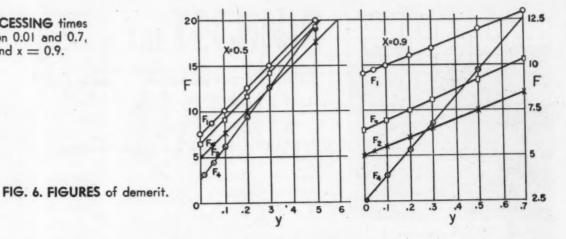


FIG. 5. PROCESSING times for y between 0.01 and 0.7, at x = 0.5 and x = 0.9.



$$T_1 = (T_r + T_w) N (1 - y) + (T_r + T_c + T_w) Ny$$
  
 $asN = L/(h + d)$   
 $T_1 = [(T_s + T_c y) (1 - x)/d + 2x/v]L$  (1)

#### System 2—Computer ("read" while "writing")

The processing time (T<sub>2</sub>) is the sum of the time to read the records plus the time to compute the active records. The write-out time is not included because the (n + 1) th record is read in while the nth record is written out.

$$T_2 = T_r N + T_c N y = [(T_s + T_c y) (1 - x)/d + x/v] L$$
 (2)

#### System 3-Buffer-Storage Device

aracter

ocord in

n inche h + d) n active

mputer,

puter o

d buffer

4)

hich re

eration

the file

return

gned so is ap-

e tape

s justi-

when a

asaction

lication

orm its

escribed

and ma-

different

e length

records

her, the

ne times

ds is ex

the sys 4. Since

tions the

systems

f any o

e time to

time to

The system described utilizes a buffer storage device between the reference file and computer. As soon as the nth record has been transferred to the computer from the buffer, the (n+1) th record is read into the buffer. The latter action, therefore, takes place concurrently with writing out the nth record, if it is inactive, or the computing and writing out, if it is active.

If no match is found, the read-in time governs the instruction time. If a match is found, the governing time is  $T_r$  or  $(T_w + T_c)$ , whichever is greater.

A time T<sub>bd</sub> is included for transferring the record from buffer to computer.

$$T_3 = (T_r + T_{bd}) N + (T_c + T_w - T_r) Ny$$
  
where  $T_c + T_w \ge T_r$ 

$$T_8 = \{T_s(1-y) + T_cy\}(1-x)/d + (1+1/k)(x/v)\}L$$
(3)

#### System 4—File Processor and Computer

The processing time (T<sub>4</sub>) consists of a time T<sub>a</sub> taken by the file processor to extract some active records from the reference file and return others to it, and a time T<sub>b</sub> taken by the computer to process the extracted active records.

Ta is assumed equal to the running time of the reference file. This assumption is true for an ideal file processor and valid for a file processor performing a low-activity operation. Because this assumption is made, the activity of the records handled by the file processor is irrelevant.

The computer in this example does not have the ability to read and write simultaneously.

$$T_a = L/v \tag{4}$$

$$T_b = (T_r + T_w + T_c) \text{ Ny}$$
  
=  $[(T_s + T_c) (1 - x)/d + 2x/v] \text{ Ly}$  (5)

$$T_{4} = T_{a} + T_{b}$$
 (6)

#### **Evaluation of Systems**

In order to evaluate the four systems, the following typical values for the system constants are used.

$$\begin{array}{l} T_s = 5 \text{ milliseconds} \\ d = 0.5 \text{ inches} \\ v = 100 \text{ inches/sec} \\ L = 30,000 \text{ inches} \\ k = 10 \end{array}$$

The value of T<sub>c</sub> depends on the operation being performed. It cannot readily be related to the average length of the record because the record may be padded with "copy" information which takes no part in the computation. As a representative figure, 50 milliseconds is used. If the average time per instruction is 100 microseconds, 50 milliseconds represent a program of approximately 500 instructions per active record which is quite modest.

Using these values, the processing times have been plotted in Fig. 5 for values of y between 0.01 and 0.7.

It will be seen that, time-wise, Systems 2 and 3 are approximately equivalent. Also that System 4 is only efficient at low values of y-i.e., in low-activity ap-

The times are longer for x = 0.5 than for x = 0.9because there are more records on the tape when x is low. Consequently more stopping and starting of the tape is involved.

#### Figure of Demerit

System cost must be taken into account to improve the comparison.

To do this, a figure of demerit (F) is used equal to the processing time (T) multiplied by the system cost expressed as a fraction of the cost (C) of the basic

Thus the figure for System 1 is numerically equal to the processing time  $T_1$ .

In practice the provision of the ability to "readwhile-writing" does not materially increase the cost of the computer so that the figure for System 2 is T<sub>2</sub>.

System 3 uses a buffer storage device of which the

cost can be expressed as Cm where m = 1/5, approximately, with existing techniques. The figure of demerit for system 3 is, therefore, T<sub>3</sub>(1+m) because both the buffer and the computer are used for

System 4 uses a file processor and a computer. The cost of the file processor can be expressed as \$Cn. It is assumed that a reasonable value for a design approaching the ideal is  $n = \frac{1}{2}$ . The file processor is in use for a time T<sub>a</sub> = L/v, and the computer for a time  $T_b$  where  $T_b = (T_4 - T_a)$ . Thus the figure of demerit for System 4 is  $T_a n + (T_4 - T_a)$ .

The values are plotted in Fig. 6.

#### Conclusions

The relative merits of the systems analyzed can be summarized as follows;

I. System 1, the basic computer, is the least efficient, as was expected.

II. System 4, the computer and file processor, is the best system on the time-cost basis when the file activity is less than 25%.

III. System 2, the computer with the "read-whilewriting" facility, is the best system on the time-cost basis when the file activity is greater than 25%.

IV. On the basis of time alone, System 2 is the best system no matter what the activity.

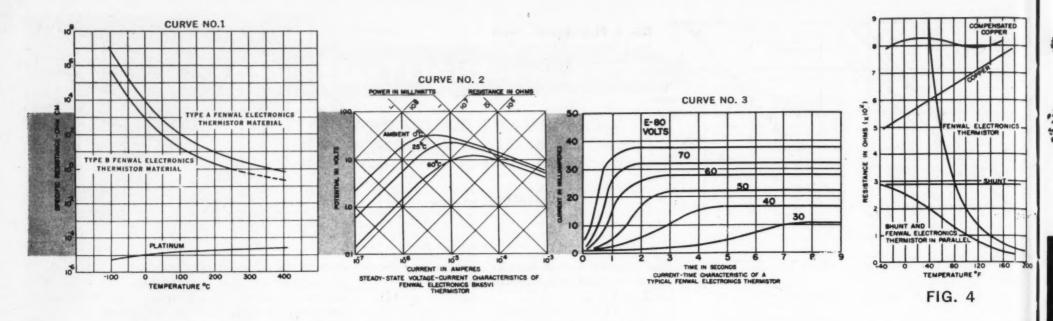
V. System 3 is only to be recommended as a method of improving the performance of a computer which lacks the ability to read-while-writing.

VI. These conclusions are valid for storage utilization factors of 50% and 90%. Consequently it is inferred that they are valid for all reasonable values of this parameter.

The conclusions stated above are based solely on consideration of time and cost. They do not reflect any thinking about the advantages which accrue in systems with only one type of major data-processing machine-namely easier maintenance, more flexible scheduling, and more uniform control methods.

#### Acknowledgments

The author wishes to thank the Radio Corporation of America for permission to publish this paper and to acknowledge the helpful criticism of his colleagues during its preparation.



The Thermistor—a Versatile Thermal Transducer

Thermistors are "thermal resistors" or resistors with a high negative temperature coefficient of resistance. As the temperature increases, the resistance goes down and as the temperature decreases, the resistance goes up. This is just opposite to the effect of temperature changes on metals. Thermistors are semi-conductors of ceramic material made by sintering mixtures of metallic oxides such as manganese, nickel, cobalt, copper, iron, and uranium.

Three important characteristics of thermistors that make them useful in electronic and electrical circuits are their resistance-temperature, voltage-current and current-time characteristics.

Resistance-Temperature Characteristic: The resistance of a thermistor as measured at very low power is solely a function of its absolute temperature. This resistance is called  $R_o$ , which means the resistance at essentially zero power.

The mathematical expression which relates the resistance and the absolute temperature of a thermistor is as follows.

$$R_o(T)/R_o(T_o) = \epsilon'(1/T - 1/T_o)$$

Where: R<sub>o</sub> (T) is the resistance at absolute temperature T.

 $R_o$  ( $T_o$ ) is the resistance at absolute temperature  $T_o$ .  $\epsilon$  is 2.718

 $\beta$  is a constant which depends on the material used to make the thermistor (approximately 4000). The temperature characteristic  $\alpha$  of the thermistor is approximately equal to  $-\beta/T^2$  at any absolute temperature T.

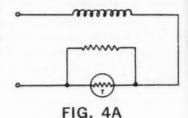
Fig. 1 shows the resistance variation of two basic Fenwal Electronics thermistor materials with temperature, and also shows the resistance variation of platinum for comparison. Between the temperature of —100°C and 400°C., there is a change of ten million to one in resistance of thermistor materials whereas platinum changes by only ten to one over the same temperature range.

Voltage-Current Characteristic: If a very small voltage is applied to a thermistor, a small current will flow which does not produce enough heat in the thermistor to heat it measurably above its surroundings. Under these circumstances, Ohm's Law will be followed and the current will be proportional to the applied voltage. However, if the voltage is gradually increased, the current will increase, and the heat generated in the thermistor will finally begin to raise its temperature above that of its surroundings. The resistance will consequently be lowered and more current will flow than if the resistance had remained constant (Fig. 2). In the latter portion of the curve, the thermistor is exhibiting a negative resistance characteristic. Under normal operating conditions the temperature may rise 200° or 300°C and the resistance may be lowered to 1/1000 of its value at low current.

Current-Time Characteristics: If a voltage is applied to a thermistor and resistor in series, a current will be determined by the voltage and the total circuit resistance. If the voltage is high enough, some heat will be generated in the thermistor which will lower its resistance and more current will flow. This, in turn, will heat the thermistor still more and lower its resistance still further. This process will continue until the thermistor reaches the maximum temperature possible for the amount of power available in the circuit, at which time a steady state will exist.

Since the thermistor has a certain mass, it takes time for it to be heated to its maximum value and this time is a function of the mass of the thermistor, the

FIG. 4. COPPER temperature characteristic in meter coil (4A) is corrected by shunted thermistor.



tr

cy

aı

to

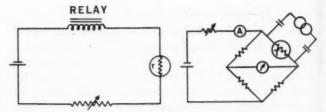


FIG. 5. TEMPERATURE FIG. 6. POWER meas-Control Circuit. FIG. 6. POWER measurement for RF energy.

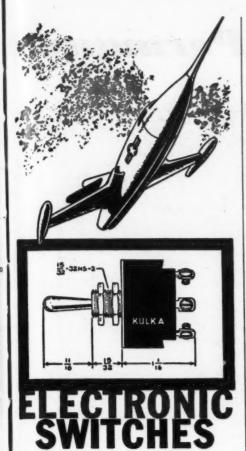
value of the series resistance and the applied voltage.

Fig. 3 shows that the time delay for the circuit to reach maximum current for a given thermistor is a function of the applied voltage. By suitable choice of thermistor and associated circuitry, it is possible to produce time delays from 0.001 seconds to several hours.

#### How Thermistors Are Used

The number of successful thermistor applications is growing rapidly and the future use of thermistors appears to be limited only by the imagination and enterprise of skilled engineers. Three typical applications are suggested below:

Temperature Compensation: Most circuit elements have a positive temperature coefficient of resistance such as the copper wire in a meter coil (Fig. 4). A thermistor may be used to compensate such a coil so the meter resistance is substantially constant over a wide temperature range. The thermistor is shunted by a resistor so that resultant negative temperature co-



made to Joint Army and Navy specs

Tiny yet sturdy. Long trouble-free service. Operating cycles above minimum required by specs. Available in SPST, SPDT, DPST and DPDT. DC and AC up to 1600 cycles. Made to JAN-S-23, MIL-S-6745, MIL-S-21195 and MIL-S-3950A.

All parts treated against corrosion. Units come with mounting nuts and sleeve lockwasher. AN switches supplied with toggle seal.

#### ASK FOR DATA ...

neas-

ergy.

ltage.

it to

is a

hoice

ssible

everal

ations

istors

n and

plica-

ments

stance

4). A

coil so

over a

ted by

re co-

DESIGN

Latest catalog on switches, miniature power outlets, lamp sockets, harness assemblies, etc., sent on request.

Complete the wiring with



CIRCLE 35 ON READER-SERVICE CARD November-December, 1960

efficient of resistance is equal to the positive coefficient

Temperature Control: A sensitive temperature control may be made by placing a thermistor (Fig. 5) in one leg of a bridge circuit, a variable resistor in another leg, and a polarized relay across the output. When the thermistor becomes warm, the relay will operate in one direction and when the thermistor becomes cold, the relay will operate in the opposite direction. The point of operation may be adjusted by changing the value of the variable resistor.

A very sensitive control may be made by applying ac to the bridge and placing a high gain amplifier between the bridge and the relay. Such controls have operated to a precision of .001°F with ease.

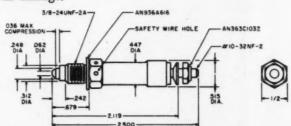
Power Measurement: If a bead thermistor of 2000 ohms is placed in a 200 ohm bridge circuit with a variable resistor in series with the bridge (Fig. 6) the current may be increased gradually until the thermistor heats up enough to lower its resistance to 200 ohm at which point the bridge will be in balance. This current may be measured and the dc power in the thermistor calculated. If a source of high frequency power is applied to the thermistor through suitable capacitors, it will be still further heated and the bridge will be unbalanced. The dc power may then be reduced until the bridge balances again and the new dc power calculated. The difference in the two dc power calculations will be the HF power. (From 20-page "Thermistor Manual". Fenwal Electronics, Inc., Framingham, Mass.)

FOR THIS LITERATURE CIRCLE 108 ON READER-SERVICE CARD

#### **Tip-Sensitive Heat Limit Switch**

New rugged, precision thermal switch for military and industrial applications called the "Tip-Stat," Type Q-1 (See Figure) is most effectively used where inner temperatures must be controlled. Typical applications include its use in aircraft generators where it signals a warning to actuate a control when the windings reach dangerously high temperatures.

When supported in a bearing housing with its tip pressed against the bearing race or shell, it signals any bearing overheat condition in time to prevent seri-



The switch is factory preset to actuate at any point from 20° to 550°F, employing a hermetically-sealed inner cartridge. The reaction time is less than 0.5 seconds and temperature differential is from 1° to 2°F. Repeatability of operation is within ±1°F. Contact rating is 11/2 ampere resistive or 1/2 ampere inductive, 115 v ac or 28 v dc. (From 8-page catalog, "CPI Bi-Metal Thermal Switches," Control Products, Inc., 280 Ridgedale Ave., East Hanover, N. J.)

FOR THIS LITERATURE CIRCLE 109 ON READER-SERVICE CARD

## THE TECHN **Precious Metals**

A pilot plant which offers laboratory controls under production conditions is available to industry without charge.



This unique facility is designed to solve plating problems or develop specialized plating methods . . . and may be used for investigating both still and barrel plating processes. The line may be operated by any

plater or engineer, by our own technical staff or by a team of both. It is designed to eliminate

difficulty, time, and expense in translating laboratory findings to practical production.

P.O. Box 965 Providence 1 R.I. • 7001 N.Clark St. Chicago 22 III.

STuart 1-6100 Plant: Cranston, R.I. CIRCLE 34 ON READER-SERVICE CARD



The IEE digital readout puts the digit right up front, visible from any angle. Vision is unimpaired by stacked characters and sharp, clear-white digits provide high-contrast, error-proof reading. Use of words, color, and multiple projections offer utmost versatility.

WRITE TODAY FOR COMPLETE SPECIFICATIONS

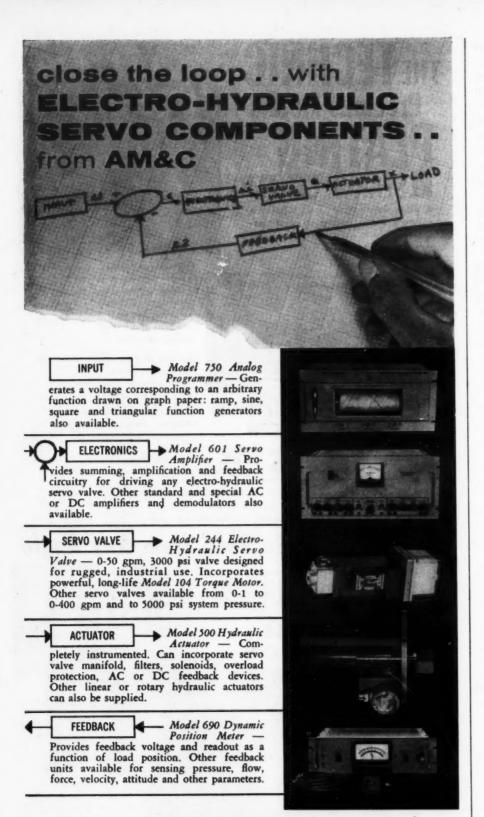
**Binary-To-Decimal** Decoders Available.

Principal Cities



INDUSTRIAL ELECTRONIC ENGINEERS, IN

CIRCLE 37 ON READER-SERVICE CARD



AM & C can provide all of the elements for successful servo control - from the engineering and production of unique electronic, electro-hydraulic and electro-mechanical components to complete integrated system "packages" to do a specific job. If your problem involves instrumentation or automatic control of position, speed, pressure, flow, or force, our engineers can assist you. Telephone or write:



AMERICAN MEASUREMENT & CONTROL, INC. Subsidiary of CompuDyne Corporation WALTHAM 54, MASSACHUSETTS TWinbrook 4-6212

CIRCLE 38 ON READER-SERVICE CARD

## Modern Permanen

form

magi

teria to be Th

ing i posit the 1 envir M size tions to m

nary

make Inhe

atom

are 1

magr magr

In

cerar

in m oxide

trica

netic air.

not mean Ge

but p

plica

in th the 1 energ orien

oz/cı

In

have

Alnic gauss Geno times

that

in cr to po er, b

speak

"Gua

netic Mich Reg

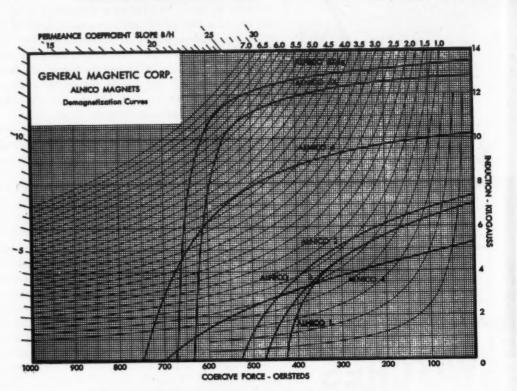


FIG. I. CHARACTERISTIC Demagnetization Curves, Alnico Magnets.

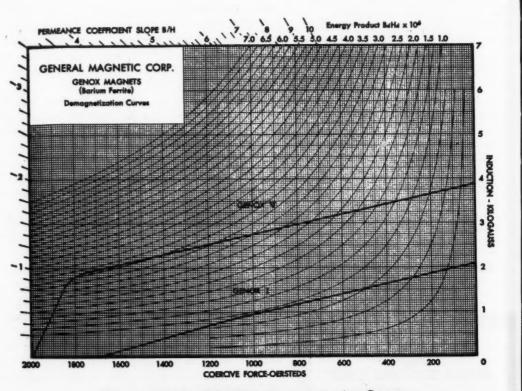


FIG. 2. CHARACTERISTIC Demagnetization Curves, Genox® Magnets.

## nMagnets

Modern permanent magnets of high-energy Alnico are now available in many convenient pre-machined forms. Today a one-inch Alnico block will have more magnetomotive force at its poles than a 6-inch bar of equal cross-section made from old chrome-steel materials, which were formerly bent into a horseshoe to bring its poles the same distance apart.

The length and cross section of a magnet materially affects the magnetic field it is capable of producing in any magnetic circuit. The metallurgical composition (Fig. 1) also is a vital factor in determining the magnetic properties and its characteristics under environmental stresses.

Magnetic alloys are cast into approximately the size and shape needed for stock and sample applications. After casting a melt of the appropriate alloy to meet the end-use specifications, the rough magnets are shot-blasted, tumbled and subjected to preliminary grinding to clean and size. Heat-treating then makes these metallic forms into powerful magnets. Inherent magnetic "domains," which are chains of atoms grouped to form the smallest magnetic unit, are made mobile by heat. When cooled in a strong magnetic field, these domains literally freeze in a magnetic state.

In addition to the metallic magnetic alloys, a new ceramic magnetic material, Genox®, is now available in many standard and sample shapes. Genox is an oxide material (barium ferrite), not a metal. Electrically it is an electrical insulator and has a magnetic permeability of approximately one, the same as air. Therefore, the parts which are magnetized do not affect the magnetic circuit leakage field. This means that salient poles are not usually required.

Genox is made in two grades, chemically similar but processed differently. Each has its individual applications (Fig. 2). Genox V is magnetically stressed in the preferred direction of magnetization during the manufacturing process resulting in a magnetic energy product about three times that of the unoriented Genox 1. Genox weighs approximately 2.8 oz/cu-in, while Alnico weighs about 4.23 oz/cu-in-

In comparison with Alnico V the Genox materials have a lower saturation and residual magnetization—Alnico V, approximately 12,000 gauss; Genox 1, 2,000 gauss; and Genox V, 4,000 gauss. Both Genox 1 and Genox V have a coercive force approximately three times that of Alnico V. These characteristics indicate that for any given application Genox will be larger in cross section than Alnico V but shorter from pole to pole. Total volume of Genox will usually be greater, but frequently at lower cost. Applications include: speaker magnets, alternators, tachometers, TWT focussing assemblies, etc. (From 50-page catalog, "Guaranteed Magnetic Components", General Magnetic Corporation, 10001 Erwin Ave., Detroit 34, Mich.)

Registered Copyright U. S. Pat. Off. by General Corporation.
FOR THIS LITERATURE CIRCLE 110 ON READER-SERVICE CARD

## HIGH RESOLUTION SPECTRUM ANALYZERS



#### **Analysis Problems**

Vibration • Distortion • Pulses • Noise

Probescope Sonic and Ultrasonic analyzers all have automatic optimum resolution circuitry. Guesswork has been taken out of spectrum analysis. One control sets the proper bandwidth and sweepwidth to give the best possible resolution... other features include...60 db dynamic range... linear and log amplitude scales... internal calibration markers.

SPECIFICATIONS
Frequency Range
Sweep Width
Sensitivity
Resolution

S\$-20 7 cps to 23 kc 50 cps to 6 kc 500 microvolts 14 cps

## SPECIFICATIONS Frequency Range Sweep Width Sensitivity Resolution

\$\$-100 13.5 cps to 110 kc 200 cps to 20 kc 500 microvolts 27 cps

SPECIFICATIONS
Frequency Range
Sweep Width
Sensitivity
Resolution

\$\$-500 75 cps to 600 kc 2 kc to 200 kc 250 microvolts 150 cps



#### **Synchronous Sweep Generator**

All Probescope analyzers feature 100 db dynamic range sweep generator attachments to visually display passband characteristics of amplifiers and filters. Noise and distortion which normally obscures response curves are eliminated.

Other spectrum analyzer models for subsonic, single sideband and telemetering analysis.

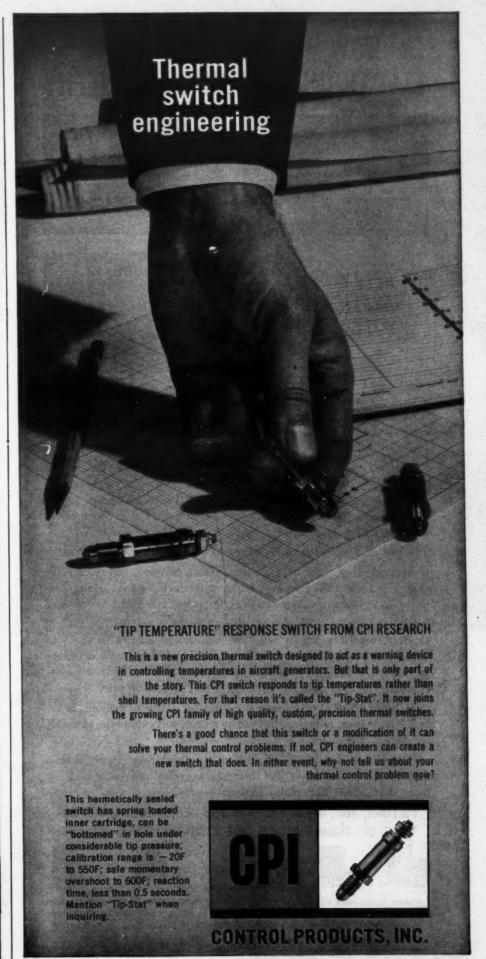
Write for more information



#### PROBESCOPE COMPANY INC.

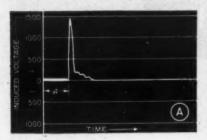
SAGAMORE HILL DR., MANORHAVEN, L.I., N.Y POrt Washington 7-8150

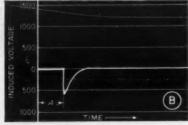
CIRCLE 39 ON READER-SERVICE CARD



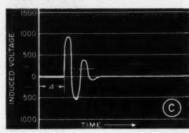
274 Ridgedale Ave., Hanever, H. J. CIRCLE 40 ON READER-SERVICE CARD

## HOW DO YOU RATE AS AN ELECTRONICS DESIGN ENGINEER?





#### RELAY APPLICATION QUIZ



CHANCES are that a circuit with more than one relay will use the contacts of one relay to energize the coil of a second relay. Which curve best represents the emf induced by interrupting the power to a standard subminiature 28-volt, d-c relay coil: A, B, or C?

When the current through a relay coil is interrupted, the emf induced opposes the change of current which caused it. The magnitude of the emf equals -L di/dt, and, since the time increment is practically instantaneous, the induced emf assumes very large proportions, often reaching values of 1200 to 1500 volts. The answer is A.

#### What does this mean in terms of relay circuit design?

It means that there isn't a subminiature or microminiature relay that can handle 1200 volts between open contacts without arcing. Arcing erodes contact surfaces and creates radio-interference problems.

Most contact erosion occurs during contact break. The rate of erosion correlates closely with the amount of energy in the load which is approximated by the relation  $W=\frac{1}{2}LI^2$  where W is energy in joules, L is the load inductance in henries, and I is the steady-state current. The L/R ratio has little effect on the erosion rate.

A life of 100,000 operations is a limit for contacts handling a 1.5 to 2.0-joule load; reducing the load by a third will extend the probable life by a factor of 10.

Filtors' has developed an efficient arc-inhibiting circuit that is sealed within the relay. The increase in relay reliability and life more than offsets the small additional cost.

FILTORS, INC., SPECIALISTS IN THE DESIGN AND MANUFACTURE OF SUBMINIATURE AND MICROMINIATURE RELAYS.











Makers of the most efficient microminiature relay motor in the industry—the powerful new Sensi-Terk rotary relay motor; used in the J-series relays, the "Pillbox" printed circuit relay, and in the first premium quality microminiature relay, the Golden G.

#### **FILTORS, INC. RELAYS**

PORT WASHINGTON/NEW YORK/POrt Washington 7-8220

CIRCLE 41 ON READER-SERVICE CARD



#### INERTIAL GUIDANCE TRANSDUCERS

#### GYRO TEST CONSOLE

A complete test console includes torque-to-balance feedback loop; magnetic suspension panel; compensation; dual photocell amplifiers; gyro wheel



supplies; frequency source; dual demodulator and servo amplifier required for MIT Type "D" gyro turntable, and for gyros developed at M.I.T. Full instrumentation and metering, and all power supplies are also included.—Northeastern Engineering, Inc., Manchester, N. H.

CIRCLE 119 ON READER-SERVICE CARD

#### **DUAL-CHANNEL AMPLIFIER**

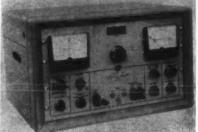
New dual-channel transistorized amplifier for compensated resolver applications features a parallel summation input circuit which can ac-



cept as many as five inputs per channel. Voltage transfer ratios can be maintained to an accuracy of 0.1% over the operating temperature range of — 55° to 105°C. Amplifiers operate at a signal frequency of 400 cps, provide output of 26 volts rms.—Components Marketing Div., Reeves Instrument Corp., Roosevelt Field, Garden City, N. Y.

CIRCLE 120 ON READER-SERVICE CARD

#### SERVO ANALYZERS



inp

plie

Clif

Sta

ters tion

fro

Unit

Type

gear

to g

0.01

inclu

Oper

ing.

strun dle E

Ne

el 97

into :

its lir

to +5

New Series 400 controls analyzers provide a self-contained signal generator, provide signals over frequency ranges up to 10,000 to 1. Three models cover frequency ranges of 0.3-20 cps, 0.003-30 cps, and 0.02-200 cps. Frequency and amplitude to ±2% of full scale accuracy.—Superior Manufacturing and Instrument Corp., 154-01 Barclay Ave., Flushing 55, N. Y.

CIRCLE 121 ON READER-SERVICE CARD

#### INERTIAL GYRO TEST



New data recording system, used with MIT Type D turntable supplies mean solar and sidereal time base to stability of 5 parts/108/wk and includes electronic digital voltmeter with printer readout; neon 6-digit timing unit; averaging unit and 11-digit printer recorder.—Northeasttern Engineering, Inc., Manchester, N. H.

CIRCLE 122 ON READER-SERVICE CARD

#### RATE GYRO

New dc rate sensor, including hermetically-sealed gyro, dc-ac inverter and signal pickoff, operates from a 28 v dc input. This is inverted to drive



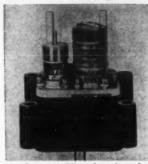
the gyro motor; also the output of the pick-off is demodulated, balanced, gain-adjusted and filtered, providing de outputs up to 12 volts. Resolution is below 0.05%, constant damping coefficient is within ±0.15% of nominal, linearity is within 1% of maximum rate, zero calibration is 0.01 to 0.02% of maximum rate, and life is 500 hrs min.—R. C. Allen Aircraft Instrument Div., 333 Commerce Ave., S. W., Grand Rapids, Mich.

CIRCLE 123 ON READER-SERVICE CARD

MILITARY SYSTEMS DESIGN

#### **POSITION TRANSDUCER**

New miniature position transducer for aircraft control converts shaft inputs up to 50° to a precise linear



genfreo 1. nges 0.02-

erior

orp.

cord-

with rntanean real pility 8/wk troneter dout; ming

unit

inter

east-

ster,

hererter

a 28

drive

of the

anced,

viding

lution

ng co-

nomi-

maxi-

.01 to

life is

rcraft

Ave.,

DESIGN

ARD

RD

output when a 28v dc signal is applied, and the clutch energized.— Clifton Precision Products Co., 5050 State Rd., Drexel Hill, Pa.

CIRCLE 124 ON READER-SERVICE CARD

#### SYNCHRO TRANSMITTERS

New Series PX-1 synchro transmitters supply linear or angular position information to a remote location from electro-mechanical devices.



Units consist of either one or two Type 23TX6 synchro transmitters geared to a shaft at different ratios to give maximum flexibility. System accuracies range from 0.05% to 0.01%.—Scientific-Atlanta, Inc., 2162 Piedmont Road, N. E., Atlanta 9, Georgia.

CIRCLE 125 ON READER-SERVICE CARD

#### SYNCHRO TESTER

New synchro tester measures major characteristics in MIL-S-20708A including electrical zero, electrical error, fundamental null and total null. Operation is semi-automatic with switch manipulation by rotary solenoids, and all outputs are direct reading, dc analog voltages.—Theta Instrument Corp., 520 Victor St., Saddle Brook, N. J.

CIRCLE 126 ON READER-SERVICE CARD

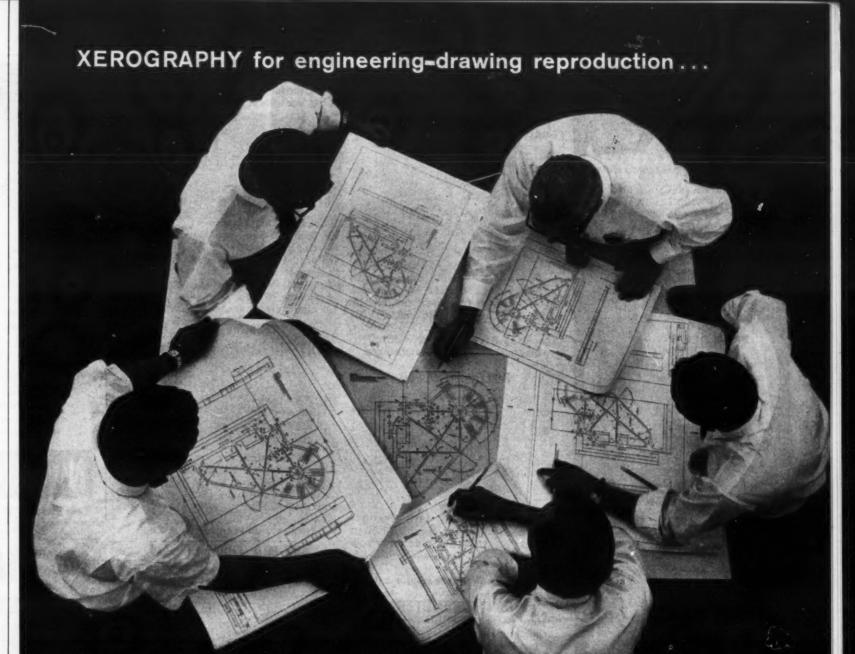
#### LINEAR TRANSFORMER

New size 8 linear transformer Model 9708-005 can deliver ½-w power into a 500-ohm load while retaining



its linearity of .33% over a range of ±30°. Has a 26-v, 400-cycle input, with phase shift control, capabilities to ±30'.—imc Magnetics Corp., 6058 Walker Ave., Maywood, Calif.

CIRCLE 127 ON READER-SERVICE CARD



## High-quality prints on ordinary paper... reduced or size-for-size...the fast, economical way

Clean, fast, dry, electrostatic . . . xerography has virtually revolutionized the reproduction of engineering drawings! Major industrial firms all over the country have discovered that Haloid Xerox copying equipment has more than met their every print-duplicating need . . . with reported annual savings from \$20,000 to \$500,000 over previous methods! There's no problem of capital investment, either . . . all XeroX® equipment is available at modest monthly rentals.

For high-quality offset paper masters:



XeroX® Model 1218 copying equipment combines with offset duplicating... and the results are spectacular! This equipment prepares sharp, in-

expensive paper masters from original drawings of A to D size. The larger drawings are perfectly reduced to 12" x 18" masters, from

which multiple prints can be run off in seconds!

Volume reproduction from original drawings or roll microfilm: Just push a button



on the XeroX Copyflo® continuous printer for sharp, dry, ready-to-use prints (on ordinary paper vellum, or offset paper masters up to 11" wide). Prints are made at the

rate of 20' a minute. Copyflo printers enlarge from roll microfilm (16 or 35mm), reduce, or copy size-to-size from original drawings.

Reproduction from card-mounted microfilm: The XeroX Copyflo 24C continuous printer and the exciting new Copyflo 1824 printer automatically produce dry, positive prints on ordinary paper, vellum, or offset paper masters from 35mm card-mounted



microfilm! The Copyflo 24C produces ready-touse prints (up to 24" x 36") at the rate of 20 linear feet a minute! The new low-cost Copy-

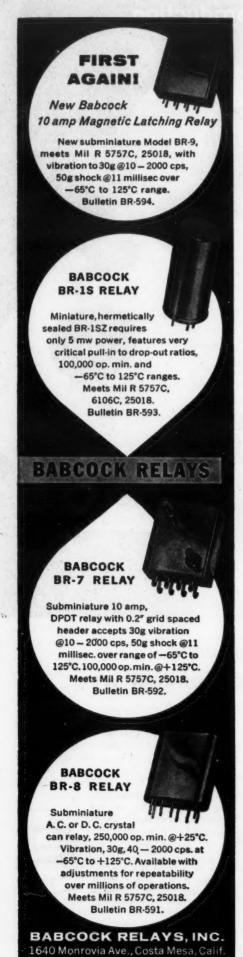
flc 1824 printer for small-volume users or large, decentralized users, produces prints from 8½" x 11" to 18" x 24".

GET ALL THE FACTS! Send for EDX Booklet today. Write: HALOID XEROX INC., 60-203X Haloid St., Rochester 3, N.Y. Branch offices in principal U.S. and Canadian cities. Overseas: Rank-Xerox Ltd.,



HALOID XEROX

CIRCLE 42 ON READER-SERVICE CARD



CIRCLE 43 ON READER-SERVICE CARD

#### **TRANSDUCERS**

#### ALTITUDE CONTROL TRANSDUCER

New economical Model 571 altitude control transducer can be used in ex-



pendable target drones or in tactical missile and aircraft applications. Specifications: functional range, ±0.5 psi; operating range to 80,000 ft.; dynamic error band, ±2%;.—Bourns, Inc., 6135 Ave., Riverside, Calif.

CIRCLE 128 ON READER-SERVICE CARD

#### POTENTIOMETER



New Megohm (PM) series features Resistance Range—1 Meg to 10 Megs ±5%; Linearity—1% std; 0.5% special.—Accuracy, Inc., 4 Gordon St., Waltham 54, Mass.

CIRCLE 129 ON READER-SERVICE CARD

#### DC TACHOMETER

New Model SS-779E-1 Size 8 dc tachometer has output of 3 v/1000



rpm with linearity of 0.1%, and ripple not over 3% of dc output.—Servo-Tek Products Co., 1086 Goffle Rd., Hawthorne, N. J.

CIRCLE 130 ON READER-SERVICE CARD

#### TIMER MOTOR TACHOMETER



New %" diameter Type 9001-00 permanent magnet motor withstands over 500 G shock; negligible speed variation from -67° to 167° F results from dry lubrication. Gear ratios range from 6:1 to 46,656:1, with peak loads to 500 oz-in.—John Oster Mfg. Co., Avionic Div., Racine, Wis.

CIRCLE 131 ON READER-SERVICE CARD

#### PRECISION PRESSURE SWITCH

New Model 400100 precision pressure switch for absolute, differential or gage pressure has accuracy of



½% and is available in any pressure setting from 0.2 to 250 psi. Wide band of adjustment is provided for a given nominal switch pressure.—Wallace O. Leonard, Inc., 373 S. Fair Oaks Ave., Pasadena, Calif.

CIRCLE 132 ON READER-SERVICE CARD

#### TRIMMER POT



New subminiature trimmer potentiometer Model 540 features 2-watt ratings, operation to 200°C, and humidity-proofing.—Handley, Inc., 12960 Panama St., Los Angeles 66, Calif.

CIRCLE 133 ON READER-SERVICE CARD

#### SUB-MIN TRIMMER POT

New general purpose trimmer potentiometer in resistances from 10

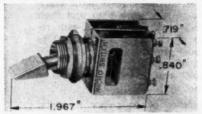


through 100,000 ohms ± 10% are available with insulated wire leads, solder lugs or end-mounted printed circuit pins.—Atohm Electronics, 7648 San Fernando Rd., Sun Valley, Calif.

CIRCLE 134 ON READER-SERVICE CARD

#### INDICATING TOGGLES

Bright aluminum tabs provide instant position indication with new compact toggle switches, each of



which provides two isolated SPDT circuits UL listed at 5 amp, 125 or 250 v. Dry circuit switches also available.—Micro Switch Div., Minneapolis-Honeywell Regulator Co., Freeport, Ill.

CIRCLE 135 ON READER-SERVICE CARD





With t

trial S

shaped

or flan

#### VOL-O-FLO

#### gas flow meters meet all the requirements for laboratory and field test use!

1. Highest possible accuracy is assured by the use of laminar flow elements.
2. Linear scale, accurate down to zero flow, provides good readability.

3. 19 full scale ranges from .001 to

200 SCFM are available.

4. Rugged all metal flow elements provide the reliability necessary to efficient metering.

Gauges protected against excessive pressure and flow.

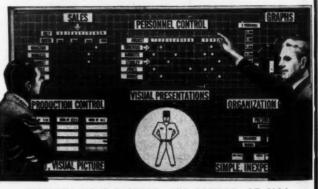
Special meters for exacting requirements: High pressure models, extended range models, super-accuracy models.

### NATIONAL NSTRUMENT ABORATORIES, INC

828 EVARTS ST. N.E. . WASHINGTON 18, D. C.

CIRCLE 44 ON READER-SERVICE CARD

### VISUAL MAGNETIC CONTROL



#### MAGNETS MOVE FASTEST—AND EASIEST—OF ALL!

SIMPLEST VISUAL SYSTEM FOR

Production Personnel

Sales Maintenance

Scheduling

Machine Loading
Charts—Graphs

Visual Presentations

MAGNETIC ELEMENTS

show facts instantly
organize for action
eliminate mistakes
get the jeb done

PRICED FROM \$38 INCLUDING MAGNETIC ELEMENTS PRICE LIST & BROCHURE MSD-II only

made

erand

sign

cation

WI

FREE

ON REQUE

REPRESENTATION DESIRED IN SOME AREAS

#### Methods Research Corp.

105 Willow Ave., Staten Island 5, New York
CIRCLE 45 ON READER-SERVICE CARD

MILITARY SYSTEMS DESIGN Nove

# PPHIRE

VERSATILE, ECONOMICAL MATERIAL WITH OUTSTANDING ENGINEERING ADVANTAGES

- . MELTING POINT-2040 C . POROSITY-0%
- . HARDNESS-Moh 9 . LOW DIELECTRIC LOSS
- . HIGH CHEMICAL RESISTANCE . TRANSPARENT

With the highly specialized facilities of the Industrial Sapphire Company synthetic sapphire can be shaped to nearly any desired form, and mechanically

d

e

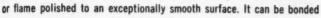
D. C.

LI

.....

EQUEST

orp.







COMPLETE FACILITIES FOR FABRICATING ALL HARD MATERIALS TO YOUR EXACT REQUIREMENTS

P. O. BOX 422M, QUAKERTOWN, PA. Phone: KE 6-3500

CIRCLE 46 ON READER-SERVICE CARD

Don't pay for **Precision** you don't need

**RMB Filmoseal Bearings** available in low-cost ABEC-1 as well as ABEC-5 and 7 tolerances.

Big news in the miniature bearing field! RMB's famous Filmoseal Bearings-the only sealed miniature bearings—are now made to low-cost ABEC-1 as well as ABEC-5 and 7 tolerances. This means designers can use these advanced design bearings even in those slightly less demanding applications where cost is a primary consideration. Designers can take advantage of such features as:

1. Stainless-steel construction throughout.

Lubricant retention at high temperatures.

3. Non-contaminating at all times. 4. Two-piece ball separators for high speeds.

Open radial Conrad-type bearings are also available in this new grade. A wide range of sizes is available from h" (0.1875") to ½" (.5000") OD including many metric

Write for your copy of the new RMB Miniature Bearings Catalog which gives full details on these as well as the entire line of quality RMB Bearings. Ask for Bulle-

# LANDIS & GYR, INC.

45 West 45th Street, New York 36, New York

CIRCLE 47 ON READER-SERVICE CARD

ESIGN November-December, 1960

# POT TAPS RE-SETTABLE

New 2" diameter Protractatap precision potentiometer provides up to 8 re-settable taps which can be adjusted by eye without tools to 1/2° ac-



curacy. Initial accuracy is maintained over wide ranges of temperature, humidity vibration and other critical factors .- Accuracy, Inc., 4 Gordon St., Waltham 54, Mass.

CIRCLE 136 ON READER-SERVICE CARD

# **MULTIGANG POTS**

New precision wire-wound 1/2" pots in multigang configurations up to six gangs, servo or bushing mounted, are supplied with choice of ball or jewel bearings. Standard linearity is 0.3%



in standard resistances from 100 ohms to 250K ohms; power ratings are up to 2.5 watts at 65°C and max operating temperature is 150°C .-ACE Electronics Associates, Inc., 99 Dover St., Somerville, Mass.

CIRCLE 137 ON READER-SERVICE CARD

## INERTIAL SWITCH

New miniature inertia switch Model 6UO-200 is preset to respond to ac-



celeration forces up to 250 G within a tolerance of ±15% of setting, operating range of  $-65^{\circ}$  to  $+200^{\circ}$ F. It has only one moving part, a precision-ground steel ball held against a solid base by a uniform magnetic field. When the opposing force of acceleration exceeds the magnetic force, the ball moves to close a normally open electrical contact .- Inertia Switch, Inc., 311 W. 43rd St., New York 36, N. Y.

CIRCLE 138 ON READER-SERVICE CARD

# CONTINUOUS ROTATION POT

New 360° continuous rotation composition variable resistor, series

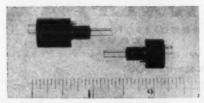


CR45, increases effective rotation from approximately 270° to 330°, makes exact resistance adjustments easier. Resistance range is 250 ohms through 10 megohms with linear resistance gradient. Rating is ¼ to ½ watt depending on resistance.—CTS Corp., Elkhart, Ind.

CIRCLE 139 ON READER-SERVICE CARD

# MINIATURE POTS

New miniature single-turn potentiometers feature rugged construction, small size and light weight for trimming, control and servo applications.



Model 140 bushing mount is 0.3" long, weighs 0.1 ounce with a standard resistance range from 50 ohms to 10 kohms, standard resistance range from 20 to 70 kohms.—Spectrol Electronics Corp., 1704 South Del Mar Ave., San Gabriel, Calif.

CIRCLE 140 ON READER-SERVICE CARD

# THERMAL SHOCK CHAMBERS

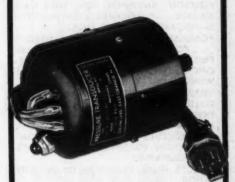
New Portable Temperature Test Chamber with ultra-rapid cycling completes a hot-cold cycle from -100°F to 500°F in slightly less than



10 minutes. Window drawer, access ports for test and operational wiring, liquid CO2 cooling and automatically programmed test cycle conserve test engineer's time. 10" x 7" x 7" test volume weighs under 50 lbs for portability.-Delta Design, Inc., 7460 Girard Ave., La Jolla, Calif.

CIRCLE 141 ON READER-SERVICE CARD

# SEA WATER DEPTH **PRESSURE TRANSDUCERS**



SONAR, SUBMARINE. AND TORPEDO APPLICATIONS

- Input: sea water pressure
- Output: volts, a-c or d-c
- Hermetically sealed case
- Patented angle-wipe potentiometer
- 1000-hour service life

Ranges: 0-50 to 0-7500 feet

regarding your transducer requirements.

364 Glenwood Avenue East Orange, New Jersey

CIRCLE 48 ON READER-SERVICE CARD

# TAKE A CLOSER LOOK

Discover the advantages
of the new
TRU-LOK
aluminum
self-locking nut

- MEETS ALL PERFORMANCE REQUIREMENTS OF MIL-N-25027 (160,000) PSI TO 550°F.
- CAN BE REUSED EXTENSIVELY WITH THE ABSOLUTE ELASTIC MEMORY OF A STAIN-LESS STEEL SPRING.
- MAINTAINS CONSTANT VIBRATION-PROOF POSITION ANYWHERE ON THE MALE MEMBER . . . LOCKING CONSTRUCTION IS INBOARD FROM THE ENDS.
- POSSESSES SMOOTH UNVARYING TORQUE

   POSITIVE, ACCURATELY CONTROLLED

   PRESSURES ARE FORMED INTO THE SPECIFIC CONFIGURATION OF THE MIDDLE WINDING.
- VIRTUALLY ELIMINATES WEAR, SEIZURE, GALLING OR DEFORMATION OF MATING THREADS . . . MAKING TORQUE MEASURE-MENT A MORE MEANINGFUL PARAMETER AND REDUCING THE POSSIBILITY OF CON-TAMINATION TO SENSITIVE INSTRUMENTS AND EQUIPMENT.
- · EFFECTS HIGH STRENGTH-TO-WEIGHT



\* Palent Nos. 2363662 and 2363663

Write for your copy of Bulletin #3002 and #3003

# WALTHAM

PRECISION INSTRUMENT

Waltham 54, Massachusetts

CIRCLE 49 ON READER-SERVICE CARD

# NEW MINIATURIZED DELAY LINES ARE ELECTRICALLY VARIABLE

Now you can achieve continuous delay variations electrically. Particularly suited to defense applications, these General Electric Delay Lines provide total delays up to 12 microseconds (depending on frequency) and a variability range up to 50%. With special delay lines for carrier or pulse type applications at frequencies to 30 megacycles, the electrical variation of delay provides a new method for solution of problems in:

- transmission time control
- pulse control and shaping
- high frequency phase control
- pulse position modulation
- phase or frequency modulation

Highly adaptable to transistorized circuitry . . . able to withstand extreme humidity, shock, vibration . . . tailored to customers' needs in radar, computers and communications.

For complete specifications write to: Defense Industries Programs Section 227-30 E



DEFENSE ELECTRONICS DIVISION
HEAVY MILITARY ELECTRONICS DEPT., SYRACUSE, NEW YORK
CIRCLE 50 ON READER-SERVICE CARD

# TRANSISTOR BETA TESTER

New Model 200 Transistor Tester measures Beta (HFE) directly on calibrated scale to accuracy of 1% at



different collector current reference levels. Accommodates PNP, NPN transistors, also power transistors, germanium diodes, selenium and silicon rectifiers.—Westmore, Inc., Fanwood, N. J.

CIRCLE 142 ON READER-SERVICE CARD

# MIXER DIODE

First commercially available gallium arsenide microwave mixer diode, IN3096R, is specified for 24,000 mc



(K-band) first-detector operation and is housed in a coaxial package identical to that used for existing silicon K-band diodes. Gallium arsenide diode exhibits an over-all noise figure of 10.5 db, surpassing the lowest noise figure available for any K-band crystal.—Philco Corp., Lansdale Div., Lansdale, Pa.

CIRCLE 143 ON READER-SERVICE CARD

# LOW-LOSS TUBE SOCKETS

New series Chemlec 7- and 9-pin miniature tube sockets designed for high frequency service where low loss-



factor and low dielectric constants are required, use FEP Teflon or CTFE (chlorotrifluorethylene), both withstanding high frequency, high temperature and high voltages. Meet or exceed all JAN specs.—Garlock Electronic Products, Garlock Inc., Canden 1, N. J.

CIRCLE 144 ON READER-SERVICE CARD

# Digital Variable Increment Computer Solves Weapon Systems Problems

GEVIC, General Electric's Variable Increment Computer, a new concept in digital computers, provides a unique combination of rapid slew, high iteration rate, and digital precision in applications formerly restricted to analog methods of computation. GEVIC is a multi-purpose stored-program digital computer employing all solid-state logic elements and circuitry.

gran

can

tiplic

and

are

gram

ΔV.

**GEV** 

drift

good

eithe

prog

Ligh

trol .

City,

Ne

ters,

0.50" sistar

numb

sistan

phrey

"RP3

Mode

lowin

(2) r

in 0.]

(5) n

For

rectili

x 9.8

9.8",

l oz

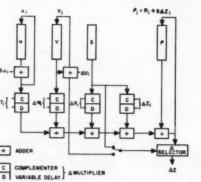
and w

on all

eter is

St., S

GEVIC's ability to operate in real-time on continuously changing data permits the computer to be incorporated directly into multiple highspeed servo loops. Designed for high-performance weapon control, guidance, and navigation systems, GEVIC is particularly suited to those digital applications where small size, light-weight, and extreme reliability are additional factors affecting the choice of computing techniques.



COMPUTER block diagram is diagrammatic restatement of basic algorithm (see next page).

# The Variable Increment Concept

The variable increment concept overcomes the two limitations of the fixed increment computer—slewing and rate limiting—without the expense of a multiple arithmetic section or without requiring excessively high clock frequencies:

(1) The incremental or decremental change of each variable is approximated by zero or by the closest allowed integral power of radix two (0, ±1, ±2, ±4, ... etc.).

These increments are easily stored and transferred as sign plus binary coded exponent (e.g.,  $+0.101 = +2^5 = +32$ ).

Multiplication of a binary coded number by an increment becomes the simple process of delaying the multiplicand by a number of digit positions equal to the power of the multiplier.

(Just as in the decimal system 19 × 10<sup>2</sup> = 1900).
 GEVIC usually mechanizes a more general algorithm than the integrator of the DDA. While the GEVIC concept is applicable to either differential or algebraic mathematics, the latter is usually preferred because of its ease of use and high pro-

MILITARY SYSTEMS DESIGN

24

gram efficiency (about 2 or 3:1 over the single integrator DDA).

# Basic Algorithm

t

Comles a

rate,

re-

IC is

tinu-

e in-

servo

con-

par-

where

uting

re-

e two

ewing

ultiple

sively

each

closest

, ±2,

trans-

(e.g.,

by an

delay-

posi-

1900).

algo-

ile the

fferen-

usually

h pro-

DESIGN

 $S\Delta Z_i + R_i = \rho_{i-1} - S\Delta Z_{i-1} + U_i\Delta T_i + V_{i-1}\Delta W_i + S\Delta X_i$ 

The computer block diagram (see figure) is a diagrammatic statement of this algorithm. This algorithm can be modified to provide addition-subtraction, multiplication, division, integration, exponential filtering, and differentiation and filtering. These modifications are developed from the basic algorithm by programmed-addressing of the proper variables ( $\Delta U$ ,  $\Delta T$ ,  $\Delta V$ ,  $\Delta W$ ,  $\Delta X$ ,  $\Delta Z$ ). All arithmetic operations solved in GEVIC are exact. No approximations are used and no drift is possible. The integrative operations are as good as is possible for their configuration. (e.g., either retangular or trapezoidal integration may be programmed). (From new 8-page brochure, GEVIC ... A New Concept in Incremental Digital Computers, Light Military Electronics Dept., Armament & Control Section, General Electric, 600 Main St., Johnson City, N. Y.)

FOR THIS LITERATURE CIRCLE 145 ON READER-SERVICE CARD

# New Linear Pots are Standardized

New Humphrey Standard Rectilinear Potentiometers, available in mechanical travels ranging from 0.50" to 9.90" in 0.10" increments, and in total resistance ranges from 100 ohms/in to 20,000 ohms/in, are accurately described under a standardized stock number system.



STANDARDIZED designations describe New Humphrey Rectilinear Pots.

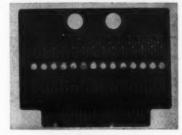
When the designer has picked the stroke and resistance he requires, he specifies the standard Humphrey model number as follows: First, he writes "RP38-" which stands for Rectilinear Potentiometer Model No. 38 Series. The next five digits have the following meaning: (1) Resistance/inch in 10K-ohms, (2) resistance/inch in K-ohms, (3) resistance/inch in 0.1K-ohms, (4) mechanical travel in inches, and (5) mechanical travel in 0.10".

For example, RP38-16598 would be a RP 38 series rectilinear potentiometer with a resistance of 16,500 x 9.8 = 16,1,700 ohms and a mechanical travel of 9.8". The RP38 potentiometers have a weight of about 1 oz per travel-inch, life in excess of 500,000 cycles, and withstand vibration of 10G from 10 to 2000 cps on all axes. The RP 38 standard rectilinear potentiometer is a development of Humphrey, Inc., 2805 Canon St., San Diego 6, Calif.

FOR MORE INFORMATION CIRCLE 146 ON READER-SERVICE CARD

# NOR LOGIC MODULES

New "HS" Series modules provide transistorized Sheffer Stroke gates for use in mechanizing digital sys-

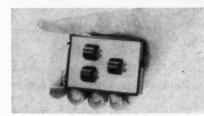


tems. Complete digital switching networks including flip-flops can be built from these gates. When Stroke gates are used with Abacus clocked flip-flops, two level logic can be operated with a single phase clock at 3mc.—Abacus, Inc., 3040 Overland Ave., Los Angeles 34, Calif.

CIRCLE 147 ON READER-SERVICE CARD

# TRANSISTOR CHOPPER KIT

Three plug-in transistor choppers with application notes comprise a circuit designer's kit to acquaint design-



ers with solid-state chopper characteristics. Model 50P and 60P are germanium units for operation to 90°C whereas 70P is a silicon transistor unit capable of operation to 150°C.—Solid State Electronics Co., 15321 Rayen St., Sepulveda, Calif.

CIRCLE 148 ON READER-SERVICE CARD

# **DRUM COMMUTATORS**

New facilities for production of drum-type printed circuit commutators and encoding disc provide units



from ¾" up to 12" diameter with precious metal segment paths raised or flushed to insulating areas. Constant linear rate for all brushes avoids errors inherent in flat disc commutator design.—The Sibley Co., Haddam, Conn.

CIRCLE 149 ON READER-SERVICE CARD

CIRCLE 51 ON READER-SERVICE CARD ----





LOW FRICTION and WEAR
LASTING PRECISION ALIGNMENT
ELIMINATE BINDING and CHATTER
ZERO SHAKE or PLAY
LONG LIFE — LOW MAINTENANCE
SOLVES SLIDING LUBRICATION PROBLEMS

Used by progressive engineers in the latest guidance, fire control and navigation systems, computers, inertial devices, instruments.

Various types of BALL BUSHINGS are made for shaft sizes from 1/8" to 4"... with small sizes available in Stainless Steel. Write for literature and name of our representative in your city.

THOMSON INDUSTRIES, Inc.

Dept. D. MANHASSET, NEW YORK

# SUBCARRIER FM OSCILLATOR



New solid state FM telemetering subcarrier oscillator Model 0-20 having excellent data stability over the -55° to 125° C range uses silicon transistors and diodes in diecast aluminum case .- Dorsett Electronics Labs., 119 West Boyd, Norman, Okla.

CIRCLE 150 ON READER-SERVICE CARD

### PLANAR TUBE OSCILLATOR

New L-band planar tube oscillator comprising dual cavity with tuned plate and tuned cathode controlled by

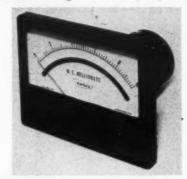


a single lead-screw covers range of 920 to 1400 mc with small change in output level. Designed for CW or pulse applications in low-power transmitters, signal generators, local oscillators and test fixtures; full characteristics available on request .- General Communication Co. 677 Beacon St., Boston 15, Mass.

CIRCLE 151 ON READER-SERVICE CARD

# MINIATURE AC VTVM

New Model 130-1 AC VTVM has standard ranges to 300 v, input im-



pedance of 1 megohm, and 1% accuracy. Can measure from 50 to 50,000 cps.-Trio Laboratories, Inc., Plainview, L. I., N. Y.

CIRCLE 152 ON READER-SERVICE CARD

# SONAR SOUNDING SET

New AN/SQN 11 Sonar Sounding Set indicates depths from 5 to 100 ft to ±3% of full scale. Transistor-



ized, lightweight, low-cost unit consists of remote indicator-control box, transmitter-receiver-power supply box, and through-the-hull transducer. Operates on input power of 115 v  $\pm 15\%$ , 60 cps  $\pm 2\%$ , 30 watts between 0° to 50°C.-Kearfott Div., General Precision Inc., 1150 McBride Ave., Little Falls, N. J.

CIRCLE 153 ON READER-SERVICE CARD

# SPECTRUM ANALYSIS FILTER

New Rayspan Spectrum Analyzers, Type MRFR, each with 100 filters covering portions of the 50 cps to 100 kc spectrum, are available for shock



and vibration studies, acoustic studies, equipment inspection, speech analysis, transmission surveillance and telemetered data analysis. Full specifications on request.—Commercial Apparatus & Systems Div., Raytheon Company, 1415 Providence Turnpike, Norwood, Mass.

CIRCLE 154 ON READER-SERVICE CARD

# Precision in timing-Accuracy in setting



GROUND SUPPORT **EQUIPMENT** 

> 20 TURN MICROMETE

The EAGLE Microflex Timer provides unequaled accuracy in closing and opening a circuit. 20 turn, double micrometer dial speeds the selection of new settings over full 7200° range,

- PIN-POINT ACCURACY with 1200 different dial settings. No
- 9 DIFFERENT ACTIONS available for each of 3 SPST 10 ampere contacts to suit various circuits.
- PLUG-IN COMPONENTS permit quick timer replacement.

### OTHER POPULAR HIGH QUALITY EAGLE TIME-COUNT CONTROLS







B

For more details on the Microflex Timer, write for free Bulletin 110. or contact your local Eagle Representative listed in Thomas Register or Phone Directories in 25 principal cities.

RACKMOBILE

CIRCLE 53 ON READER-SERVICE CARD

# ESCO CABINETS "STACK EFFECT" COOLING (pat.pend.)

- · RETMA AND MIL SPEC SIZES
- . SHOCK PROTECTION (pat. pend.)
- VIBRATION ATTENUATION
- · SHIPPING PROTECTION
- NOISE ATTENUATION
- · ADJUSTABLE SHELVES
- OVER 500 POUNDS CAPACITY
- "WORK BENCH" TOP
- TOUGH GRAY HAMMERTONE FINISH
- EXCLUSIVE BY ESCO
- Write for additional information

# STACKRACK



ESCO ENG. & MFG. CORP 6550 South Stalford La Grange, Illinois Fleetwood 4-5128



CIRCLE 54 ON READER-SERVICE CARD

MILITARY SYSTEMS DESIGN Nove

# New! Motor-Tach 1/3 Shorter Than Models You're Now Using



Now you can design instrument packages that are more compact than ever before!

CEDAR ENGINEERING has created for you a new line of precision miniature servo motors and motor-tachometers that are shorter, lighter, and electrically more efficient than ever before

possible. The new short CEDAR Size 10 motor-tach, for example, is only 1.375" long . . . a full third shorter than conventional Size 10's and even shorter than commonly used Size 8's.

In addition to permitting more compact instrumentation, the shorter length and reduced weight minimize susceptibility to vibration failure.

Efficiency? You get normal motor output at a lower wattage input. And these rugged new space misers are built without compromising reliability. They fully meet requirements of MIL-

Specifications are now available for the new CEDAR short servo motors and motor-tachs in Sizes 8, 10 and 11. For more information, contact us today at the address below. We're standing by to give you immediate service.

# Write, Call, or TWX Collect:

Mr. David Baker, Sales Manager CEDAR ENGINEERING **Control Data Corporation** 5806 West 36th Street Minneapolis 16, Minnesota Phone: WEst 9-1681 TWX MP-974

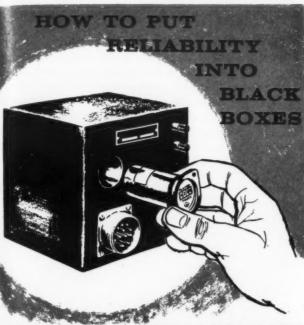


CEDAR ENGINEERING Division of

# CONTROL DATA CORPORATION

Minneapolis 16, Minnesota

CIRCLE 52 ON READER-SERVICE CARD



tting

METE

racy in rometer

range,

10 am

gs.

# "INDEX OF RELIABILITY" ... Mean Operating Time Between Failures.

Reliability and Maintainability are always important — and most often very critical factors. Their definitions invariably involve "time". Some military specifications use "mean operating time between independent failures" as the index of reliability and call for the incorporation of elapsed time indicators into the operating equipment. Replacing critical components before they reach the limit of rated life contributes greatly to peak operating efficiency and reliability.

Waltham's subminiature elapsed time indicators are being used and designed into both military and commercial equipment for ground support and airborne applications. They are small and light enough to go anywhere. Jewel bearings, precision gear trains — some with a reduction of 1.8 billion to 1, a new low inertia synchronous motor are teamed with over 110 years of experience to provide instruments reliable and accurate enough to provide precise "measures of reliability".



MOIT

Waltham can provide subminiature elapsed time indicators in both digital and dial readouts - and in production quantities. Write for bulletins #5001 and #5002 or telephone TW 3-4000

WALTHAM

PRECISION INSTRUMENT COMPANY ALTHAM 54, MASSACHUSETTS

CIRCLE 55 ON READER-SERVICE CARD

DESIGN November-December, 1960

## AM-CW RECEIVER



New special-purpose receiver Type 2501 for AM and CW reception has a tuning range of 55 to 260 mc designed for measuring the Doppler shifts of incoming signals, and features a low noise figure with uniform performance throughout the entire range.-Nems-Clarke Co., 919 Jesup-Blair Dr., Silver Spring, Md.

### CIRCLE 155 ON READER-SERVICE CARD

### COMPACT X-BAND DELAY

New compact and lightweight X-Band waveguide delay lines are up to



50% smaller than conventional X-Band delays, but have same low loss and low reflection properties of the standard Turbo delay lines .- Turbo Machine Co., Lansdale, Pa.

CIRCLE 156 ON READER-SERVICE CARD

# STRIP LINE CIRCULATOR

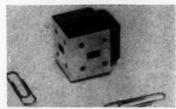
New X-band miniaturized strip line circulator has a minimum isolation



of 20 db and a maximum insertion loss of 0.4 db over a 6% band. Has VSWR of less than 1.4:1, handles 10w average power and 10 kw peak power. Input impedance is 50 ohms .-Hycon Mfg. Co., 1030 S. Arroyo Parkway, Pasadena, Calif.

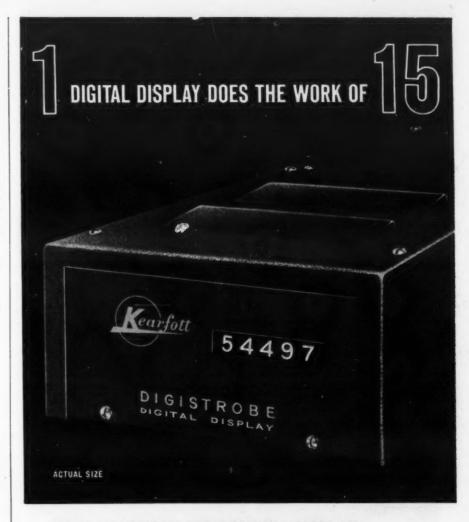
CIRCLE 157 ON READER-SERVICE CARD

# TEE CIRCULATOR



New compact Ka-band ferrite microwave tee circulator will handle 20-kw peaks and average power of 20 watts. Isolation between channels is 20 db minimum and maximum VSWR is 1.20.-Airtron Inc., 200 E. Hanover Ave., Morris Plains, N. J.

CIRCLE 158 ON READER-SERVICE CARD



# **NEW KEARFOTT DIGISTROBE\* DISPLAY**

Kearfott's new, highly compact Digistrobe digital display utilizes the stroboscopic principle to produce an exceptionally high-definition readout in the actual size shown here. Through the use of a unique shutter arrangement, a single diode-encoding matrix is shared by all columns (5 in the standard model), resulting in substantial savings in electronic components and circuitry. The fast response time of the Digistrobe (56 milliseconds transition from one five-digit quantity to a totally different one) permits a single unit to sample several different inputs on command through an input selector switch. Up to 15 individual displays of existing types can thus be replaced by a single Kearfott Digistrobe!

Incorporating only two moving parts and exclusively solid-state switching circuitry, the Digistrobe has extremely long life expectancy and requires minimum maintenance and service. Operation is directly from the output register of a computer, counter or allied equipment, eliminating the cost of intervening circuitry. Two years of extensive laboratory tests assure compliance with Kearfott's rigid standards of quality. For complete data and specifications, write for Digistrobe bulletin.

\*Kearfott Trademark



**KEARFOTT DIVISION** GENERAL PRECISION, INC.

Little Falls, New Jersey CIRCLE 56 ON READER-SERVICE CARD



Precision's Type TX resistors are unsurpassed in uniformity of performance.

New winding techniques mass-produce resistors free from dangerous "cross-overs" and insulation breakdowns. Maximum reliability is assured . . . and . . . at mass-production prices.

According to your need, PRECISION'S Type TX Resistors may be had in the size and resistance value you want for your circuit. Terminals may be either axial or radial. Tolerances are standard from  $\pm 1\%$  to  $\pm 1/20\%.$  Where extreme accuracies are required, tolerances to  $\pm 1/100\%$  may be obtained . . . inductively or non-inductively wound.

Military requirements are to PRECISION'S specifications.

**PHYSICAL SIZE:** Available in 75 sizes, ranging from diameters from 3/32'' through 3/8'' and lengths from 3/16'' to  $1\cdot1/2''$ .

**RESISTANCE RANGES:** From .01 ohm through 5.0 megohm — in any resistance value required or decimal part thereof.

ACCURACY:  $\pm 5\%$  to  $\pm 1/20\%$ . Tolerances  $\pm 1/50\%$  to  $\pm 1/100\%$ (absolute) available on specification.

TEMPERATURE COEFF. OF RESISTANCE: Standard ±0.001% °C. throughout. Special temperature coefficient + 5000 ppm° to ±1 ppm°C.

For complete information about PRECISION'S Sub-Miniature Type TX Resistors, write to:

# PRECISION RESISTOR Co., Inc.

MANUFACTURERS OF WIRE WOUND RESISTORS EXCLUSIVELY 119 U. S. Highway #22, Hillside, New Jersey

CIRCLE 57 ON READER-SERVICE CARD

# VARIABLE ATTENUATOR

New low cost model of PI Line Continuously Variable attenuator, usable where large values of attenuation (over 10 db) are not required,



features 1.5 max VSWR for all attenuation values, max insertion loss of 0.5 db, 10 watt average power, over a range from 1.0 to 9.0 kmc. Either micrometer or shaft drive .-Antenna & Radome Research Associates, 27 Bond St., Westbury, L. I.,

CIRCLE 159 ON READER-SERVICE CARD

# REMOTE ATTENUATOR

Remotely controlled, new coaxial unit is non-attenuating type "N' connector when control voltage is applied. Upon removal of operating

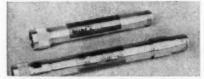


voltage, unit becomes a 20 db bi-directional attenuator usable from 50 mc to 3500 mc. Is available for 28 v dc or 115 v 400 cps operation; meets military environmental specs .- Don-Lan Electronics Inc., 1131 Olympic Blvd., Santa Monica, Calif.

CIRCLE 160 ON READER-SERVICE CARD

# MINI COAX ISOLATORS

A complete line of miniaturized coaxial line isolators with no external permanent magnets cover frequencies from UHF to X-band. Three basic units designed for C, S, and L-



band operate over 10% bandwidths to provide more than 15 db isolation with less than 0.9 db insertion loss, weight 4, 5 and 6 oz respectively. Advantages claimed for new units are extremely small size and weight, excellent electrical performance and almost 100% shielding.—Sperry Micro-wave Electronics Co., Clearwater, Fla.

CIRCLE 161 ON READER-SERVICE CARD

# Synchro Test Standard

Synchro testing conventionally has depended on the use of a control transmitter unit mounted in an index stand and used with a null detector to assure precise dyna input signals. The Astrosystem Synchro Standard (see orin Figure) provides a test signal with a functional ac the curacy of 2 seconds of arc, which can serve as a base men of reference for synchro testing or as an extremely accurate forward feed control input device for machine tools, computers, radar simulators and flight simula-



moto ргес

leaf

natu

1) is

of 10

20K

mum

picko

in sil

accon

1 17/8

Th

Th

When utilized in synchro testing, the new standard is manually switched to discrete positions. Elimination of the null detector and control transmitter in an index stand eliminates error due to operator misinterpreta again

Synchro standards are constructed with passive electromagnetic elements, fulfilling the requirements for military quality equipment and stability against deterioration of its initial accuracy. The Standards have been effectively used in qualification testing, production testing, production assembly testing and final system testing of synchros. They are a development of Astrosystems, Inc., 220 East 23rd St., New York, N. Y.

FOR MORE INFORMATION CIRCLE 162 ON READER-SERVICE CARD

# **Digital Products Section** Forms New Firm

NATICK, MASS.—The digital and nuclear divisions differ of the Harvey-Wells Corporation, a wholly-owned subsidiary of Hercon Electronics Corporation, have expanded into two separate and independent organizations, the Harvey-Wells Corporation and Harvey-Wells Electronics, Inc. The Harvey-Wells Corporation, continuing as a Hercon subsidiary, will develop and manufacture electromagnetic and nuclear magnetic resonance product lines, many of which require numbers of multi-ton magnets, and will relocate where better facilities for such construction can be acquired.

The Harvey-Wells Electronics, Inc. is owned and operated by a newly-formed group, composed of key members of the digital division of the parent company, with Mr. J. W. Wood as president. This organization Fig. 2 will specialize in the advancement of the parent or environment ganization's lines of high-speed "Data Bloc" and "Data Macha Pac" digital building blocks and related digital prod Comm ucts. It will remain in the present modern manufactur Editor ing plant located in Natick, Mass., expanding its prod gyro, uct digital development programs in phase with the be avrelocation of the Harvey-Wells Corporation.

FOR MORE INFORMATION CIRCLE 163 ON READER-SERVICE CARD

**Gyro Characteristics Vary to** Meet Job Requirements

on the

n index

nely acnachine simula-

tandard

nination

n index

erpreta-

ive elec-

inst de

ds have

produc

inal sys

ment of

k, N. Y

CE CARD

ned sub

rganiza.

on, conlop and

magnetic

ire num-

here bet-

and op

of ke

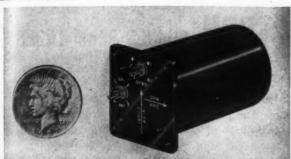
ompany

ICE CARD

rired.

n

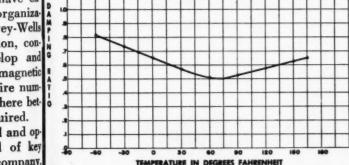
A new fluid-damped angular rate sensor having precise dynamic characteristics so controlled as to permit tailrd (see oring to the peculiar requirements of any customer, is mal ac the contribution of the R. C. Allen Aircraft Instrua base ment Division.



This miniature (13/4" dia x 33/8" long) hermetically sealed unit employs a synchronous, hysteresis type motor supported on radial ball bearings, with gyro precession restrained by opposing beryllium copper leaf springs. Through variations of leaf thickness, the natural frequency is controlled, allowing selected angular momentum rates and/or gimbal deflection to act against the resulting spring rate and produce the desired sensitivity. Maximum angular rates from 0.05 to 10 radians/sec., undamped natural frequencies from 8 to 80 cps and angular momentum rates of 100,000 gm cm<sup>2</sup>/sec to 800.000 gm cm<sup>2</sup>/sec are coupled with excellent pickoff characteristics. Mounting flange (Fig. 1) is optional.

The microsyn pickoff provides output impedances of 10 to 2,000 ohms, 19v signal at maximum rate into 20K load and a 10 mv rms null voltage, with a minimum phase shift near null. Calibration curves of the pickoff produce a relatively sharp "V" at null.

The damper consists of opposing plungers operating in silicone oil within cupped chambers. Compensation for viscosity change due to temperature fluctuation is accomplished by selection of suitable material having different thermal coefficients for the piston and cylinder walls. A typical damping curve is shown in



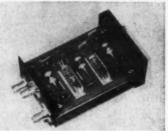
anization Fig. 2. (From 4-page Rate Gyro Data sheet, providing arent or environmental specifications.—R. C. Allen Business d "Data Machines, Inc., Aircraft Instrument Division, 333 tal prod Commerce Ave., S. W., Grand Rapids, Mich.)

nufacture Editor's Note: The manufacturer advises this rate its prodgyro, with identical performance characteristics will be available in subminiature form (1-5/16" diameter 1 1 1 long) in approximately three months.

FOR MORE INFORMATION CIRCLE 164 ON READER-SERVICE CARD

# **MIXER-PREAMPLIFIER UNITS**

New line of matched mixer preamplifier units gives optimum performance from a UHF system. Orion-matched mixer-preamplifier in



one assembly assures symmetrical bandpass, specified bandwidth, gain and noise figure .- Orion Electronic Corp., 108 Columbus Ave., Tuckahoe, N. Y.

CIRCLE 165 ON READER-SERVICE CARD

# COMPUTER-TYPE DELAY LINE

New lumped-constant delay lines Models F-577A (10-μsec delay) and F-578A (15-µsec delay) are totally encapsulated in epoxy resin, utilized



internally in computers, and eliminate the need for terminal boards which commonly trap moisture. Both have multiple taps, impedance of 400 ohms and operating temperature to 125°C .- Control Electronics Co., c/o Delay Line Div., 10 Stepar Place, Huntington Station, L. I., N. Y.

CIRCLE 166 ON READER-SERVICE CARD

# TEMPERATURE TEST CHAMER

New Model A-120-2-HC, providing over 2 cuft test volume with controllable temperatures from - 150°F to 300°F (± 2°) with indicating con-



troller. Recording and programming are optional features for production or R/D testing.—Cincinnati Sub Zero Products, 3932 Reading Road., Cincinnati 29, Ohio

CIRCLE 167 ON READER-SERVICE CARD

NOW...AN INDUSTRY FIRST FROM FAIRCHILD

# A REVOLUTIONARY PRESSURE TRANSDUCER WITH 5V. D-C OUTPUT



# Solid-State Strain Gauge transducer

OTHERS MAY HAVE PROMISED IT . . . STILL OTHERS MIGHT HAVE HINTED THEY'RE ON THE VERGE OF GETTING IT... BUT ONLY FAIRCHILD HAS IT!...THE INDUSTRY'S FIRST 3S-G

The Fairchild 3S-G combines the best overall characteristics of both strain gauge and pot-type transducers, has none of their inadequacies. It has a semiconductor strain-gauge sensor. It possesses extraordinary accuracy and environmental capabilities. It produces a 5-volt d-c output signal that eliminates the need for impedance-matching or signal amplification. In its utter simplicity (only two mechanically-functioning parts) it is extremely reliable. It also incorporates a resistive calibration device.

The Fairchild 3S-G is responsive to both static and high-frequency dynamic pressures. It is fully compatible with existing military ground telemetry and industrial systems. It is competitively priced, measures all media and is insensitive to case distortions.

The Fairchild 3S-G is only 3" long, 11/8" diam., and weighs only 5 ounces. It meets and exceeds MIL-E-5272B. Pressure ranges from 0-100 to 0-10,000 psig full scale now available, below 100 psig will be available soon. Better than ±0.1% linearity and 0.1% hysteresis over temperature range of -65 to +250°F. Both zero and full range sensitivity change less than 0.5% over any 100°F excursion within the rated temp. range. It has infinite resolution.

Fairchild components ... built and tested beyond the specs for Reliability in Performance.

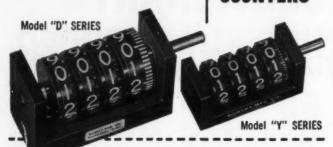


**TRANSDUCERS** RATE GYROS **POTENTIOMETERS ACCELEROMETERS** 

CIRCLE 58 ON READER-SERVICE CARD

# DURANT

# DIGITAL READ-OUT COUNTERS



for MISSILE TRACKING, RADAR CONTROLS, COMPUTERS, NAVIGATION INSTRUMENTS, GAUGING INSTRUMENTS, and ANY other indicator applications.

- Meets military specifications.
  High speeds, lower torque, lower moment of inertia for long life.
  Nylon wheels with legible figures, nylatron pinions.
  Single, 1½, or double wheels.
  Right or left hand drive, clockwise or anti-clockwise rotation.
- One-piece aluminum die cast frame.
  Base mounting. Threaded mounting holes may be placed in frame top or ends.
  "Y" Series, single or dual bank.
  Component parts can be purchased separately to meet design requirements.

Your answer to an infinite number of variable demands for PRECISION CONTROLS. Send for Catalog No. 400



1949 N. Buffum St., Milwaukee 1, Wis. • 49 Thurbers Ave., Providence 5, R. I.

REPRESENTATIVES IN ALL PRINCIPAL CITIES CIRCLE 59 ON READER-SERVICE CARD

# **MM MILITARY CASES**

COMBINATION . TRANSIT . INSTRUMENT MIL-T-945, T-4734, T-21200, STD-108, C-4150



# **OVER 1,000,000** VARIATIONS AVAILABLE NO DIE CHARGE

Your choice of over 1,000,000 variations in dimensions, proportions, metals finishes, and custom accessories for military combination, transit, instrument and portable cases. Whatever your need, the MM (multi-measure) method gives you high production savings even on custom runs as low as 20 units. Send us your print or requirements direct or contact your MM representative.

FREE: Send for free catalog and dimension specification sheets

111 BLOOMINGDALE RD., HICKSVILLE, N. Y.

# VARIABLE DELAY LINES

New Series 700 Miniature Variable Delay Networks provide time delays from 1/8 to 1.5 µsec with pulse rise



times from 0.03 to .30 µsec (max), 1.0 db max pulse attenuation. Networks are rated at 500 v dc max working volts .- ESC Electronics Corporation, 534 Bergen Blvd., Palisades

CIRCLE 168 ON READER-SERVICE CARD

### RECTIFIER

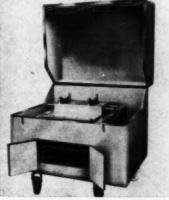


New compact convection-cooled power supply suitable for laboratory and industrial applications, Ramm Rectifier Model SB115-10 operates from 220/440 v to  $\pm 10\%$ , 3-phase, 60-cycle power source; continuous duty output rating of 115-v dc at 10 amps. All components designed to withstand overloads up to 200% .-Ramm Rectifier Co., Inc., 527 Faile St., The Bronx 59, N. Y.

CIRCLE 169 ON READER-SERVICE CARD

# PORTABLE VIBRATION TEST

New simplified "Rotocon" portable vibration tester for operation by factory quality control personnel provides a fundamental output at 50 cps



and overtones at predetermined multiples. To operate, bolt component to table of machine and turn on switch. Timer automatically turns off at end of test. Simple data take-off and other characteristics explained on request .- Rototest Laboratories, Inc., 2803 Las Flores, Lynwood, Calif.

CIRCLE 170 ON READER-SERVICE CARD

# **NEW LOW PRICES!**

# ON CHARACTRON® SHAPED BEAM TUBES

Economies made possible by increased production now permit drastic price reductions on almost all types of CHARACTRON Shaped Beam Tubes. These unusual cathode ray tubes have the spot writing capabilities of conventional tubes and also have a unique capability for high speed display of exceptionally clear characters. Some typical CHARACTRON Shaped Beam Tubes are shown below. Write today for complete list of tubes and new low prices. Stromberg-Carlson-San Diego, Department A-71, P. O. Box 2449, San Diego 10, California.



Used for situation display applications. Features the highest character quality. Type G3049 is similar to the C19R, but uses fewer external components for faster setup, easier maintenance.



Used for situation display applications. Character size may be dynamically changed by varying a single tube voltage. This same voltage also produces a focused spot for spot writing.

# C7F11 7-INCH

For data recording. Capable of displaying more than 10,000 characters within a 41/2 inch square on its screen. Adjustable character size. Low voltage Type C7D11 also available.



# C5G 5-INCH

For data recording. Designed for minimum size and ease of operation, this tube requires only one external component and is only 15"



STROMBERG-CARLSON-SAN DIEGO A DIVISION OF GENERAL DYNAMICS CORPORATION

CIRCLE 61 ON READER-SERVICE CARD

MILITARY SYSTEMS DESIGN

CIRCLE 60 ON READER-SERVICE CARD

dition equip matic

liquid contro range lows h onds. Electr Cottm

RAN

CIR

binati bratio tion.-Ave.,

INST Min fier,

gain o input ment. from

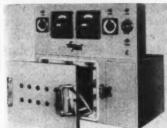
amplif gain Uses o operat Yu E Terhu

CIR

CIRCLE

# **ENVIRONMENTAL CHAMBER**

New table-top portable environmental chamber for testing and con-

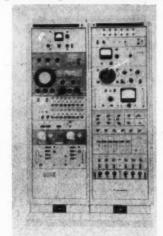


ditioning of electronic components is equipped with dual timers for automatic cycling of electric heat and liquid CO<sub>2</sub> cooling without constant control adjustment. Temperature range —100°F to 400°F (± 1°F) allows hot-cold shock to —100°F in seconds. Chamber is 14" x 10".—The Electric Hotpack Co., Inc., 5060 Cottman St., Phila. 35, Pa.

CIRCLE 171 ON READER-SERVICE CARD

# RANDOM VIBRATOR CONTROL

New Model 1011 System controls any power amplifier and shaker com-



bination to provide true random vibration to match any test specification.—Genisco, Inc., 2233 Federal Ave., Los Angeles, Calif.

CIRCLE 172 ON READER-SERVICE CARD

# INSTRUMENT PREAMPLIFIER

Miniature transistorized preamplifier, Type A102 provides sensitivity gain of 100 by connecting it between input signal and laboratory instrument. Bandwidth is flat within 3 db from 10 cps to 80 kc, max output is



2.5 v rms with 100 Kohm load. Two amplifiers can be used in tandem for gain of 10,000 without oscillation. Uses one 15 v radio type battery with operational life of 1,000 hours.—Ad-Yu Electronics Lab., Inc., 249-259 Terhune Ave., Passiac, N. J.

CIRCLE 173 ON READER-SERVICE CARD

CIRCLE 62 ON READER-SERVICE CARD



ES

eatures 1049 is xternal enance.

naracter rying a ge also g.

ON

ESIGN

# Engineering notes



Report No. 13 Type CC 506 Thrust Control System

BY STANLEY M. INGERSOLL, Capabilities Enginee

Designed for tactical artillery weapons, this system maintains the thrust levels of liquid propellant rocket engines at specified magnitudes. Its sensitive SM/I-designed pressure transducer measures combustion chamber pressure and is statically and dynamically accurate even in the extreme shock and vibration environments of the missile. When the transducer detects a deviation from the pre-set reference pressure, it generates an error signal. This signal is amplified and transmitted to a servo controlled valve which restores the pressure to the proper setting. The amplitude of the signal is proportionate to the magnitude of pressure change. Heart of the transducer is a unique, SM/I-developed twisted Bourdon tube that combines high pressure sensitivity (rotational movement) and low acceleration and vibrational sensitivity (linear movement). A 200 PSI unit has called 200 sensitivity (linear movement). movement). A 300 PSI unit has only a .2% error under 15 g's vibration and 10 g's acceleration and withstands 20 g's shock without disturbing its setting.

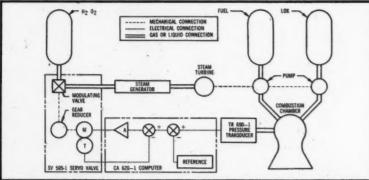
Typical Technical Data

Temperature Vibration												 					 	65° to +165°F .10-38 cps ±0.25"
Shock																		Double Amplitude. 38 to 2000 cps ±25 g's 50 g's
Weight												 	 				 	Sea Level to 200,000 ft. 10 pounds 115 volts 400 cycles
Accuracy																		better than 1% of the pressure
Magnitude o	f:	S	el	t	P	re	1	18	U	IF	e							30 lb/min H2O2 300-1000 psi 2-3 seconds









For more information and complete operating specifications, write or wire SM/I today. Address your inquiry to Stanley M. Ingersoll,



SERVOMECHANISMS/INC.

Los Angeles Division 200 Aviation Boulevard El Segundo, California

CIRCLE 63 ON READER-SERVICE CARD

# TUBULAR RELAY

New tubular design having only one moving part (armature) features simplicity with very high reli-



ability-life of more than 200 million mechanical operations. Hermetic sealed and nitrogen filled, it meets 15 G vibration, 10 to 2000 cps, 30 G shock de-energized, 100G shock energized with no contact opening. Complete technical data on request.-Wheelock Signals, Inc., Long Branch,

CIRCLE 174 ON READER-SERVICE CARD

# DICE-CUBE RELAY



New half-inch cube SPDT relay meeting all MIL-specs for relays of this size have terminals for 0.100" grid mounting, ratings from dry circuit to 1 amp resistive, temperature -65° to 125°C. One pin is off set for keying. Hi-G, Inc. Bradley Field, Windsor Locks, Conn.

CIRCLE 175 ON READER-SERVICE CARD

# MINIATURE AIR CAPACITOR



New Type 2951 capacitor, less than " long is fully adjustable from 0.8 to 10.0 mmf. Used in missiles, computers, and other electronic devices requiring fine tuning .- Johanson Mfg. Corp., 400 Rockaway Valley Rd., Boonton, N. J.

CIRCLE 176 ON READER-SERVICE CARD

# QUARTZ SEALCAP TRIMMER

New miniature high-voltage hightemp quartz sealcap trimmer features capacitance range of 2 to 10 pf, 3000

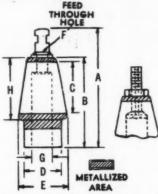


vdc working voltage, 5000v dielectric strength; 2 x 10° megohms insulation resistance; temp coefficient of ± 50 ppm/° C; Q of 1500 at 1 mq.—JFD Electronics Corp., 6101 16th Ave., Brooklyn 4, N. Y.

CIRCLE 177 ON READER-SERVICE CARD

# Metalized Ceramic Insulators

A silver fired coating on terminal areas of ceramic insulators now enables manufacturers of capacitors Systems and transformers, etc., to efficiently make connections gage fa at test voltages to 15,000 V and still maintain her. metically sealed units.



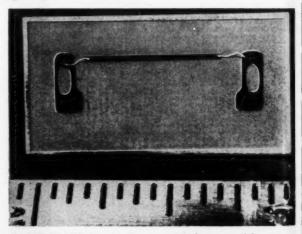
Soldering to the metalized portion of the ceramic terminal is easily accomplished. This tinned metalized coating will withstand 450° for 11/2 minutes. When used in feed-through applications the solder provides complete sealing at the base and at the feedthrough hole of the insulator (See Figure). (From 2-page technical Bulletin M-102, Metalizing Industries, Inc., 338 Hudson St., Hackensack, N. J.)

FOR MORE INFORMATION CIRCLE 178 ON READER-SERVICE CARD

# **Bondable Semiconductor** Strain Gage

New Micro-Sensor bondable semiconductor strain gage Model MS 105-350 for microstrain measurement in all types of military space and industrial systems are now available in production quantities from Micro-Systems, Inc., 2925 East Foothill Blvd., Pasadena,

The new strain detection device (see Figure) measuring 1" x 1/2" utilizes a thin silicon element only 1/2" long and .0005" thick attached to an epoxy-based carrier for application to test surfaces, provides an output 50 to 60 times greater than bondable metallic strain gages. Also its impedance is low, resulting in a high signal-to-noise ratio.



SOLIDSTATE Strain Gage provides over fifty times the output of bondable metallic strain gages.

The -65° tempera stages. erating FOR MO Fa

The 1

two-y

ducted

New Texas I capable tions fr stations

transmi

all faul pervisor every fo

and 3 single c ny tim ind tun Fault nd rece parate

so pro e bridg nputs n ervice o e tran aia cor ystems, anged 1

Each ingle p

sy mai or ope ircuitry FOR MOR

MILITARY SYSTEMS DESIGN Novem

The new semiconductor strain gage is the product of a two-year research and development program conducted by the Solid State Division of Electro-Optical Systems, parent company to Micro-Systems, Inc. Its gage factor is said to be approximately 130.

tions

rough

only

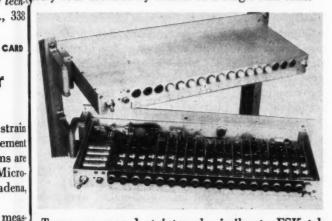
etallic

The current operating temperature range is from -65° to 180°F for the Model 105-350, and higher temperature models are in advanced development stages. Resistance is 350 ohms, with a maximum operating strain of over 3000 microinches per inch.

FOR MORE INFORMATION CIRCLE 179 ON READER-SERVICE CARD

# **Fault Monitor Scans Thirty Remote Stations**

New transistorized fault alarm developed by the Texas Division, Collins Radio Co., Dallas 7, Tex., is capable of reporting 11 or 17 different fault conditions from each of as many as 30 remote microwave stations. Shown in the accompanying illustration, a transmitter (upper unit) at each remote station conalized tinuously scans for faults and simultaneously reports all faults present to its associated receiver at a supervisory station (but here shown as lower unit) every four seconds by means of a single AM tone.



Tones are spaced at intervals similar to FSK telegraph and can be set within one of five ranges between and 30 kc. The number of stations reporting over a single communication channel may be increased at any time by adding transmitter and receiver pairs g in a and tuning them to unused frequencies.

Fault reports are displayed at both the transmitter and receiver by front panel indicator lights, with a separate light for each fault. A remote alarm signal is also provided by the receiver. Transmitter outputs may be bridged directly on the baseband, while receiver nputs may be bridged on an isolation amplifier or ervice channel output. In addition to fault reporting, he transmitter and receiver may be used for binary ata communication or remote control. In very large ystems, the transmitters and receivers may be aranged for automatically interrogated operation.

Each transmitter and receiver unit is housed in a ingle plug-in module, 11/2" high, 7" deep and 18" vide. Plug in subassemblies are also used to permit asy maintenance. Only 20 watts of power are required or operation, due to the completely transistorized ircuitry.

FOR MORE INFORMATION CIRCLE 180 ON READER-SERVICE CARD

# "GUM DROP" TOROID

New miniature "gum drop" epoxy encapsulated toroid in the 2 kc to

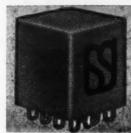


25 kc range has a maximum inductance of 2 hy. Toroids feature high Q, excellent stability vs temperature and current, self shielding and high L-to-volume ratio. Meet MIL-T-27A. -Cinema Engineering, 1100 Chestnut St., Burbank, Calif.

CIRCLE 181 ON READER-SERVICE CARD

# **CUBE-SHAPED RELAY**

New 4-PDT 2-amp crystal case relay meeting MIL-R-25018 and MIL-R-5757C is packaged in a case 0.800" square and 0.875" high. It will be



produced in quantity by early spring, 1961, and will occupy the same chassis space as two DPDT crystal case relays mounted side by side.—Union Switch & Signal Div., Westinghouse Air Brake Co., Pittsburgh 18, Pa.

# CIRCLE 182 ON READER-SERVICE CARD CONSTANT CURRENT SUPPLY

New Model 151B transistorized constant current supply covers 0.05



to 500 ma in four ranges, regulated within 0.25% for 0-20 volts load and 105-125 volt line. Particularly useful for semiconductor testing, potentiometer and sensitive relay tests. also strain-gage systems .- Quan-Tech Laboratories, Inc., Boonton, N. J.

CIRCLE 183 ON READER-SERVICE CARD

# Engineering notes from the



Report No. 14 AME 604 Thermocouple Reference Junction Temperature Compensating System

The AME 604, the most advanced version of the SM/I Temperature Compensator, is a highly accurate device for electronically compensating for the cold junction in a thermocouple temperature measurement system for use where extreme environmental demands are made on airborne or ground equipment.

This 12-channel temperature measurement system is composed of 12 compensator modules and 12 power supply modules and operates from a 28 V.D.C. input. This unit is completely encapsulated to insure mechanical stability of the system. One power supply which incorporates solid state devices and one compensator module are required for each channel. Components in the compensator and power supply modules are assembled on a Melamine-Glass terminal board and following lead attachments are individually potted with a Ureathane foam-type potting compound that provides maximum stability under extremes of temperature and humidity as well as protection against operational vibration. The system design is such that the number of channels may be changed to suit a customer's requirements.

Typical Performance **Specifications**  

			THERMOCOUPLE LEADS
00 11 00	-		ALUMEL
28 V. D.C.	POWER	COMPENSATOR	CHROMEL-
INPUT	SUPPLY		C OUTPUT

AME 604 Temperature Compensating System - System Diagram

For more information and complete operating specifications, write or wire SM/I today. Address your inquiry to Stanley M. Ingersoll, Capabilities Engineer.



SERVOMECHANISMS/INC. Los Angeles Division 200 N. Aviation Boulevard El Segundo, California

CIRCLE 64 ON READER-SERVICE CARD

# FOR PRECISION MEASUREMENTS

# RESISTANCE DECADES-MODEL DR

Available in a wide variety of standard models. Accuracy at 1.0 and 0.1 ohm steps is  $\pm 0.25\%$ . Accuracy of all other resistors is  $\pm 0.1\%$  of indicated value. Self-cleaning, molded nylon and silver plated brass switch mounted below panel. Zero resistance is less than .003 ohms per dial. Hardwood case. Models DR-1D to DR-4D, 8" x 5½" x 4½" h. Weight 4 lbs. net, 6 lbs. shipping. Models DR-50D to DR-52D, 9" x 6" x 4½" h. Weight 5 lbs. net, 7 lbs. shipping. Models DR-70D and DR-71D, 17¼" x 5" x 4½" h. Weight 6 lbs. net, 8 lbs. shipping.



ELECTRICAL SPECIFICATIONS								
Medel No.	Total Res. Ohms	Decade Steps	Accuracy					
DR-1D	1,110,000	10x(1,000 +10,000 +100,000)	±0.1%					
DR-2D	111,000	10x(100+1,000+10,000)	±0.1%					
DR-3D	11,100	10x(10+100+1,000)	+0.1%					
DR-4D	1,100	10x(1.+10+100)	±0.25 & ±0.1%					
DR-50D	11,111	10x(.1+1+10+100+1,000)	±0.25 & ±0.1%					
DR-51D	111,110	10x(1+10+100+1,000+10,000)	±0.25 & ±0.1%					
DR-52D	1,111,100	10x(10+100+1,000+10,000+100,000)	±0.1%					
DR-70D	1,111,111	10x(.1+1+10+100+1,000+10,000+100,000)	±0.25 & ±0.1%					
DR-71D	11,111,110	10x(1+10+100+1,000+10,000 +100,000+1,000,000)	±0.25 & ±0.1%					

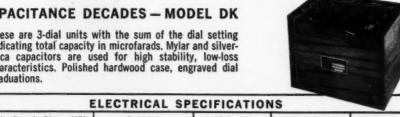
# WHEATSTONE BRIDGES - MODEL RN

Universally used for the measurement of all types of resistance devices and circuits where high accuracy is required. Models available for performing Murray-Varley Loop tests.

	ELECTRICAL SPECIFICATIONS							
Model	Total Res. of Decade	Ratio Dial Settings	Circuits	Dimensions				
RN-1	9X(1+10+100+1000)	.001, .01, .1, 1.0, 10, 100, 1000	************	9"x8"x6½"				
RN-2	9X(1+10+100+1000)	.001, .01, .1, 1.0, 10, 1000, M10, M100, M1000	Murray & Varley	9½″x8″x6½″				
RN-3	10X(1+10+100)+9(1000)	1/1000, 1/100, 1/10, 1/9, 1/4, 1/1, 10/1, 100/1, M10, M100, M1000	Murray & Varley	9½"x8"x6½"				

# CAPACITANCE DECADES - MODEL DK

These are 3-dial units with the sum of the dial setting indicating total capacity in microfarads. Mylar and silvermica capacitors are used for high stability, low-loss characteristics. Polished hardwood case, engraved dial



	ELECTRICAL SPECIFICATIONS								
Model	Decade Steps (MFD)	Accuracy	Dielectric	Power Factor	Peak Volts				
DK-2A	0.001, 0.01, 0.1	±1.%, ±1.%, ±1.%	Silver Mica	0.2%, 0.2%, 0.2%	700, 700, 500				
DK-4	0.001, 0.01, 0.1	±1.%, ±1.%, ±3.%	Silver Mica, Mica & Foil, Mylar	0.2%, 0.2%, 1.%	700, 700, 400				
DK-5A	0.01, 0.1, 1.0	±1.%, ±3.%, ±3.%	Mica & Foil, Mylar Mylar	0.2%, 1.%, 1.%	700, 400, 400				
DK-11A	0.01, 0.1, 1.0	±0.5%,±0.5%,±2.0%	Silver Mica, Silver Mica Mylar	0.2%, 0.2%, 1.0%	700, 500, 400				
DK-10	0.0001, 0.001, 0.01	±0.5% in 10 mmf	Silver Mica	2.0%, .2%, .2%	700, 700, 700				

Industrial
Zurrenge -
- No. 1
Instruments

	PHYSICAL SPECIFICATIONS		
-	Over-all Dimensions	Weigh Net	ht (Lbs.) Shipping
DK-2A, DK-4, DK-10	8 x 51/2 x 71/2	8	10
DK-5A, DK-11A	103/4 x 73/4 x 71/2	10 _	12

Industrial Instruments: 89 COMMERCE ROAD, CEDAR GROVE, N. J.

CIRCLE 65 ON READER-SERVICE CARD

# **VOLTAGE REGULATOR**



New solid-state miniature voltage regulator for space vehicles accepts unregulated 24 to 32 volts dc and provides a regulated voltage of 16 to 18 volts (customer adjusted). For load currents up to 100 ma, the output voltage is constant within 300 mv.-Acton Laboratories, Inc. Space Instrumentation Div., 533 Main St., Acton. Mass.

CIRCLE 184 ON READER-SERVICE CARD

# HI-VOLTAGE DIVIDER

A new record in high-precision highvoltage divider was set when a 300:1 ratio network of 30-megohm resist-



ance for use on 30,000 volts was specified by a special order customer to operate at 0.05% accuracy. Large divider, here compared with a conventional small resistor network, actually maintained voltage division within 0.01%. believed to be a new record in this size divider .- Resistance Products Co., 914 So. 13th St., Harrisburg, Pa.

CIRCLE 185 ON READER-SERVICE CARD

## MINIATURE COOLING BLOWER

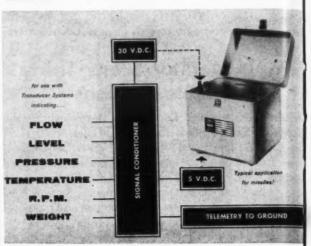
New all-aluminum axial blower Unit MSA-11050 has a 60-cps motor,



is rated at 12 cfm at 3600 rpm, specs, and weighs only 0.5 lb. Dimensions: 2.94" wide, 3.44" high, and 3.50" deep .- Specialty Blower Div., Torrington Mfg. Co., Torrington, Conn. CIRCLE 186 ON READER-SERVICE CARD

# Multirange Digital Voltmeter Reads Missile Transducers

A new portable multirange digital-indicating volt meter, designated Model BH190, available in 4 ranges covering from 0-.020 v to 0-10,000 v dc, is adapted to many uses in flight and ground support testing o



MULTIRANGE digital voltmeter is adapted to mis

Outputs from transducers sensing flow, level, pres sure, temperatures, rpm and weight are digitally displayed to an accuracy of 0.1% of range. Each instru ment is calibrated to an accuracy of better than 0.05% and resolution is better than 0.02%. Individual cali bration of each instrument to this precision is ac complished by a mylar tape slidewire 144" in length in which sprocket holes are variably spaced to linearize up to 13% input deviation. This tape actuates the digital readouts. When the input deviation is greater than 13%, printed tape presentation is used.

Digital electrical and analog electrical outputs an available for telemetry systems of any type, making this instrument particularly useful in the checking of telemetry units at all points in the missile launching complex. (From 4 page Technical Bulletin BH190 DC Digital Voltmeter, Howell Instruments, Inc., 347 West Vickery Blvd., Fort Worth 7, Texas, former the B&H Instrument Co., Inc., of the same address.

FOR THIS LITERATURE CIRCLE 187 ON READER-SERVICE CARD

# Function Error in a **Computing Resolver**

A computing resolver is a rotatable transforme whose output obeys the equation

 $E_{01} = K_1 E_{11} \sin \theta$ 

where  $\theta$  is the rotor angle relative to the stator and K is the complex transformation ratio.

When it is necessary to compute this simple trigo nometric function in an analogue computer, the com puting resolver is employed. For most application such a computation is too elementary, so another out put winding is added permitting the design engine to simultaneously utilize both a sine and cosine func tion, and for complete flexibility in computation, sti

of cor

Cor The o tempe are us still o 16 pa solver Saddl

> FOR Ele

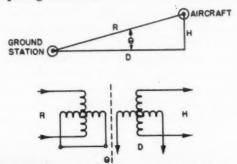
Ele an el from the fi as sh prepa gradie Mo thick

of the

Mot stack stricti are fo

Dielec 1-page bach East 2

another input winding is added (See Figure). Such is the general winding configuration when one speaks of computing resolvers.



**RESOLUTION** of Distance and Altitude from Slant Range is simple problem for resolver.

Compensated resolvers are still more sophisticated. The objective of compensation is to produce a complex transformation ratio which is virtually independent of temperature and impedance loading. Several techniques are used, but the schematic and equations shown above still comprise the basic computing resolver. (From 16 page monograph "A Primer for Computing Resolvers" by Theta Instrument Corp., 520 Victor Street, Saddle Brook, N. J.)

FOR THIS LITERATURE CIRCLE 188 ON READER-SERVICE CARD

# Electrostrictive Ceramics are New Motor Elements

y dis

instru

0.059

l cali

is a

ength

neariz

es th

greate

its ar

nakir

ing

nching 3H190 ., 3479 ...

CARD

form

and K

ne com

ication

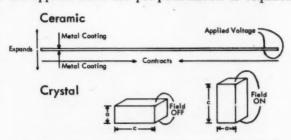
ner ou

ngine

ie fund

Electrostrictive ceramic changes dimensions when an electric field is applied. The ceramic, prepared from modified barium titanate, expands parallel to the field and contracts perpendicular to the field, as shown in the sketch. Electrostrictive ceramic is prepared in thin, flat sheets so that a high voltage gradient is readily obtained.

Motion data given in the table is typical of a 5 mil thick specimen and is independent of the polarity of the applied field. No pre-polarization is required.



TYPICAL CON	ITRAC	TIO	N FO	R 3"	LEN	GTH	
Volts/Mil	12.5	25	37	50	63	75	88
Mils of Motion	0.2	0.5	0.75	1.0	1.25	1.45	1.5

Motor elements, or Capadynes, in beam, disc and stack types, have been developed utilizing electrostrictive ceramics. Other uses for this new material are for memory units and thermal voltage converts. Dielectric constant is about 2000. (From set of four 1-page technical data sheets, Electronic Dept., Mullenbach Division, Electric Machinery Mfg. Co., 2100 East 27th St., Los Angeles 58, Calif.)

FOR THIS LITERATURE CIRCLE 189 ON READER-SERVICE CARD

# **BLOWER MOTOR**



New C-20-37 induction motor features extreme speed, low noise, high efficiency, precision balance, and superior quality. Features: ¾ hp, 200-v 400-cps, 22,300 rpm, 2.83 oz-ft torque.—Kearfott Div., General Precision, 1150 McBride Ave., Little Falls, N. Y.

CIRCLE 190 ON READER-SERVICE CARD

# SUBMERSIBLE COUNTER



Hermetically sealed electric counter can operate indefinitely under water because electric reset mechanism is sealed. Model 5-YE-9156-ER is high speed unit running to 2400cpm and resetting in 105 msec.—Durant Mfg. Co., 1981 No. Buffum St., Milwaukee 1, Wis.

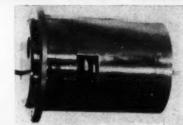
CIRCLE 191 ON READER-SERVICE CARD

# LINT-FREE COVERALL

New lint-free, static-free, acid-resistant Coverall featuring streamline pattern for plant safety, is made of white herringbone Dacura, a blend of polyester fiber and rayon. Details in six-page folder.—Angelica Uniform Co., 1427 Olive St., St. Louis 3, Mo.

CIRCLE 192 ON READER-SERVICE CARD

# FRAMING CAMERA GEARHEAD



New gearhead for portable, continuous-writing Model 326 Dynafax framing camera takes 7100-rpm input from a small motor and steps it up to 100,000 rpm for fast mirror rotation.—Bowmar Instrument Corp., 8000 Bluffton Rd., Ft. Wayne, Ind.

CIRCLE 193 ON READER-SERVICE CARD

WANT MORE INFORMATION? Let us get it for you. Use the Postage Paid Inquiry Card in each issue of . . .

MILITARY SYSTEMS DESIGN

Its Fast and Easy

# ACTUAL



# SIZE

**20 TO 30 VOLTS DIRECT CURRENT** 

TIMING FOR RELIABILITY of systems, sub-systems and modules is accurate, dependable with Houston Fearless "Alert" sub-miniature Elapsed Time Indicators. Measure life expectancy, provide operational warnings to prevent overuse failure. Tested for severe environmental use. Exceeds MIL-E-5272C. 1,000 and 10,000 hour models. Weight, 2 oz., 1" dia., 1\(\frac{1}{4}\)" depth. Write for specifications.



HOUSTON FEARLESS
DIVISION OF HOUSTON FEARLESS CORPORATION

DIVISION OF HOUSTON FEARLESS CORPORATION 11801 West Olympic Blvd., Los Angeles 64, California

CIRCLE 66 ON READER-SERVICE CARD



FIG.

Labo

with :

circui

Beca

The

is quit

amplif

1). Th

play a

The

The

FOR M

TRAN

and o

Electr

Fifth

chapte

Tunne fiers a

ability

transis

INTR

THES

FOR '



# Includes everything needed to perform a wide variety of logical operations

Now Digital offers a basic selection of 500 kilocycle logic circuit packages which can be used to design, test and demonstrate up counters, down counters, four-bit shift registers, decimal decoders, Gray-to-binary decoders, two-binary-digit adders and subtracters, and other similar digital pulse apparatus.

Graphic front panels (a Digital first) permit all logical interconnections to be made quickly and easily by means of handy stacking banana-jack patch cords. And the units can be assembled and reassembled in any number of different combinations in the plug-in mounting panel.

Included in the Basic Kit are nine DEC Digital Test Equipment units one inverter, one diode nor, four flip-flops, one delay, one clock, and one pulse generator — and the necessary accessory equipment — power supply, power cable, mounting panel, and one hundred patch cords. Other Building Blocks from Digital's fully compatible 500 kilocycle, 5 megacycle and 10 megacycle lines can be added to increase the versatility of this unique new kit.

Complete Kit (FOB Maynard) \$1038





WEST COAST OFFICE . 8820 SEPULVEDA BOULEVARD . LOS ANGELES 45, CALIFORNIA CIRCLE 67 ON READER-SERVICE CARD

# HYDRAULIC PUMP

New Model 905 piston-type hydraulic pump operates at 40,000 rpm, is 2.5" dia x 2.7" long and delivers



13.1 hp at 40,000 rpm. At lower speeds the pump has a volumetric efficiency of 98% and an over-all efficiency of 90%. Flow response is 30 msec or less .- Vickers Inc., Div. of Sperry Rand Corp., Detroit 32,

CIRCLE 194 ON READER-SERVICE CARD

# EXTENDED RANGE ANALYZER

New high resolution spectrum analyzer, Model MD-500, accomplishes separation of signals only 10 cps apart in the 450 kc to 100 mc range.

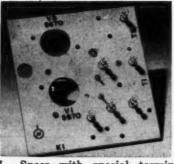


Two inputs provide use of external oscillator to automatically scan the difference frequencies in such applications as single sideband monitoring, FM modulation, parasitic oscillations and power frequency hum. Complete specifications on request.-Probescope Co., Inc., 8 Sagamore Hill Drive, Port Washington, N. Y.

CIRCLE 195 ON READER-SERVICE CARD

# TERMINAL BOARDS

Custom designed terminal boards from silicone, melamine, epoxy or other laminates to meet customer and



MIL- Specs with special terminals are available in small or large production runs .- Special Products Div., National Connector Corp., 311 Fifth Ave., North, Minneapolis 1, Minn.

CIRCLE 196 ON READER-SERVICE CARD

# A Pocket Laboratory Scope

Designed to be the answer to a busy field engineer prayer, the new EI Lab Model 150 Oscilloscope offer a number of interesting examples in transistorize design. Five circuit boards (Fig. 1) plug into a mothe board, which in turn is incorporated in an anodize aluminum case with a front panel assembly and a rea panel assembly in an overall size of 23/4" x 31/4" x 51/4 (Fig. 2). Electro Instruments, Inc., is located at 116 Morena Blvd., San Diego 10, Calif.

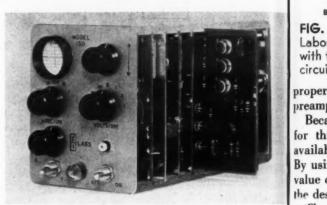


FIG. I. MINIATURE SCOPE with full-scale per formance utilizes printed circuit ultra compact cor struction made possible by transistorization an high definition I" CRT.

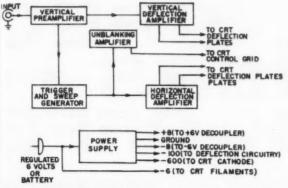


FIG. 2. FIELD ENGINEERS show high interest in extremely portable, battery-powered oscilloscope they can carry in their brief case. 2" model is shown in background.

Small size, moreover, is accomplished without sac fice of excellent performance characteristics, due ingenious circuitry arrangements. The vertical defle tion amplifier is direct coupled with a typical ban width of dc to 3 mc and a vertical sensitivity of 1/1 v/div. Input impedance is 1 megohm shunted by 20 The use of a physical input resistor prevents injury the first transistor if the input should be overloaded.

The input vertical attenuator mounted on the from assembly panel serves to attenuate the signal to

Wiley N. Y.,



pe

gineer e offe

storiz

mother nodized a real x 51/2

at 116

t con

rest in

oscope

odel is

ut sac

due

1 defle

al ban

of 1/

y 20 p

njury

aded

FIG. 3. BLOCK DIAGRAM of Electro Instrument Laboratory Model 150 Oscilloscope agrees closely with the organization of the circuitry on five printed circuit cards.

proper level for the first circuit board, the vertical preamplifier.

Because of the broad-band characteristics desired for this attenuator and the small amount of space available, an unconventional design was necessary. By using matched fixed capacitors, with a single fixed value of resistance plus one trim value for each range, the desired dc to 3 mc band-pass is achieved (Fig. 3).

The output impedance of the vertical preamplifier is quite low and feeds the main vertical deflection amplifier and the trigger and sweep circuit board (Fig. 1). The vertical deflection amplifier positions the display and amplifies the signal to give full-scale vertical deflection on the CRT. The signal going to the trigger and sync generator is coupled into an inverting amplifier which can provide either plus or minus signals to the trigger generator.

The horizontal sweep may be triggered at any point on the slope of a negative or positive going signal of one-half division or more in amplitude. The sweep may also be made to free-run by adjusting the trigger slope control, and will sync onto a fast-recurring signal. Sweep speed is variable from 1 µsec/div to 10 msec/div, and all normal CRT adjustments are available.

The internal rechargeable battery provides continujous operation for two hours and for longer intermittent periods. It can also be powered from an external sixvolt battery. (Schematic circuits of the Horizontal Deflection Amplifier and the Power Supply are discussed in the Circuitry Section of this issue, page 16). FOR MORE INFORMATION CIRCLE 103 ON READER-SERVICE CARD

# BOOK REVIEWS (Cont. from page 23)

TRANSISTOR MANUAL, by H. R. Lowry, Manager, and others, Semiconductor Products Dept., General Electric Company, Kelley Bldg., Liverpool, N. Y., Fifth Edition (1960) 329 p., 5½" x 8½", \$1.00. New chapters on Tunnel Diode Theory, Switching Circuits, Tunnel Diode Amplifiers, Feedback and Servo Amplifiers and Test Circuits. Specifications and interchangeability information on American JEDEC-registered transistor types.

FOR THIS LITERATURE CIRCLE 197 ON READER-SERVICE CARD

INTRODUCTION TO MODERN NETWORK SYNTHESIS, by M. E. Van Valkenburg, (1960) John Wiley & Sons, Inc., 440 Fourth Ave., New York 16, N. Y., 498 p., 5½" x 9", \$11.75. Basic methods of modern network synthesis, including applications to communications and automatic control systems.

FOR THIS LITERATURE CIRCLE 198 ON READER-SERVICE CARD

# TAB TERMINAL SWITCHES

New aircraft-type toggle switches meeting all Mil-Specs are available



in complete line of single- and doublepole units having 4" wide male tab connections.—Kulka Electric Corp., 633-643 S. Fulton Ave., Mt. Vernon, N. Y.

CIRCLE 199 ON READER-SERVICE CARD

# INCREMENTAL MULTIMETER

New Tensor 5880 Incremental Multimeter enables increments of any range of the unit to be expanded about any point in the range and dis-



played on an external servo recorder. Range consists of over 50 different values of current, voltage, resistance, audio power, temperature, and transistor characteristics. Typical accuracies are 1.5% dc and 2% ac.—Tensor Electric Development Co., Inc., 1873 Eastern Parkway, Brooklyn 33, N. Y.

CIRCLE 200 ON READER-SERVICE CARD

# ALUMINUM CABLE CONNECTORS

New Cold-Forged aluminum connectors for aluminum aircraft cables exceed Mil-specs. Electro-tin plated



surfaces over high-purity aluminum provide contacts operating 20°F less than cables used on.—The Thomas & Betts Co., 36 Butler St., Elizabeth, N. J.

CIRCLE 201 ON READER-SERVICE CARD

### **AMPLIFIERS**

New M2201-A broadband X-band traveling-wave tube amplifier for test instrument application is designed as a direct electrical and mechanical replacement for use in the HP494A amplifier unit and operates over the 7.0-12.4 kmc frequency range.—

Microwave Electronics Corp., 4061

Transport St., Palo Alto, Calif.

CIRCLE 202 ON READER-SERVICE CARD



# EYE TEST FOR RADAR

B&L optical-electronic-mechanical capabilities assure accuracy in missile tracking system

The strength of our missile defense program depends in part on extreme accuracy of radar tracking.

Bausch & Lomb has developed a camera lens for boresighting a radar antenna—in essence, this lens checks the performance of radar just as one's vision is checked in an eye examination.

Accuracy of this lens system easily meets the most extreme requirements.

The same skills that made possible this missile track radar camera lens are available to assist on your project. Write us for full details. Bausch & Lomb Incorporated, Military Products Division, 92112 Bausch St., Rochester 2, N. Y.



CIRCLE 48 ON READER-SERVICE CARD

ESIGN November-December, 1960





# "PIG-TAILORING"

a revolutionary new mechanical process for higher production at lower costs. Fastest PREPARATION and ASSEMBLY of Resistors, nents for TERMINAL BOARDS, PRINTED CIRCUITS and MINIATURIZED ASSEMBLIES.

PIG-TAILORING eliminates: • Diagonal cutters Long nose pliers · Operator judgment · 90%
 operator training time · Broken components · Broken leads · Short circuits from clippings · 65% chassis handling · Excessive lead tautness · Haphaxard assembly methods.

PIG-TAILORING provides: • Uniform component position • Uniform marking exposure • Miniaturization spacing control • "5" leads for terminals • "U" leads for printed circuits • Individual cut and bend lengths • Better time/rate analysis • Cleser cost control • Invaluable labor saving

Pays for itself in 2 weeks



Write for illustrated book to Dept. MS-12



**Unique Vertical Gyro** for Target Drones

A new vertical gyroscope, Model NV 3203F (Fig. 1) designed for stabilization control in drone missile targets uses a unique erection system. This technique uses two weighted vanes and four reaction nozzles mounted atop the rotor case containing the electrically driven rotor.



FIG. I. REACTION jet nozzles, partially covered by unbalanced vane ends are shown in uncovered view of top of gyro, tilted toward the right. Weighted end of vane (far end) has uncovered its nozzle, while near end covers its nozzle, diminishing the air flow.

The inner gimbal, to which the pitch potentiometer is attached, is mounted in pitch axis bearings; and the outer gimbal, which holds the pitch axis bearings, has freedom on the roll axis provided by two similar bearings. A blower ring attached to the rotor forces air past the rotor and out of the four reaction nozzles.

When the gyro axis is vertical during a starting operation each vane leaf closes off half its accompanying air nozzle (Fig. 2). The resultant jet reaction forces are equal and opposite each other, equalling zero. When drift occurs and the top of the gyro tips forward, the weighted end of the pitch axis air control vane tips

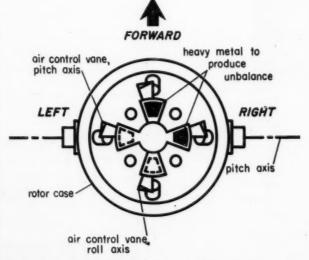


FIG. 2. ROLL and PITCH stabilization are separately controlled by four nozzles and two air control vanes for each axis.

# MIL-SPEC TIMERS AND PICK-OFFS

Countdown Controllers accurately show split-second, continually corrected visual missile countdown sequence. Electrically synchronized with actual count.



forwar

orifice

vane's

hand e

returni

again

forces

restore The

accura

of 30 (

aturiza

It is a

Firema

Portla

FOR MC

To

For

networ

must h

is ava

pick-uj

the fre

To

the pre

Q, low

field e

ment o

DIMEN

Adjust

Tod

molyb

for co

larly

portan

roid is

pact as

a min

(From

dimen.

three o

cies a

way, P

**Elapsed Time Indicator gives** visual check of power interruptions. Tied in with missile power supply from final assembly to launching. Records length of individual interruptions and total time off.



Transistorized Time Delay Relay (left) controls timing intervals from 50 milliseconds to 5 minutes. Made in 72 forms. Hermetically Sealed Delay Timer (right) provides fixed or adjustable time delay for repeat and reset cycle delay timing and sequencing for missiles or ground support equipment.



Atcotran Differential Transformers are electromechanical transducers for measuring linear motions. Three ATC milspec approved types, 6210-K (left) 6207-K (center) and 6203-K (right) give unprecedented reliability as displacement pick-offs for altimeters, pressure cells, servo feed-back signals, etc.

and engineered to the most

stringent specifications. Exten-

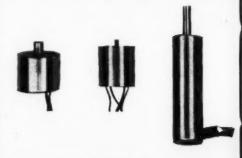
sive research and development is constantly increasing relia-

bility, design compactness and

circuit simplicity to meet ever

more exacting air and ground

requirements.



ATC can supply all kinds of differential transformers, timers, pick-offs and other related milspec components - designed

Send for your free Condensed Catalog "Automation Components and Control Systems"-today!

AUTOMATIC TIMING & CONTROLS, INC.

KING OF PRUSSIA, PENNSYLVANIA A Subsidiary of American Manufacturing Company, Inc.

CIRCLE 70 ON READER-SERVICE CARD

CIRCLE 69 ON READER-SERVICE CARD

50

MILITARY SYSTEMS DESIGN Nove

forward, its valve leaf uncovering the right-hand jet orifice. At the same time the opposite valve leaf on the vane's unweighted end closes the left-hand orifice. The uncovered jet's reaction forces forces down the right hand end of the gimbal, causing the gyro to precess, returning the gyro axis to vertical. As the vane leaves again cover half the opposing jet pipes, the reaction forces are balanced and the starting position is again

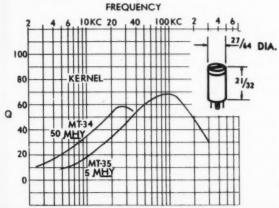
The method achieves true vertical within ±0.5° accuracy. The rugged construction withstands shocks of 30 G and vibration of 2 G to 1000 cps. Engineered for reliability and low cost rather than extreme miniaturization, the unit weighs approximately five pounds. It is a development of the Electronics Division, Iron Fireman Manufacturing Co., 2838 S. W. Ninth Ave.,

FOR MORE INFORMATION CIRCLE 203 ON READER-SERVICE CARD

# **Toroid Applications Chart**

For optimum performance of tuned circuits, phase networks and similar impedance devices, reactance must be an exact quantity. Even when the reactance is available in a fixed value capacitor or inductor, pick-up from other circuit components may change the frequency response of the impedance network.

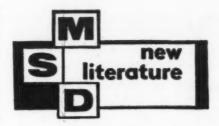
To meet the needs for coils which would possess the prerequisites for providing exact reactance-high Q, low change in inductance with dc current variation, temperature stability and freedom from external field effects-Burnell & Co. pioneered in the development of the toroid.



DIMENSIONAL and characteristic data for ATE-34 Adjustoroid coil, .0001 to 1.00 hy.

Today, the toroidal type winding combined with molybdenum core advantages provides the standard for coil characteristics in audio applications particularly where small space and accessibility are important considerations. Another advantage of the toroid is its self-shielding properties which permit compact assemblies of coils in miniaturized networks with a minimum of deleterious effects from coupling. (From 22" x 34" Coil Chart giving electrical and dimensional data on Toroidal Inductors. Coded in three colors for low, intermediate and high frequencies and with 20 applicable Q-Frequency characteristic graphs. Burnell & Co., Inc., 10 Pelham Parkway, Pelham, N. Y.

FOR THIS LITERATURE CIRCLE 204 ON READER-SERVICE CARD



PROXIMITY SWITCHES including control amplifiers are described in 8-page Catalog EDPS-80.—Electro Products Laboratories, Inc., 4501 Ravenswood Ave., Chicago 40, Ill.

CIRCLE 205 ON READER-SERVICE CARD

MIGROPHONES, accessories, high-ficomponents, etc. are covered in 28-page Catalog 60A.—Shure Brothers, Inc., 222 Hartrey Ave., Evanston, Ill.

CIRCLE 206 ON READER-SERVICE CARD

STRAIN GAGE, miniature Type HTM monofilament gage for use in crevices, fillets, etc. is described in 4-page data sheet 4331.—Baldwin-Lima-Hamilton Corp., Electronics & Instrumentation Div., 42 Fourth Ave., Waltham 54,

CIRCLE 207 ON READER-SERVICE CARD

SERVO MOTOR, hi-temp, size 8 precision, is detailed in 2-page Data Sheet 5004-09.—John Oster Mfg. Co., Avionic Div., Racine, Wis.

CIRCLE 208 ON READER-SERVICE CARD

SHAFT ENGODER. 12-page folder describes miniaturized shaft angle encoder, scan circuitry, and 8- and 13-digit analog to digital converter.—Litton Systems, Inc., 5500 Canoga Ave., Woodland Hills, Calif.

CIRCLE 209 ON READER-SERVICE CARD

TIME CODE GENERATOR for airborne application is described in 2-page Bulletin ZA-26211.—Electronic Engineering Co. of Calif., 1601 E. Chestnut Ave., Santa Ana, Calif.

CIRCLE 210 ON READER-SERVICE CARD

SPECTRUM ANALYZER models are described in 8-page Bulletin 7-300.—Raytheon Co., Commercial Apparatus & Systems Div., Norwood 67, Mass.

CIRCLE 211 ON READER-SERVICE CARD

SERVO CONTROL simplification using Servoscope analyzer is illustrated in 2-page Bulletin NB-660.—Servo Corp. of America, 111 New South Rd., Hicksville, L. I., N. Y.

CIRCLE 212 ON READER-SERVICE CARD

QUARTZ Crystal Transducers for pressure, force, acceleration and vibration measurements are described in 20-page folio of data sheets .-Kistler Instrument Corp., 15 Webster St., No. Tonawanda, N. Y.

CIRCLE 213 ON READER-SERVICE CARD

DIGITAL TEST EQUIPMENT. (5000 Series) and System Building Blocks (6000 Series) are described in 6-page bulletin.—Digital Equipment Corp., Maynard, Mass.

CIRCLE 214 ON READER-SERVICE CARD

SINGLE-TURN wirewound precision pots for missiles, computer assemblies, calibration controls, etc., are described in 6-page catalog.—Fairchild Controls Corp., 225 Park Ave., Hickesville, L. I., N. Y.

CIRCLE 215 ON READER-SERVICE CARD

SUBCARRIER transistorized oscillator for telemetery is detailed in 4-page Model 0-20 folder.—Dorsett Elec-tronics Laboratories, Inc., 119 West Boyd, Norman, Okla.

CIRCLE 216 ON READER-SERVICE CARD

SEMICONDUCTOR DIGITIZER applications have been compiled in 2-page Voldicon Bulletin.—Adage Inc., 292 Main St., Cambridge 42, Mass.

CIRCLE 217 ON READER-SERVICE CARD

VARISTORS and thermistors are described in 8-page catalog.—Victory Engineering Corp., 537 Springfield Rd., Union, N. J.

CIRCLE 218 ON READER-SERVICE CARD

ELECTRONIC CHOPPER. 2-page leaflet describes Model 70 silicon transistor chopper (or modulator).—Solid State Electronics Co., 15321 Rayen St., Sepulveda, Calif.

CIRCLE 219 ON READER-SERVICE CARD

MAGNETIC CERAMIC devices are described in 2-page bulletin.—Lockheed Electronics Co., Avionics & Industrial Products Div., 6201 E. Randolph St., Los Angeles 22, Calif.

CIRCLE 220 ON READER-SERVICE CARD



### **500 HOUR LIFE GUARANTEE\***

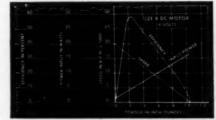
Due largely to improved brush design, CPPC size 8 DC motors qualify to catalogue specification after 500 + hours of continuous duty or 200,000 cycles of intermittent duty in controlled environments

## PRECISION CONSTRUCTION

Featuring a 12-bar commutator (5/16" dia.), stainless steel ball bearings, and corrosion resistant materials, the DC-8 family of motors is designed for miniature instrument systems. Weight 40 gms., length 1.380" max., dia., .750".

### **OUTSTANDING EFFICIENCY**

The typical performance curves (below) exhibit a linear torque-speed characteristic. The efficiencyup to 60% at .25 in. oz. torque-considerably surpasses that of other types of Servomotors.



For full information, write or call: Sales Dept., 5050 State Road, Drexel Hill, Pa., MAdison 2-1000, TWX Lnsdwn, Pa., 1122(U), or our Representatives.

# CLIFTON PRECISION PRODUCTS CO., INC.

ENGINEERS—Join a pioneer in the rotary components field. Write David D. Brown, Director of Personnel.

CIRCLE 71 ON READER-SERVICE CARD

today!

precision GO.. NO-GO AUTOMATIC comparators

**DECISION** DEVICES

Additional Products: MODULAR AUTOMATIC TESTING EQUIPMENT and COMPLETE AUTOMATIC TESTING SYSTEMS.

**OPTIMIZED** DEVICES, INC. ROgers 9-6110 864 FRANKLIN AVE. THORNWOOD, N. Y.

various models vacuum tube or transistorized

APPLICATIONS:

**Automatic** Go...No-Go Testing **Automatic Decision** Making **Automatic** Checkout Circuits **Automatic** Control **Automatic** Voltage

Calibration

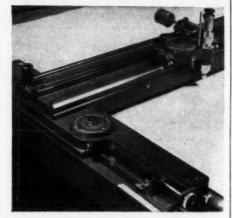


MORE SENSITIVE & PRECISE THAN METER RELAYS

Comparative sensitivity-better than 1 millivolt Repeatability of trip point-better than 50 microvolts Output-relay centacts for external connections

write for free Engineering Guide to Dept. MSD. CIRCLE 72 ON READER-SERVICE CARD





# A BETTER PLOTTER

for Precision Layout of Grid Systems and Coordinate Positions

The Coordinatograph, a new, better plotting instrument, is now being used for all types of precision layouts. It plots within .001" over a 471/2" x 471/2" working table. Rack and pinion construction for counter dials assures accurate measurements. 7 diameter pricker microscope permits observation and plotting in one operation. Radii from 12" to 40" can be plotted with beam compass. Vertically laminated plywood table. Vibration-free tripod mount. Write now for free folder.

AERO SERVICE CORPORATION 210 E. Courtland St., Dept. 111, Phila. 20, Pa.

CIRCLE 73 ON READER-SERVICE CARD



# CURRENT GOVERNOR

# Constant Current

- Meter Calibrator
- **Precision Current Source** Transistor and Diode Tester

High Accuracy > Excellent Stability > Programmable

For testing and measurement of transistors, diodes, clutches, solenoids, meters, other current sensitive devices.

- Current Range is 10µa to 1 amp. with 5 decade selectors.
- Regulation 0.002%
- Accuracy 0.03%

In use by leading companies for transistor test, diode test, clutch testing, calibration.

Literature describing this and other constant current sources from 0.1µa to 30 amp. may be obtained from



NORTH HILLS

GLEN COVE, L. I., N. Y.

CIRCLE 74 ON READER-SERVICE CARD

SERVO MOTOR size 15, precision, hitemp, Milspec Type is described in Data Sheet E 131A.—John Oster Mfg. Co., Avionic Div., Racine, Wis.

CIRCLE 230 ON READER-SERVICE CARD

SYNCHROS and Resolvers are listed in 4-page Condensed Catalog.—Verni-tron Corp., 125 Old Country Rd., Carle Place, L. I., N. Y.

CIRCLE 231 ON READER-SERVICE CARD

ELECTRONIC industrial equipment is featured in new 576-page 1961 catalog.
—Allied Radio Corp., 100 N. Western Ave., Chicago 80, Ill.

CIRCLE 232 ON READER-SERVICE CARD

RADAR Pulse Modulator is described in 2-page MRC Data Sheet 30-116-0.— Magnetic Research Corp., 3160 W. El Segundo Blvd., Hawthorne, Calif. CIRCLE 233 ON READER-SERVICE CARD

MECHANICAL FILTERS. 2-page Bulletin CR-WD-1005 lists 90 filters in tabular form.—Collins Radio Co., Western Div., 2700 W. Olive Ave., Burbank, Calif.

CIRCLE 234 ON READER-SERVICE CARD

PULSE GENERATOR. 2-page Data Sheet 3352 details Cintel double pulse generator Model 3352.—Marconi In-struments, 111 Cedar Lane, Engle-wood, N. J.

CIRCLE 235 ON READER-SERVICE CARD

PRECISION CRYSTAL FILTERS are described in a kit of 8 leaflets.—Systems, Inc., 2400 Diversified Way, Box 7726, Orlando, Fla.

CIRCLE 236 ON READER-SERVICE CARD

L-CAP RF FILTERS are described in 8-page catalog.—Devco, Inc., 24 Maple Court, E. Longmeadow, Mass.

CIRCLE 237 ON READER-SERVICE CARD

SEMICONDUCTORS, 12-page brochure lists key specs of transistors, rectifiers, and diodes.—Motorola Semiconductor Products Inc., 5005 E. Mc-Dowell Rd., Phoenix, Ariz.

CIRCLE 238 ON READER-SERVICE CARD

TRANSISTORS AND DIODES, diffused silicon, are described in 4-page guide.

—Schweber Electronics, 60 Herricks Rd., Mineola, L. I., N. Y.

CIRCLE 239 ON READER-SERVICE CARD

SILICON solar devices, transistors, diodes, zeners and SCR devices are described in 20-page catalog.—Semiconductor Div., Hoffman Electronics Corp., 1001 N. Arden Dr., El Monte, Calif.

CIRCLE 240 ON READER-SERVICE CARD

DIODE characteristics for Sperry Switching Types 1N690-1N693 and 1N920-1N923 are listed in 6-page Bulletin 2105.—Sperry Semiconductor Div., Sperry Rand Corp., South Nor-

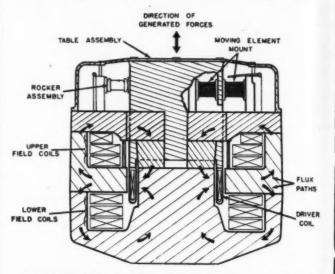
CIRCLE 241 ON READER-SERVICE CARD

DC TO DC Current Monitors for measuring flow of bus current up to 250 amps described in 2-page Data Sheet CM 9-1.—Arnold Magnetics Corp., 6050 W. Jefferson Blvd., Los Angeles

CIRCLE 242 ON READER-SERVICE CARD

# **Electrodynamic Shakers** Calibrate Transducers

The MB Model C11 (50 lb force) and Model C12 (150-lb force) Calibrator-Shakers are designed to calibate accelerometers, velocity type pickups, displacement pickups, etc., over a wide range of frequency and acceleration, as well as to conduct vibration tests.



MAGNITUDE of generated force is proportional to ampere-turns of the movable coil at any instant.

The force generated in the electrodynamic type of vibration exciter (See Figure) is as pure as the current supplied from the power supply. In general either a power supply of the electronic amplifier or rotating electrical equipment type generates pure voltages without appreciable harmonic content and therefore produces currents in the vibration exciter which are mainly fundamental with little or no harmonic content. The generation of a sinusoidal force without harmonic content results; which allows the excitation of structures under tests without interference of response caused by harmonics.

The system best suited to test requirements is determined by the equation F = Wg, where F is exciter force rating, W is the moving weight (exciter table weight plus specimen weight) and g is acceleration in gravitational units. The force rating of the exciter should be sufficient to accommodate the range of testing to be accomplished.

The force generated is derived from a current flowing in the movable coil which is positioned in a region of high magnetic flux density, obtained by connecting the stationary field coil to a suitable dc voltage.

The magnetic structure offers a continuous path of low resistance to the magnetic flux except for the region occupied by the movable coil, where it crosses the wires of the movable coil. Accordingly, the direction of the generated force is as indicated in the diagram. It may be reversed by reversing the direction of current in the movable coil. (From 16-page Bulletin, Products for Vibration Testing and Control," MB Electronics, A Division of Textron Electronics, Inc., 781 Whalley Ave., New Haven 8, Conn.)

FOR THIS LITERATURE CIRCLE 243 ON READER-SERVICE CARD

CYCLIC BINARI



- Accuracy 210 Plus Sign
- Parallel Operation

VER

of

ur-

th-

ro-

in-

he nic

uc-

nse

iter

ble

in

iter

OW.

ion

ing

of

the

sses recdia-

tion

etin. MB

nc.,

SIGN

20

- Command Readout
- 61/2" long × 33/4" Diameter
- Modular Construction
- Fully Transistorized
- Interrogation Rates to 250 pps
- 1000 RPM Slew Rate
- 30g Shock
- Separate Sine and Cosine Interrogation
- −50°C to +70°C Operation
- Specified Accuracy at 100 rpm

Other models include Linear 213 and 216 Encoders. Other models with Linear and Non-Linear encoding to customer specifications.

> Our staff is prepared to handle your Servo Repeater and Digital Readout requirements associated with Encoders.



CIRCLE 75 ON READER-SERVICE CARD November-December, 1960

SECONDARY FREQUENCY standards and steel-tape program timers are described in a series of five 2-page bulletins.—Designers for Industry, Inc., 4241 Fulton Parkway, Cleveland 9, Ohio.

CIRCLE 244 ON READER-SERVICE CARD

PULSE GENERATORS in solidstate-9KW series for microwave applicators are described in 2-page Data Sheet. Magnetic Research Corp., 3160 W. El Segundo Blvd., Hawthorne, Calif.

CIRCLE 245 ON READER-SERVICE CARD

POST AMPLIFIERS. AFC UNITS. Discriminators, Detectors, Oscillators and Mixer-Preamplifier Assemblies are described in 8-page catalog.—Orion Electronic Corp., 115 Winding Brook Rd., New Rochelle, N. Y.

CIRCLE 246 ON READER-SERVICE CARD

BISTABLE AMPLIFIER specs and design data are presented in 4-page bulletin.-Norbatrol Electronics Corp., 356 Collins Ave., Pittsburgh 6, Pa. CIRCLE 247 ON READER-SERVICE CARD

MINI OSCILLATOR, "C" band triode Model 151C, is described in 2-page Data Sheet C-2.—John Gombos Co., Inc., Webro Rd., Clifton, N. J.

CIRCLE 248 ON READER-SERVICE CARD

cps to 220 mc, having 3 beat-frequency bands, is described in 2-page leaflet. -Kay Electric Co., Maple Ave., Pine

CIRCLE 249 ON READER-SERVICE CARD

TOROIDS AND AMPLIFIERS. Two 4-page bulletins describe toroidal winding, inductor, and magnetic amplifier facilities; and stock servo and SCR control amplifiers.—Magnetico, Inc., 6 Richter Court, E. Northport, L. I., N. Y.

CIRCLE 250 ON READER-SERVICE CARD

MULTIPLE INPUT commutator-amplifier producing 5 to 10 v output from mv level sources is described in 4-page brochure.—San Diego Scientific Corp., 3434 Midway Dr., San Diego 10, Calif.

CIRCLE 251 ON READER-SERVICE CARD

DATA AMPLIFIERS for wideband transducer signals are described in new 8-page bulletin SCE-1.—Computer Engineering Associates, Inc., 350 N. Halstead, Pasadena, Calif.

CIRCLE 252 ON READER-SERVICE CARD

PREAMPLIFIERS. 4-page supplement (to Catalog 60) gives specs on microwave mixer-preamps, telemetry preamps, receivers, etc.—LEL, Inc., 75
Akron St., Copiague, N. Y.
CIRCLE 253 ON READER-SERVICE CARD

CATHODE RAY TUBES and recording storage tube types have characteristics listed in simplified chart.—William Weed, Raytheon Co., Industrial Components Div., 55 Chapel St., Newton 58, Mass.

CIRCLE 254 ON READER-SERVICE CARD

MIGROWAVE TEST EQUIPMENT is described in 4-page brochure.—Waveline, Inc., Caldwell, N. J.

CIRCLE 255 ON READER-SERVICE CARD

COAXIAL TERMINATIONS for RG cable designed for tank mounting and for either cable-to-air or cable-to-oil operations are described in 2-page sheet.—Components for Research, Inc., 979 Commercial St., Palo Alto, Calif.

CIRCLE 256 ON READER-SERVICE CARD

RECEIVING TUBES, 11" x 17" chart lists Preferred Mullard electron tubes.

—International Electronics Corp., 81 Spring St., New York 12, N. Y. CIRCLE 257 ON READER-SERVICE CARD

SEMICONDUCTORS. 24-page Short Form Catalog covers over 800 diodes, rectifiers, etc.—International Rectifier Corp., El Segundo, Calif.

CIRCLE 258 ON READER-SERVICE CARD

CAPACITORS in polar or non-polar Tantalum foil and meeting MIL-C-3965 are listed in 4-page Bulletin 2625. —International Electronic Industries, Inc. Div., Standard Pressed Steel Co., Box S8, Jenkintown, Pa.

CIRCLE 259 ON READER-SERVICE CARD

WIRE-WOUND RESISTORS. 20-page Catalog 14 RE covers encapsulated and bobbin type units.—Cinema Engineering Div., Aerovox Corp., 1100 Chestnut St., Burbank, Calif.

CIRCLE 260 ON READER-SERVICE CARD

TRANSFORMERS, epoxy molded for transistor power supplies, are de-scribed in 6-page TY-61.—Triad Transformer Corp., 4055 Redwood Ave., Venice, Calif.

CIRCLE 261 ON READER-SERVICE CARD

SCR AMPLIFIERS and modular phase controllers for missiles, rockets and servo motors applications are de-scribed in 4-page bulletin 60711.— General Electronic Control, Inc., 8001 Bloomington Freeway, Minneapolis 20,

CIRCLE 262 ON READER-SERVICE CARD

MICROWAVE SYSTEMS. 8-page catalog explores applications of RT-3A heterodyne repeater for 2 kmc communications relay.—Adler Electronics, Inc., 1 Le Fevre Lane, New Rochelle, N. Y.

CIRCLE 263 ON READER-SERVICE CARD

MICROWAVE TUBES and components are described in 24-page short form catalog.—Bomac Laboratories, Inc., Salem Rd., Beverly, Mass.

CIRCLE 264 ON READER-SERVICE CARD

MINI CERAMIC CAPACITORS, 2-page Bulletin H-4 describes NARROW-CAPS to fit 1/10" modular spacing; 4-page Bulletin J-1 describes custommade miniature ceramic capacitors.— Mucon Corp., 9 St. Francis St., Newark 5, N. J.

CIRCLE 265 ON READER-SERVICE CARD

POWER TRANSISTOR TEST SET. variable duty cycle, Model NC-1, is described in 2-page data sheet.—Baird-Atomic, I.c., 33 University Rd., Cambridge 38, Mass.

CIRCLE 266 ON READER-SERVICE CARD

CAPACITORS. 4-page bulletin details Series 38H and 38M plastic cased tubular capacitors.—John E. Fast & Co., 3598 N. Elston Ave., Chicago 18,

CIRCLE 267 ON READER-SERVICE CARD

# Select the transistorized DYNA-EMPIRE **GAUSSMETER** best suited to your needs

Completely transistorized Dyna-Empire gaussmeters accurately measure flux density and determine "flow" direction. Ideal for measuring and locating stray fields, plotting variations in strength and performing rapid comparisons of production lots against a standard. Easy-to-operate,—no jerk, pull, ballis-tic readings or circuit breaking required.



### **NEW TRANSISTORIZED GAUSSMETER MODEL D-874**

This precision instrument reads from 300 to 30,000 gauss full scale, with an accuracy of ±3.5%. It fulfills all needs of a quality gaussmeter at a modest

Special Features:

FIVE RANGES: 300 gauss full scale, 1,000 gauss full scale, 3,000 gauss full scale, 10,000 gauss full scale, 30,000 gauss full

SCAIC.
LINEAR OVER ENTIRE OPERATING RANGE
PORTABLE, OPERATES FROM OWN SELFCONTAINED BATTERIES
BATTERY LIFE—1,000 HOURS
REQUIRES NO EXTERNAL POWER SOURCE
INTERNAL CALIBRATION STANDARD
WEIGHT—4 LBS.
UNIVERSAL PROBE SUPPLIED IS 0.025" THICK BY
0.200" WIDE. ACTIVE AREA IS ONLY 0.0079
SQUARE INCHES LOCATED NEAR THE
TIP OF THE PROBE.

Complete with Universal probe \$195.

# TRANSISTORIZED GAUSSMETER MODEL D-855

This quality precision built Gaussmeter reads flux densities to 30,000 Gauss full scale ±2.5%. It is a highly sensitive instrument and provides tremendous flexibility. Complete with two linear probes—one high sensitivity probe for measurement of low density fields and one probe for measurement of high density fields. Special probe available for reading 3 gauss full scale.

Dyna-Empire, Inc. 1075 Stewart Avenue, Garden City, N. Y.



CIRCLE 76 ON READER-SERVICE CARD

CORROSION. THE THORNIEST PROB-LEM in liquid-level sensing, has met its match in Acoustica ultrasonic sensors. Machined from a single piece, the probes of these units offer no inroads to even the most corrosive media. Moreover, because they operate at high ultrasonic frequencies, oustica sensors are in no way affected by high-energy acoustic noise.

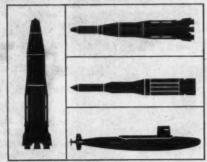
MANY TIMES MORE PRECISE than other types of sensors, Acoustica units offer control in the order of 1/32" -with response in microseconds. And because the system does not depend on sensing the difference in dielectric constants, there is no chance for ambiguity in operation, even in measuring low-density media such as hydrogen.

DESIGNED TO MEET CRITICAL MIL SPECS, Acoustica sensors measure almost any fluid in almost any environment. Models are available for operation at tem-peratures as low as — 420°F and higher than +500°F. Compact and lightweight, they operate at infinitesimal power levels. You can specify probes and transistorized control packages as integral or separate units with the full assurance that they will meet the most advanced space-age re-

WRITE FOR COMPLETE DATA



ACOUSTICA ASSOCIATES, INC. 10400 Aviation Blvd., Los Angeles 45, Calif. 600 Old Country Road, Garden City, N.Y.



THANKS TO ACOUSTICA ULTRASONICS —

# A LIQUID-LEVEL SWITCH THAT CORROSIVE LIQUIDS CAN'T ATTACK!



CIRCLE 77 ON READER-SERVICE CARD

VARIABLE CAPACITORS including tuning and trimming models are listed in 16-page Catalog 60.—Hammarlund Mfg. Co., Inc., 460 W. 34th St., New York 1, N. Y.

CIRCLE 248 ON READER-SERVICE CARD

CAPACITORS. Series of four 2-page data sheets describe metallized Mylar capacitors, and metallized paper capacitors in epoxy tubes.—Electron pacitors in epoxy tubes.—Electron Products Div., Marshall Industries, 430 N. Halstead St., Pasadena, Calif.

CIRCLE 269 ON READER-SERVICE CARD

LATCHING RELAY, 2-page Bulletin BR-594 describes BR-9 miniature, crystal-can sealed, 10-amp magnetic relay for aero-space and undersea applications.—Babcock Relays, Inc., 1640 Babcock Ave., Costa Mesa, Calif.

CIRCLE 270 ON READER-SERVICE CARD

RELAY MAINTENANCE is detailed in 8-page booklet.—P. K. Neuses, Inc., 8-page booklet.—P. K. Neuses, Inc., 511 N. Dwyer St., Arlington Heights,

CIRCLE 271 ON READER-SERVICE CARD

RELAYS, 4-PDT, 10 amp hermetically sealed BR-14 relay series meeting Mil Specs is described in 2 page Bulletin BR-595.—Babcock Relays, Inc., 1640 Babcock Ave., Costa Mesa, Calif.

CIRCLE 272 ON READER-SERVICE CARD

POWER SUPPLY, 8-page Catalog 120 lists specs and applications of mini power packs, transistorized frequency changers, solid-state power supplies, etc.—Electronic Research Assoc., Inc., 67 Factory Place, Cedar Grove, N. J.

CIRCLE 273 ON READER-SERVICE CARD

VOLTAGE REGULATORS, 8-page Catalog 4-265 provides spec data for 2,020 standard magnetic voltage regulator models.—Raytheon Co., Power Supply and Voltage Regulator Operations, Keeler Ave., So. Norwalk, Conn.

CIRCLE 274 ON READER-SERVICE CARD

POWER SUPPLY, 2-page Bulletin TT-160 describes compact 31/2", regulated d-c power supplies.—Dynamic Controls Co., 2225 Massachusetts Ave., Cambridge, Mass.

CIRCLE 275 ON READER-SERVICE CARD

DC POWER MODULES transistorized and packaged for proper dissipation of heat are described in 4-page brochure.

Dressen-Barnes Corp., 250 N. Vinedo Ave., Pasadena, Calif.

CIRCLE 276 ON READER-SERVICE CARD

POWER SUPPLY. Transistorized dc unit with 0.0005% regulation is described in 4-page Bulletin 201.—Krohn-Hite Corp., 580 Massachusetts Ave., Cambridge 39, Mass.

CIRCLE 277 ON READER-SERVICE CARD

ENGINE and generator applications are described in 24-page brochure are described in 24-page brochure "Onan Mliitary Products Capabilities." —D. W. Onan & Sons, Inc., 2515 University Ave., S. E., Minneapolis 14,

CIRCLE 278 ON READER-SERVICE CARD

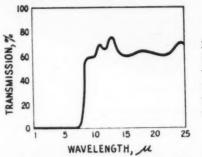
HERMETIC SEALS. 28-page Catalog 1259 lists types of precision hermetic seals.—Dage Electric Co., Inc., Beech Grove, Ill.

CIRCLE 279 ON READER-SERVICE CARD

# Far Infrared Filters Have Sharp Cut-On

Isolation of infrared radiation out to 25 microns in wavelength is said to be possible with new interference filters developed by Spectracoat, Inc., of Belmont, California. These filters pass an average of at least 60% of the desired radiation but less than 1% of radiation in the rejection band. At present the cut-on point can be placed anywhere between 1.5 and 8.0 microns, as desired. Research to place the cut-on point at any point up to 16 microns is continuing.

The availability of infrared interference filters to the wavelengths beyond 8 microns extends the application of infrared detection and discrimination techniques to the possibility of identifying objects having a relatively small temperature difference from their background, over the thermal range of 110°C to -160°C, which is approximately the range from boiling water to liquid air.



SHARP CUT-ON is typical of a transmission curve for the new long. wave interference type infrared filter.

An important characteristic of the Spectracoat filters is their sharp cut-on (See Figure). Heretofore, the isolation of long-wave infrared has been by scatter or absorption filters, which have the undesirable characteristics of gradual cut-on and poor rejection. The cut-on slope of the new filters can be made considerably steeper-better than 13% of the cut-on wave-

The first use of the new long wave-length infrared filters is expected to be for military and astonomical purposes, but a growing use in industrial process control is anticipated.

FOR MORE INFORMATION CIRCLE 280 ON READER-SERVICE CARD

# **Calibrated Field Intensity** Meter

A completely redesigned Model FIM Microwave and velo Calibrated Field Intensity Meter and Receiver was ductor recently announced by the Polarad Electronics Corp., unit fo Long Island City 1, N. Y. Four interchangeable RF tuning units cover the 1000 mc to 10,000 mc range, derwate and additional tuning units, presently under develop neutrall ment will extend the range to 20,000 mc.

Intended for use in locating and measuring RF depth a interference, field intensity measurements, determination tul tion of shielding effectiveness, propagation studies, support RF leakage measurements, and the analysis of transically emitters, receivers and other microwave components, days. Tit has been approved by US Air Force to perform means of the state of the radiation measurements under specification MIL-1- (From 26600. Incorporating a self-contained power supply, Inglewe its size and weight are greatly reduced over former

ration of enuated

models.

Single-k receiver recorder generato calibrate tional b FOR MOR

Unde

nents d

Rugge

graphi among oration The I thermor init w modulat and ter which o portion

The M Rotor ( derwate signals The

ing a tv

properly

nodels. It also has a peak-indicating VTVM for loation of impulse noise. All input signals can be atenuated up to 80 db in 1 db steps.

ence ont. least

of

it-on 8.0 point

s to

lica

techving their C to

from

rence

filter.

ilters

, the

er or

char-

The

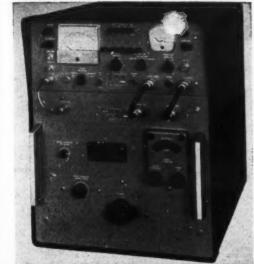
con

rared

mical

con-

ormer



Rugged and compact, the new Model FIM features: Single-knob tuning control (UNIDIAL) tunes both the receiver and the signal calibrator; video, audio and recorder outputs; direct-reading frequency dial; signal curve generator function can be externally modulated; and calibrated narrow-band horn antennas and omnidirectional broadband antenna.

FOR MORE INFORMATION CIRCLE 281 ON READER-SERVICE CARD

# **Underwater Transducers**

Underwater transducers and instruments designed for marine and oceanographic research and operations are among the products of the Hytech Corporation, Inglewood 3, Calif., including:

The Model 472 Telerecording Bathythermometer consists of an underwater unit which transmits two frequency modulated signals representing depth and temperature, and a surface unit which converts these signals into proportional de voltages suitable for driving a two-function analog recorder.

The Model 370 Telerecording Savonius Rotor Current Meter consists of an underwater unit which transmits two FM signals representing current direction owave and velocity over a single insulated conwas ductor with sea return, and a surface Corp., unit for driving indicator units.

e RF The Swallow Type Expendable Unange, derwater Pinger (See Figure) is a velop neutrally buoyant float which, when

properly weighted, will sink to any predetermined g RF depth and remain at that depth. It consists of a flotamina tion tube which houses batteries and circuitry, and udies, supports a magnetostrictive transducer which periodtrans ically emits an audible energy pulse in from 8 to 21 nents, days. The position of the pinger can be determined by rform means of two or more suitably separated hydrophones. IIL-1. (From 32-page catalog Hytech Corp., 6803 West Blvd., apply, Inglewood 3, Calif.)

FOR THIS LITERATURE CIRCLE 282 ON READER-SERVICE CARD

PNEUMATIC MOUNTS for supporting loads up to 30,000 lb/mount and to maintain absolute level within 0.00005 in/ft are described in Bulletin 60-05.1 (Serva-Levl Mount, series AM). Bulletin 59-04.5 describes 5200 series capable of 50 lb/mount.—Barry Wright Corp., 700 Pleasant St., Watertown 72, Mass.

CIRCLE 283 ON READER-SERVICE CARD

COMPRESSION TERMINALS. 6-page Bulletin SCT-60-101 lists g'ass-to-metal hermetically sealed term nals.— Electrical Industries, 691 Central Ave., Murray Hill, N. J.

CIRCLE 284 ON READER-SERVICE CARD

TUBING. 8-page Catalog 101 describes 8 types of insulating tubing and sleeving and zipper tubing.—Alpha Wire Corp., 200 Varick St., New York 14, N. Y.

CIRCLE 285 ON READER-SERVICE CARD

CERAMIC-TO-METAL sealing alloys available in air-or-vacuum-melted wire or strip are described in 6-page bro-chure.—Wilbur B. Driver Co., 1875 McCarther Highway, Newark 4, N. J.

CIRCLE 286 ON READER-SERVICE CARD

WIRING HARDWARE of all types listed in New 76-page Engineering Design Manual #212G.—TA Mfg. Co., Engineering Dept., 4607 Alger St., Los Angeles 39, Calif.

CIRCLE 287 ON READER-SERVICE CARD

DISCOVERER RECOVERY Program is summarized in 8-page PIB-52 booklet. —General Electric Co., Missile and Space Vehicle Dept., 3198 Chestnut St., Phila. 1, Pa.

CIRCLE 288 ON READER-SERVICE CARD

HYDRAULIC COMPONENTS. 8-page Bulletin 204 outlines use of hydraulic pumps, motors, and controls in missile ground support.—Denison Engineering Div., American Brake Shoe Co., 1160 Dublin Rd., Columbus 16, Ohio.

CIRCLE 289 ON READER-SERVICE CARD

AIR TRAFFIC CONTROL. 20-page booklet traces development of air navigation and automated controls. General Precision Equipment Corp., 92 Gold St., New York 38, N. Y.

CIRCLE 290 ON READER-SERVICE CARD

CONTROL SYSTEMS. 6-page Bulletin EE-1008 describes electro-mechanical control systems and components for use on production machinery.—Seneca Falls Machine Co., Electronics Div., 12 Fyfe Bldg., Seneca Falls, N. Y.

CIRCLE 291 ON READER-SERVICE CARD

ELECTRG-OPTICAL shutters for speeds up to 10° sec for photographic and electronic instrumentation are described in 2-page leaflet.—Electro-Optical Instruments, Inc., 2612 E. Foothill Blvd. Pasadena Calif.

CIRCLE 292 ON READER-SERVICE CARD

MAGNETIC shield permitting more accurate magnetic testing of materials is described in Data Sheet 153.—Magnetic Shield Div., Perfection Mica Co., 1322 N. Elston Ave., Chicago 23, Ill.

CIRCLE 293 ON READER-SERVICE CARD

TRANSISTORIZED DC POWER FOR FAIL/SAFE OPERATION



Prevents damage to power supply load under any conditions. Unique electronic circuitry monitors output voltage at all times and reduces output voltage and current to nominal zero if output attempts to rise above operating voltage. Of course turn-on and turn-off transients are also eliminated.



CIRCLE 78 ON READER-SERVICE CARD

# **EMPLOYMENT OPPORTUNITIES**

ENGINEERS, SYSTEMS

Immediate Opportunities In These Development & Design Projects

FIRE CONTROL SUB-SYS-TEMS ... including data handling, computers, display, reference and control equipment for shipborne, submarine, and land-based fixed and mobile weapons systems.

DIRECTORS . . . including pedestals, antennas, power drives, servos and computors,

UNDERSEA ORDNANCE . . . torpedoes, mines and their mobile countermeasures (including seawater batteries), propulsion equipment, guidance and associated test and maintenance equipment.

RADAR & RADIO TELE-SCOPE ANTENNAS . . . associated equipment.

INERTIAL GUIDANCE . . . systems and sub-systems for missiles, space vehicles, surface ships, submarines, land survey vehicles, etc.

If you're ready for a career-move in

# **PRECISION ENGINEERING**

you can contribute to the success of General Electric's Ordnance Department

You'll be working in an engineer's department, a new department whose product is manufactured in the mind. You'll be working within a managerial climate that is dedicated to making it easy for you to extend yourself. Small groups, air-conditioned offices are a visible example of this advanced managerial awareness.

You'll be probing sensitive, intricate, and miniaturized inertial navigation systems. Your job will be to generate and apply pioneering technological conceptualization in one or several of the specific problem areas listed below. You will be asked regularly to solve problems lesser men might call impossible. You and your contribution are important at Ordnance.

This is exciting work, and tough. It's for the man who has it and seeks only the opportunity to demonstrate and develop his talent, drive and conceptual capacity.

And your rewards will be commensurate with your contribution. Ample opportunity exists for advancement both within the Ordnance Dept. and throughout General Electric, a company now employing 22,000 engineers, anticipating a need for half again as many halfway through the '60's. Even more important, there's ample room for rapid growth within the salary and responsibility structure of the job you'll first undertake with Ordnance. Full tuition refund is available to you if you work as hard at graduate studies as you will on the job itself.

Ordnance is located in the heart of the Berkshires. Halfway between New York and Boston, the Berkshires is one of the country's great cultural, sport, and recreation centers-a plus you'll find important to a rounded family life, the physical and non-technical mental activity you so seek.

Positions are available to take maximum advantage of abilities and interests at most levels of experience and development.

If you are ready for this kind of move-not just vaguely discontent with what you're now doing—send a brief resume to W. B. Walker, Manager, Professional Relations, Dept. 45-BML.

ORDNANCE DEPARTMENT of the Defense Electronics Division





ELECTRIC

100 Plastics Avenue

Pittsfield, Massachusetts

# MILITARY SYSTEMS DESIGN INDEX TO VOLUME IV, 1960

January-February, (I) March-April, 57-104 (II)

May-June, (III) July-August, (IV)

September-Actober, (V) November-December, (VI)

### SUBJECT INDEX

AC-AC Converter 57 (V)
Accelerometer Amplifier 53 (V)
Accelerometer, High-G 58 (I)
ACDC Solenoid, Midget 47 (I)
A.C. Potentiometer Simplifies Servo
Design 80 (IV)
A-D Converter, Size 15 56 (II)
Adjustable Segment Switch 52 (IV)
Air-Bearing Pump 60 (III)
Airborne Digital Tape System 84 (IV)
Air Navigation System is Multi-function
Marvel 29 (II)
Airbane 129 (II)
Airbane Computer 59 (I)
Alphanumeric Characters on any Cathode Ray Tube 40 (IV)
Amplifiers 49 (VI)
Amplifier, Dual-Channel 32 (VI)
Amplifier, Dual-Channel 32 (VI)
Amplifier, Dual-Channel 32 (VI)
Amplifier, Dual-Channel 48 (I)
Amplifier, Transistor—Scope Deflection
16 (VI)
Amplifier, Transistor—Scope Deflection
16 (VI)
Analog Computers and Long-Range Mis-Coupled 16 (VI)
Ampliffer/Resolver Module 48 (I)
Ampliffer/Resolver Module 48 (I)
Ampliffer, Transistor—Scope Deflection
16 (VI)
Analog Computers and Long-Range Missiles 8 (IV)
Analyzer, Extended Range 48 (VI)
Analyzer, Extended Range 48 (VI)
Analyzer, Extended Range 48 (II)
Angle Counter, Precision 61 (I)
Antenna Fattern Recorder 46 (I)
Antennas Stip Rings 45 (I), 58 (III)
Antennas 18 (IF/7ACAN 62 (V)
Antennas, Large Lightweight 42 (I)
Antennas Ter (III)
Antennas Ter (III)
Antennas Ter (III)
Antennas Ter (III)
Attenuator Diacs 66 (IV)
Attenuator Diacs 66 (IV)
Attenuator, Variable 40 (VI)
Attenuator, Variable 40 (VI)
Attenuator, Variable 40 (VI)
Addio Line Amplifier 51 (IIII)
Audio Line Amplifier 52 (IIII)

Backlash in Instrument Gears 28 (IV)
Balanced Coax Duplexer 50 (II)
Banana Piug Resistors 58 (V)
Band Pass Filters for Telemetering 49
Bearing Assemblies 54 (IV)
Beryllium Compounds in Reactor Applications 50 (III)
Beryllium Gears 47 (I)
Binary Thumbwheel Switch 51 (I)
Binary Thumbwheel Switch 51 (I)
Binsery Thumbwheel Switch 51 (I)
Bilower, Mini Cooling 46 (VI)
Blower Motor 47 (VI)
Blower Motor 47 (VI)
Book Reviews 62 (I), 41 (II)
Bounceless Variable Resistors 27, 70, 83 (IV), 35 (V), 23, 49 (VI)
Broadband Klystrons 49 (II)
Broadband Power Klystron 64 (IV)
Broadband Power Klystron 64 (IV)
Broadband VT Voltmeter 49 (II)
"Building Blocks" Modules for Precision
Timing and Control 18 (II)
Burst Transmission of Digital Combat
Information 36 (IV)
Buships Tube Fittings 55 (I)

Capacitor, Mini Air 44 (VI)
Capacitor Reliability! 0.905 to 10-8 10 (V)
Carbon-Deposited Resistor Characteristics
62 (V)
Carbon-Deposited Resistor Characteristics
63 (V)
Carbon-Deposited Resistor Characteristics
63 (VI)
Cashon Film Resistors 48 (III)
Cashon Film Resistors 48 (III)
Centrifuge Slip Ring 56 (IV)
Ceramic Capacitors 59 (V)
Ceramic Capacitors 59 (V)
Ceramic Capacitors 59 (V)
Ceramic Right Capacitors 44 (III)
Chassis Slide Lock 58 (II)
Character Generator 44 (III)
Chassis Slide Lock 58 (II)
Chopper Rit. Transistor 37 (VI)
Chopper Transformer 57 (II)
Circulator, Strip-Line 39 (VI)
Circulator, Strip-Line 39 (VI)
Circulator, Tee 39 (VI)
Circulator, Strip-Line 39 (VI)
Circulator, Strip-Line 39 (VI)
Circulator, Strip-Line 39 (VI)
Coax Crystal Switch 44 (I)
Coax Perminations 51 (III)
Coax Terminations 51 (III)
Coax Terminations 66 (IV)
Coaxial Connector 48 (V)
Coaxial Connector 48 (V)
Coaxial Connector 48 (V)
Coaxial 2-Way Coupler 62 (V)
Coax-Wareguide Transitron 63 (V)
Command Receiver 45 (I)
Compact Blower 69 (IV)
Compact Blower 69 (IV)
Compact Delay Line 50 (V)
Compact UHF Isolator 44 (III)
Complexed Cables 61 (III)
Component Centrifuge 55 (V)
Computer, Dig. Var. Increment 36 (VI) C

emputer Diodes 40 (III)
emputer/Indicator 56 (II)
emputer to Automate Air Control 29 omputer to Automatical operations of the conductivity Meter 77 (IV) connectors, Aluminum Cable 49 (VI) constant Current Supply 47 (III), 49 Constant Current Supply 47 (III), 49 (III)
Constant Temperatures 69 (IV)
Constant Voltage Transformer 69 (IV)
Control Test Set 53 (II)
Co-Ordinated Mini Components 63 (V)
Counter-Timer, 10MC 45 (III)
Counter, Submersible 47 (VI)
Couplings, Miniature 59 (I)
Critical Milspec Cables 54 (II)
Cryogenic & Fuel Pumps 51 (III)
Cryogenic Relief Valve 48 (I)
Cryostal Case Relay 51 (V)
Current Governor 47 (III)
Current Supply, Constant 45 (VI)
Custom-Bulls Resistors 52 (III)
Custom-Consoles 58 (II)
Custom-Designed Toroids 51 (V)
Custom Multiconductor Cables 73 (IV)

Damping for "White Noise" 12 (III)
DC-DC Converter Design 15 (IV)
DC-DC Voltage Regulators 58 (I)
DC-DC Voltage Regulators 58 (I)
DC-DC Voltage Regulators 58 (II)
DC-DC Gover Supply 77 (IV)
DC Gover Supply 77 (IV)
DC Gover Supply 77 (IV)
DC Supply, Militators 58 (II)
DC Supply, Militators 59 (II)
DC Supply, Militators 40 (IV)
Delay Gover Supply 77 (IV)
Delay Gover Supply 77 (IV)
Delay Gover Supply 77 (IV)
Delay Line, Computer Type 41 (VI)
Delay Line, Utra-Alit 47 (II)
Delay Relay, Mini 59 (IV)
Delay Relay, Sub-Min 56 (I)
Delay Trigger, Variable 59 (IV)
Design for Miniature High Capacity
Ceramic Capacitors 38 (I)
Design for Multiple Connector Features
Missile Reliability 42 (VI)
Diesign for Multiple Connector Features
Missile Reliability 42 (VI)
Diesign for Multiple Connector Features
Missile Reliability 42 (VI)
Diesign for Multiple Connector Features
Missile Reliability 42 (VI)
Diesign for Ministry 51 (I)
Differential Amplifier 51 (I)
Differential Amplifier 51 (I)
Differential Pressure Sensor 44 (II)
Digital Incremass 51 (I)
Digital Incremass 51 (I)
Digital Read-out Ostilosope Simplifies
Measurements 4 (III)
Digital Voltmeter S2 (II)
Digital Voltmeter S2 (II)
Digital Voltmeter Reads Transducers 46
UVI)
Didee Torrentster 58 (IV)
Didee Torrentster 58 (IV)
Didee Torrentster 58 (IV)
Didee Torrentster 58 (IV)
Didee Torrentster 58 (IV) Digital Voltmeter Reads Transducers 46
(VI)
Diode, Mixer 36 (VI)
Diodes Operate at 200° C, New 47 (III)
Disc Thermistor 58 (II)
Disc Thermistor 60 (IV)
Double Armature Motor—A Specialized
Type of D. C. Machine 14 (I)
Drafting Aids 69 (IV)
Dual Ag. Zn Battery 48 (III)
Dual-Coil Magnetic Latching Relay 10
(II)
Dual Coil Valve 57 (III)
Dynamic Balancer 69 (IV)
Dynamotor Replacement 61 (II)

Expanded 35 (II) coated Silicone Bleeving 25 (II)

E

"Fastest" Switching Transistor 39 (Y)
Fast-Switch Long-Dwell Duplexer 61 (Y)
Feedback Potentiometer 52 (III)
Ferrite Components, New 65 (IV)
Ferrite Filter 50 (Y)
Ferrite Switch 65 (IV)
Ferrite Switch 65 (IV)
Field Intensity Meter, Calibrated 54 (VI)

F

Filter Fan 79 (IV)
Flat Cable Connector 72 (IV)
Flexible Couplings 54 (IV)
Flexible Etched Circuitry 51 (II)
Flexible Betched Circuitry 51 (II)
Flexible Waveguide, Large 44 (III)
Floating AC VTVM 69 (IV)
Floating Measurements Easy for AC
VTVM 68 (V)
Flushing Copper Conductors in Printe
Circuits 29 (I)
Flux-Responsive Memory Drum 31 (II)
Flying Spot Seanner CRT 56 (IV)
FM/FM Commutator 54 (II)
FORE Function Measurements Aid Relay Design 62 (II)
400-CPS Standard 44 (III)
400-Cpcition Switch 59 (V)
4-Pin Transistor Holder 62 (IV)
4-Program Pulser 58 (I)
FOUR-Way Versatile Power Supply 71
(IV)
Frequency Converter 57 (IV)
Frequency Synthesizer 46 (III) (IV)
Frequency Converter 57 (IV)
Frequency Synthesizer 46 (II)
Fuel Tubing Couplings 80 (IV)
Functional Components—A
Molecular Electronics 42 (IV)
Fued Sealed Resistor 69 (IV)

Gearhead, Framing Camera 47 (VI)
Gearhead, "Smallest" 59 (II)
Glasses for Near-IR Refractive System
58 (III)
Glass-Fibre Tape Splicer 56 (I)
Graphic Readout Rapidly Evaluates Asalog Computations 20 (IV)
Gun-Mount Glass Rods 61 (II)
Gyro Application in Ballistic Missile
and Space Vehicles 8 (VI)
Gyro Characteristics Fit Job 41 (VI)
Gyro, Rate 32 (VI)
Gyro for Space Guidance Achieves UltraAccuracy 4 (VI)
Gyro is Space Reference, Electrostatic
3 (VI) Achieves Uh
Accuracy 4 (VI)
Gyro is Space Reference, Electrostati
3 (VI)
Gyro Test Console 32 (VI)
Gyro Test, Inertial 32 (VI)
Gyro Test Tables 20 (VI)
Gyro, Unique Vertical 50 (VI)
Gyroscope, the Magnetohydrodynamic
(VI)

G

"Hammer-Blow" Actuator 54 (IV)
Hand Tachometer 52 (IV)
Harmonic Generators 64 (IV)
Heat Detector Cells 64 (V)
Heat Resistant Glass 54 (I)
Heat Switch, Tip-Sensitive 29 (VI)
Hell Kantennas and Reflectors 42 (III)
Hell Kantennas and Reflectors 42 (III)
Hell Kantennas and Reflectors 42 (III)
Hermetic Seal Connectors 45 (V)
Hermetic Terminal 52 (I)
HF Resistor 48 (III)
HF Crystal Filter 58 (IV)
HF Resistor 48 (III)
H-Gain, Hi-Speed Transistor Switch
6 (III)
H-Fower Resistor Decade 70 (IV)
HI-Power Resistor Decade 70 (IV)
HI-Power Resistor Termisstor III
HI-Sensitivity CR Tube 55 (III)
HI-Sensitivity CR Tube 55 (III)
HI-Sensitivity CR Tube 56 (III)
HI-Sensitivity CR Tube 56 (III)
HI-Sensitivity CR Tube 56 (IV)
HI-Power Atlent Fransistor IIII
HI-Sensitivity CR Tube 56 (IV)
HI-Torque Mini Pot 48 (III)
HI-Torque Mini Pot 48 (III)
HI-Torque Mini Pot 48 (III)
HI-Voltage Si Rectifiers 69 (IV)
High Fraquency Scope Tube 55 (IV)
High Power Attenuator 66 (IV)
High Power Attenuator 66 (IV)
High Power Attenuator 66 (IV)
High Precision Potentiemeters 76 (IV)
High Precision Potentiemeters 76 (IV)
High Speed A/D Converter 69 (V)
High Speed Moton Picture is Imported Disgnostic Tool 27 (V)
High Voltage Test Sets 56 (IV)
High Speed Moton Picture is Imported Disgnostic Tool 27 (V)
High Voltage Test Sets 56 (IV)
High Voltage Test Sets 56 (IV)
Hot-Gas Servo Controls Missile 57 (IV)
Hydro Selector Valves 49 (I)

Improving Reliability and Replaceability of Transistorized Systems 32 (IV)
Impulse Relay 72 (IV)
Indicating Switch 60 (V)
Indicator Ampilifier 54 (I)
Indium Antimonide IR Detector Mailable 53 (V)
Inductor Design Data File 43 (III)
Industrial Tube Tester 64 (IV)
Information Flow in a High-Speed Couputer 50 (IV)
Infrared Detectors. Using Rackground puter 50 (IV)
Infrared Detectors, Using Backgrout
Limited 14 (III)
Infrared Filters Have Sharp Cut-On
(VI) In-Line" Data Modular Computer 9 (
spection Microscope 79 (IV)

Insulators, Metalized Ceramic 44 (VI)
Integral Speed Reducers 54 (IV)
Integrated Checkout Equipment for Evaluating Satellite Systems 6 (V)
Isolation Transformer 58 (V)
Isolator, Mini Coav 40 (VI)

Job Tailored Gyro 53 (V) Junction Block 80 (IV)

I) for A

Prin

31 (II

Aid Be

upply

(VI) Byst

1 (VI) res Ultra trostatic

namie

V)

42 (III)

Switch V)

111)

(IV) New Etch

8 (IV) V) thode Ba le 16 (IV Importan

Rockets

le 57 ( or 60 (1

placeabili IV)

(III) peed Con

ackgroun

Cut-On ater 9 (I

(IV)

J

Kilovolt Micro Pack 74 (IV) Klystron Tube Mounts 64 (IV) Klystron/TWT Data File 22 (V)

L

L-Band Components 50 (II)
Leveler Amplifier 49 (I)
Limit Detectors 58 (IV)
Liquid Springs Feature Return Delay
63 (V)
Logle Modules, NOR 37 (VI)
Lo-Speed Tape Unit 60 (V)
Low Frequency Standard 58 (IV)
Low Frequency Vibrations for Qualified
Products Test 60 (VI)
Low-Noise Chapters 48 (II)
Low-Noise Chapters 48 (II)
Low-Noise Circuits Required by New
Choppers 38 (V)
Low Noise Dide 48 (II)
Low-Noise Preamplifier Design 14 (II)

Made-to-Order Wire-Wounds Meet Stringent Mil-Specs 34 (V)
Magnesium Shell Plugs 49 (V)
Magnesium Shell Plugs 49 (V)
Magnesium Shell Plugs 49 (V)
Magnetic Multiplication 54 (I)
Magnetic Bhield 52 (III)
Magnetic Shield 52 (III)
Magnetic Stripe Files, Processing & Updating 24 (VI)
Magnesior Tape Files, Processing & Updating 24 (VI)
Magnetic Visual Control 60 (III)
Magnetic Magnetic Magnetic Millimagnetic Magnetic Magnet M meterless Ultrasonic Unit 65 (V)
Mete-L-Damp Mounts 77 (IV)
Meter-L-Damp Mounts 77 (IV)
Meter-L-Damp Mounts 77 (IV)
Microcircuit Reliability is Design Goal
32 (III)
Microcircuitry—A Practical Technology
for Reliable Microminiaturization 38
(IIII)
Microcircuitry—A Practical Technology
for Reliable Microminiaturization 38
(IIII)
Micro-Miniature Selven, New 21 (V)
Micro-Miniature Adjustable Toroids Tune
Printed Circuits 12 (III)
Micro-Miniature Connector 60 (IIII)
Micro-Miniature Relay, New Reliability
Claimed for 71 (V)
Micro-Miniature Relay, New Reliability
Microwave Breadboard 65 (IV)
Microwave Diodes, Higher Temperature
Thresholds 59 (I)
Microwave Sub-System 63 (IV)
Microwave Sub-System 63 (IV)
Microwave Sub-System 63 (IV)
Minicrowave Tilters 45 (I)
Minitary Combination and Transit Cases
53 (III)
Military Combination and Transit Cases
53 (III)
Military Pressure Switch 60 (IV)
Military Didial Modules 47 (II)
Military Didial Modules 47 (II)
Military Didial Modules 47 (III)
Military Didial Modules 47 (IV)
Mini Gang Potentiometer 59 (IV)
Mini Gang Potentiometer 54 (V)
Mini Gan

Naval Electric Cables 80 (IV)
Nav-Comm Transcoiver 49 (III)
Navy Cable Nomenclature 48 (IV)
Navy's Role in Astronautical Training
Devices 24 (IV)
Need for Microminiaturization, The 4
(III)
Neon Glow Lamps 56 (IV)
New Diffusion Furnace Features Wide
Temperature Profile 22 (IV)
New Firm to Produce Unique Ignitor
Wire 59 (V)
Non-Galling Clutch 53 (IV)
Non-Magnetic Latching Belay 71 (IV)
No-Shaft Fot 58 (II)
Numeric Display Converter 51 (I)
Nylon/Delrin Faris 61 (III)
Nylon/Delrin Faris 61 (III)

One-Shot Primary Battery 60 (II)
Optional Regulation 48 (III)
Ordnance Connectors 73 (IV)
"O" Bing-Seal Valve 49 (I)
Oscillator, Expendable L-Band 62 (V)
Oscillator, Planar Tube 38 (VI)
Oscillator, Subcarrier FM 38 (VI)
Oscillator, Sub-Submin 50 (I)
Oscillator, Sub-Submin 50 (I)
Oscilloscope, Miniature 64 (V)
Oscilloscope, A Pocket Laboratory 49
(VI)

P

Panel Fan Filter Designed for Combat
Conditions 28 (Y)
Parametric Amplifier Design in Radar
Receivers 26 (II)
Partial-Flux Word-Select Core Memory
Technique, The 82 (IV)
P-C Connector 48 (Y)
Permanent Magnet Focusing in 1 KW
Gridded TWT Amplifier 55 (I)
Phase-Angle Voltmeter 56 (I), 56 (Y)
Phase-Lock Discriminator 49 (III)
Photomultiplier Tube 55 (IV)
Photo-Record Timers 46 (II)
Phototransistor Applications 37 (II)
Phototransistor Applications 37 (V)
"Pinhead" Capacitor for Encapsulation
55 (II)
Planar Diode, Very Fast 64 (V)
Plastic Gears 49 (I)
PNP Switch Transistor 51 (II)
Pot, Continuous Rotation 35 (VI)
Pot, Life Predicted by Reliability Ratings 57 (II)
Pot, Life Predicted by Reliability Ratings 57 (II)
Pot, Sub-Min Trimmer 34 (VI)
Pots, Multiung 25 (VI)
Pot, Sub-Min Trimmer 34 (VI)
Pot Taps Resettable 35 (VI)
Pot, Trimmer 34 (VI)
Potentiometer Accelerometer 69 (IV)
Potentiometer Accelerometer 69 (IV)
Power Control Simplified by Mechanical
Amplifier 63 (I)
Power Divider 61 (V)
Power Supply, Regulated 60 (II)
Power Supply, Regulated 60 (II)
Power Transistor, Smaller 52 (II) Power Supply, Regulated 60 (II)
Power Supply, Transistorized-Scope 16
Power Supply, Transistorized-Scope 16
Power Transistor, Smaller 52 (II)
Power Transistor, Smaller 52 (II)
Power Transistor, I (III), 42 (III)
Power Transistors, Paired 53 (II)
Precess Digital Timer 49 (Y)
Precise Digital Timer 49 (Y)
Precise Digital Timer 49 (Y)
Precise Office of the Power Transistor I (III)
Precision Field Test for Gyros 54 (II)
Precision Field Test for Gyros 54 (II)
Precision Jerkmeter 57 (I)
Precision Jerkmeter 57 (I)
Precision Timing System for Tracking
and Control of Missiles 38 (II)
Pressure Calibrator 60 (IV)
Pressure Switch, Mint 61 (IV)
Pressure Switch, Mint 61 (IV)
Pressure Switch, Mint 61 (IV)
Pressure Switch, 1000° F 59 (I)
Pressure Switch, 1000° F 59 (I)
Pressure Switch, 1000° F 59 (I)
Pressure Transducers 61 (II), 60 (IV), 53 (V)
Print-CKT Chopper 52 (IV)
Print-CKT Chopper 52 (IV)
Print-CKT Relay 70 (IV)
Print-CKT Relay 70 (IV)
Print-CKT Relay 70 (IV)
Printed Circuit Cables 52 (III)
Printed Circuit Cables 52 (III)
Printed Circuit Motor 54 (II)
Programming Breadboarding Kit is Versatile Design Ald 20 (V)
Prop Torque Transducer 59 (I)
Prototype P-C Board 69 (III)
Proximity Sensing Head 54 (III)
Pump, Hydrualic 48 (VI)

P

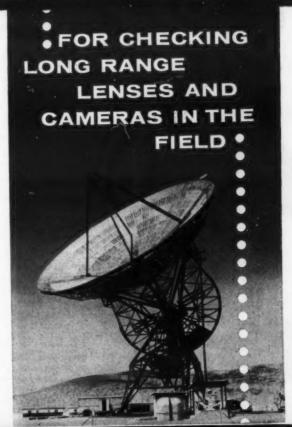
Quartz Load Cell 48 (III)
Quick-Action Clamp 49 (V)
Quick-Connect Coupling Handles Exotic
Jet Fuels 48 (IV)
Quiet Linear Pot 52 (III)

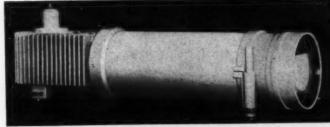
Rack & Panel Pluzs Have Improved Coaxial Inserts 43 (V) Radar Pulse Modulator uses Silicon Di-odes 30 (IV) Radar Pulse Transformer 42 (I) Radar Silip Rings 56 (IV)

Radar Test Unit 63 (V)
Radiation-proof Silicon-Carbide Diodes
Radiaconce Oscillator 49 (II)
Radiaconce Oscillator 49 (II)
Radia Check Valve 64 (V)
Rapid Interference Reduction More Important 24 (II)
Rare Earth & Noble Metals 51 (II)
Rate Gyro, A New Subminiature 28 (III)
Rate Gyro, A New Subminiature 28 (III)
Ratio Transformer 49 (III)
Ratio Transformer 49 (III)
Rescite Rod Serce 55 (V)
Receiver, AM-CW 39 (VI)
Recitifier Assemblies 58 (V)
Regulated Power Modules 58 (V)
Regulated Tentone Rates Cut 13 (I)
Relay, Dioe-Cube 44 (VI)
Relay, Sub-Miniature 55 (I)
Relay, Tubular 44 (VI)
Remote Signal Source 49 (II)
Resistors for Micromodules 61 (IV)
Resistors for Micromodules 61 (IV)
Resolver, Function Error in Computing
Parameter 45 (II)
Resonant Reed Principle has New Applications 42 (II)
Reversible Varactor Diodes 44 (I)
Ref Production Measurements 64 (I)
Reform In Michigal Ref Principle has New Applications 42 (II)
Ref Production Measurements 64 (I)
Reform In Michigal Ref Principle has New Applications 42 (II)
Reference Reduction Measurements 64 (II)
Robot Check-out Technician 53 (I)
Rocket Thrust Measurements 40 (V)
Ruggedized Triode 63 (IV)
Regulated Triode 63 (IV)
Regulated Triode 63 (IV)

Sapphire, Properties of Synthetic 54 (III)
Satellite Data Recorder 53 (II)
Satellite Power Switch 71 (IV)
Satellite Spectrometer is Triumph in Miniaturization 8 (III)
Satellite Spectrometer is Triumph in Miniaturization 8 (III)
Saland Cavitics 45 (I)
Sand Tunnel Diodes 63 (IV)
Scale Meters, Expanded 56 (IV)
Scale Meters, Expanded 50 (IV)
Scale Adjusting Submin Pot 68 (IV)
Scale Adjusting Submin Pot 69 (IV)
Scale Adjusting Submin Pot 68 (IV)
Scale Adjusting Scale For (IV)
Scale Adjusting Scale For

# ZOOMAR SERVICE COLLIMATOR





CHECKING LONG RANGE LENSES AND CAMERAS IN THE FIELD was not possible up to now because the right test equipment was not possible up to now because the right test equipment was missing. A check of infinity setting requires a distant target. This, even if readily available, is often made useless by air turbulence and poor weather conditions, just at a time

when most needed.

THE ZOOMAR SERVICE COLLIMATOR, a portable instrument of appropriate design and resistance to environmental changes, meets the requirements of field use and makes the operator independent of weather conditions. It allows last minute tests in the field with a minimum of effort and a maximum of

FEATURES AND SPECIFICATIONS:

TEATURES AND SPECIFICATIONS:

"Thermax" mounted apochromatic catadioptric system of 150" E.F.

■ Standard U.S. Air Force target (other targets optional)

■ Resolution: 300 lines per mm, therefore, usable on lenses even longer than 200"

■ Micro-adjustable legs for easy set-up.

■ Suitable for selective part coverage for testing lenses of very large diameters.

large diameters

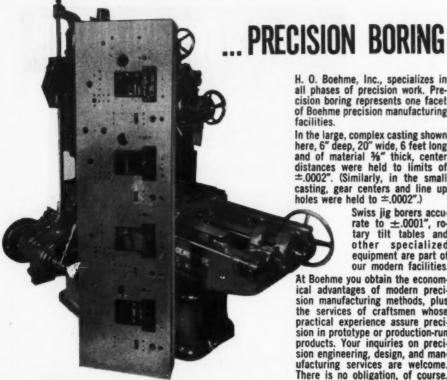
Meight: 10": Width: 61/2" Length: 30"; Weight: 25 lbs.

For prices and descriptive literature contact Dept.: MSD-11-60



ZOOMAR, INC. GLEN COVE, L. I., N. Y. . HOLLYWOOD 28, CALIF.

CIRCLE 79 ON READER-SERVICE CARD



H. O. Boehme, Inc., specializes in all phases of precision work. Precision boring represents one facet of Boehme precision manufacturing

In the large, complex casting shown here, 6" deep, 20" wide, 6 feet long and of material 36" thick, center distances were held to limits of ±.0002". (Similarly, in the small casting, gear centers and line up holes were held to ±.0002".)

Swiss jig borers accurate to ±.0001", rotary tilt tables and other specialized equipment are part of our modern facilities.

At Boehme you obtain the economical advantages of modern precision manufacturing methods, plus the services of craftsmen whose practical experience assure precision in prototype or production-run products. Your inquiries on precision engineering, design, and manufacturing services are welcome. There is no obligation, of course.



Contractors, Designers, Manufactyrers of Precision Electrical, Electro-Mechanical and Electronic Equipment since 1917

915 Broadway New York 10, N.Y.

CIRCLE 80 ON READER-SERVICE CARD



CIRCLE 81 ON READER-SERVICE CARD

Solid State Delay Relay 57 (III)
Solid-State Relay Eastly Modified 61 (V)
Solid State Timers 59 (IV)
Solid Tantalum Capacitor 70 (IV)
Sonar Sounding Set 38 (VI)
Spectrum Analysis Filter 38 (VII)
Spectrum Analysis Filter 38 (VIII)
Spectrum Analysis Filter 30 (III)
Spectrum Analysis Filter 30 (III)
Spectrum Filter 51 (IV)
Sub Trinmer 52 (IV)
Step Attenuator 44 (III)
Strain Gage, Bondable Semiconductor 44
(VIII)
Strain Gage, Bondable Semiconductor 44
Sub-Air Counter 52 (IV)
Sub Ballast Vaire 48 (I)
Sub-Air Discriminator 50 (II)
Sub-Min Counter 55 (IV)
Sub-Min Counter 55 (IV)
Sub-Min Logic Elements 40 (III)
Sub-Min Logic Elements 40 (III)
Sub-Min Logic Elements 40 (III)
Sub-Min Tube, New 40 (III)
Sub-Min Tube, New 40 (III)
Sub-Min Tube, New 40 (III)
Sub-Miniature R-F Connectors Assemble
Anywhere 46 (V)
Surface Transducer Measures ICBM
Temperatures 69 (IV)
Sweep/Signal Oscillator 47 (II)
Switch, Precision Pressure 34 (VI)
Switches, Tab Terminal 49 (VI)
Switches, Tab Terminal 49 (VI)
Synchro Control Transformer 57 (III)
Synchro Test Standard 40 (VI)
Synchro Transmitters 33 (VI)
Synchro Units 52 (VV)
Synchronous Modulator-Demodulator Component 12 (I)
Synchronous Stepping Motor 52 (IV)
Synchronous Stepping Motor 52 (IV) Synchronous Modulator-Demodulator ponent 12 (1) Synchronous Stepping Motor 52 (IV) Synchros, "2-In-1" 54 (V)

Tachometer, High-Temp 59 (I)
Tachometer, DC 34 (VI)
Tachometer, Timer Motor 34 (VI)
Tantalum Capacitors 52 (II), 32 (VI)
Taper Pin Connector 72 (IV)
Taper-Pin Terminals for Printed Circuits 84 (IV)
Taper-Pin Terminals for Printed Circuits 84 (IV)
Taper-Pin Terminals for Printed Circuits 84 (IV)
Taper-Pin Teminals for Printed Circuits 65 (IV)
Taper-Pin Teminals for Produce Multi-Pulse Code 32 (VI)
Telemetres 11 (VI)
Tefino Characteristics, Electronic Specialtics Feature 11 (VI)
Telemetry Discriminator 57 (IV)
Telemetry Discriminator 57 (IV)
Telemetry Biscriminator 57 (IV)
Telemetry Receiver, Versatile 50 (I)
Telemetry Biscriminator 55 (II)
Terminal Choice 56 (I)
Terminal Choice 56 (I)
Terminal Choice 56 (I)
Terminal Boards 48 (VI), 32 (VI)
Test-Certified Relay 50 (V)
Test Chamber, Temperature 41 (VI)
Test Noise Source 48 (II)
Tester, Transistor Beta 26 (VI)
Thermal Shock Chambers 35 (VI)
Thermal Shock Chambers 35 (VI)
Thermal Resistance Measurements 30 (II)
Thermal Switch 60 (IV)
Thermal Switch Tester 60 (IV)
Thermal Valves 52 (III)
Thermocouple Reference 60 (IV)
Thermo

Three Types of Sup Ring Assemblies 27 (III)
Thumbwheel Switch Module 54 (III)
Tilt-Lock Slide 56 (II)
Time Delay Cable 59 (IV)
Time Delay Generator 46 (II)
Time Delay Relay 46 (III), 52 (V)
Time Delay Relays Feature Rapid Ressel 36 (V)
Time Meter 62 (V)
Time Counter 48 (II)
Timing Control Modules 42 (III)
TIMM CIRCUITS—A New Concept 4
(IV)

Timing Control Modules 42 (III)
TIMM CIRCUITS—A New Concept 4
(IV)
Tiny Jack and Plug 61 (II)
Toggles, Indicating 34 (VI)
Toroid Applications Chart 51 (VI)
Toroid Applications Chart 51 (VI)
Toroidal Transformers 46 (III)
Training is Answer to Engineer Shortage 44 (III)
Transducer, Altitude Control 34 (VI)
Transducer, Costilator Unit 58 (IV)
Transducer, Position 33 (VI)
Transducer, Position 33 (VI)
Transducer, Position 33 (VI)
Transitoreres, Linear 33 (VI)
Transitor Circuits—Current Flow and
Voltage Phase Relations 13 (VI)
Transistor Thermal Tester 62 (IV)
Transistor Thermal Tester 62 (IV)
Transistor Thermal Tester 62 (IV)
Transistor Thermal Tester 63 (IV)
Transistor Edgraf Transmitter 45 (III)
Transmitting Antennas 63 (IV)
Transmitting Antennas 63 (IV)
Trimmer Capacitors 47 (IIII)
Trimmer, Quarts Sealeap 44 (VI)
Trimmer, Quarts Sealeap 44 (VI)
Triple Output Delay 59 (IV)

Tuning Fork Standards 48 (II)
Tunnel Diode Curre Tracer 57 (IV)
Tunnel Diode Features Low-Voltage Performance 18 (V)
Tunnel Diode Mass Production 11 (II)
Tunnel Diode Bartes 40 (II)
Turn Count Dial 49 (III)
TV Yoke, New 55 (IV)
Twin-Pin Connector 52 (III)
Two Press-Fit Jacks 48 (V)

U

UHF Missile Diplexer 65 (IV)
UHF Triode Socket 42 (I)
U/L Approval of Teffon Wire Eases
Non-Military Design Problems 67 (V)
Ultra-Precision Selector Switch 19 (III)
Ultrasensitive Pot 67 (IV)
Ultrasensitive Pot 67 (IV)
Ultra-Thin Wire 73 (IV)
Ultra-Thin Wire 74 (IV)
Ultra-Thin Wire 75 (IV)
Ult (IV)
Urethane Materials Meet Urgent Needs
22 (V)
Utility Slide 78 (IV)

TVM, Miniature AC 38 (VI)
Fans Axial Blower 60 (III)
Fans Axial Fan 59 (II)
Fariable Attenuator 66 (IV)
Fibration and Shock Control 53
Fibration Test, Portable 42 (VI)
Fibrator Control, Random 43 (VI)
Foliage Reference Standard 50
Voltage Regulator 46 (VI) 53 (III) (V)

Chemallo
Chicago
54 (II
Christie
Christie,
Cicoil Ci
Cinch M
Cincinna
Circle St
Clare &
Clarosta:
Clarosta:
Clifton

Clevite Clifton (V),
Cobehn,
Cohn Co
Cole Ele
Collins (VI)

Color-Li olu**mb**ia om**bina** Compone Compute (II)

Compute
67 (IV
Con-Elec
Connecte
Consolid
(II)
Consolid

Consolid
(II)
Consolid
(III)
Cons. R
Control
Consolid

Control
7 (II)
(VI)
Control
Convair
Cook Ba
Cook, D
Coors P
Corning
Couch O
Courter
Crescent
(III)

Dage E. DataTaj Daystro.
54 (V Deitzler DeJur-Loelco H Delta I Deltime De Mor Designe Dialigh Dial Se

Duncan (V) Durant (VI)

Edipse Edeliff Edison (V) Edmun

Edmun Eichen EI Lat Electri Electri Electri Electri (V) Electro (III

Electric Electric Electric Electric Electric Electric Electric Empire E.M.T. Engine

lover

Waveguide Filters 65 (IV)
Waveguide Scals 78 (IV)
Waveguide System, Low-Loss 56 (I)
Waveguide System, Low-Loss 56 (I)

X

X-band Variable Delay Line 46 (III) X-Radiation Generator 51 (III)

### BOOKS TITLE

Aerodynamics of Powered Flight, The 27 (IV)
Coupled Mode and Parametric Electronics 28 (V)
Directory of Firms, Their Buyers and Specifying Engineers 27 (IV)
Electronagnetic Energy Transmission and Rediation 23 (VI)
Electronagnetic Energy Transmission and Rediation 23 (VI)
Electronagnetic Fields, Energy, and Electromagnetic Energy, and Electromagnetic Physics 35 (VI)
Encyclopedic Dictionary of Electronics and Nuclear Engineering, An 63 (I)
Forces 41 (II)
Guide to the Bpace Age 41 (II)
Linear Noisy Networks, Circuit Theory of 23 (VI)
Modern Network Synthesis, Intro. to 49 (VI)
Quality Control Manual for Printed Circuit Boards and Board Assemblies 27 (IV)
RCA Receiving Tube Manual, RC-29 83 Quality Control Manual for Francoucuit Boards and Board Assemblies 27 (IV)
RCA Receiving Tube Manual, RC-20 83 (IV)
Rocket Propellant Handbook 35 (V)
Siliton Rectifier Handbook 63 (I)
Statistical Processes and Reliability Engineering 35 (V)
Subministure Rate Gyroscopes 62 (I)
Systems Preliminary Design 27 (IV)
Theory of Inertial Guidance 83 (IV)
Transistor Manual 49 (VI)

### BOOKS AUTHORS

Adler, R. B. 41 (II), 23 (VI) Audio Devices, Inc. 63 (I) Bell, D. A. 35 (V) Besserer, C. W. 41 (II) Besserer, Hazel 41 (II) Carroll, Robert L. 27 (IV) Chorafas, Dimitras N. 35 (V) Chu, L. J. 41 (II), 23 (VI) Electron Tube Div., BCA 83 (IV) Evered, Douglas S. 35 (V) Fano, R. M. 41 (II), 23 (VI) Haus, H. A. 23 (VI) Industrial Div., Bureau of Engraving Inc. 27 (IV) Industries Publishing Company 27 (IV) Jerger, Joseph J. 27 (IV) Kit, Boris 35 (V) Livehant, S. E. 35 (V) Louisell, W. H. 23 (VI) Lowry, H. R. 49 (VI) McClure, Connie L. 83 (IV) Sanders Associates, Inc. 62 (I) Sarbacher, Robert I. 63 (I) Van Valkenburg, M. E. 49 (VI)

## AUTHOR INDEX

A

Abacus, Inc. 37 (VI)
ACDC Electronics. Inc. 58 (V)
ACE Electronics Assoc., Inc. 35 (VI)
ACE Electronics Assoc., Inc. 35 (VI)
ACUSTAN ACOUNTY
A

Allegany Inst. Co., Inc. 48 (III)
Allen Act Inst. Div. 53 (V), 32, 41
(VI)
Allen Avionics, Inc. 59 (IV)
Allen Business Machines, Inc., R. C.
53 (V)
Alliogs Unilmited 52 (III)
Alpha Wire Corp. 73 (IV)
Amoc Engrg. Co. 78 (IV)
Amore Engrg. Co. 78 (IV)
American Electronics, Inc. 30 (III)
American Electronics, Inc. 30 (III)
American Engla Corp. 80 (III)
American Engla Corp. 80 (IV)
Amorican-Marietta Co. 60 (III)
AMP Inc. 37 (III), 42 (V)
Amphenol-Borg Electronics Corp. 49 (III)
Ander Instruments Inc. 58 (IV)
Anders Instruments Inc. 58 (IV)
Anders Instruments Inc. 58 (IV)
Anders Corp. 42 (I)
Antenna & Radome Research Assoc. 66
(IV)
Aries Labs., Inc. 79 (IV)
Armament Div. 63 (I)
Associated Research, Inc. 60 (I), 49 (III),
56 (IV)
Astromics Div. 71 (IV), 53 (V)
Astroxystems, Inc. 40 (VI)
Atlantis Electronics Corp. 49 (II)
Atlantis Fowder Co. 53 (II)
Atlee Corp. 47 (IIII)
Atohm Electronics, 34 (VI)
Aviron Mfg., Inc. 53 (II)
Aviron Mfg., Inc. 53 (II)

Babcock Badio Engineering, Inc. 45 (1)
Babcock Relays, Inc. 48 (III)
Barber-Coleman Co. 56 (III)
Barker & Williamson, Inc. 46 (III)
Barker & Williamson, Inc. 46 (III)
Barton Instrument Corp. 44 (III)
Bausch & Lomb Outleal Co. 58 (III)
Becker Electronics Mfg. Corp. 40 (III)
Becker Electronics Mfg. Corp. 40 (III)
Beckunan Instruments, Inc. 33, 52 (I), 4
(III) (III)
Beker, Andrew 14 (I)
Bell Telephone Laboratories 7 (VI)
Bendix Aviation Corp. 12, 50 (I),
(II), 56 (III), 50 (IV), 54 (IV),

8

(II), 56 (III), 50 (IV), 54 (IV), (IV)

Bendix-Pacific Div, 50 (I), 55 (II)

Bentlay-Harris Mfg. Co. 25 (II)

Bently Scientific Co. 54 (III)

Berg, Winfred M. 28 (IV)

Berkely Div, 45 (III)

Bethlehem Apparatus Co. 30 (I)

Biddle Co., James G. 42 (II)

Bitcher Corp. 62 (IV)

BJ Electronics 46 (III)

Bogart Mfg. Corp. 43 (III)

Bomac Laboratories, Inc. 50 (II), (IV), 61 (V), 63 (V)

Bomar Instrument Corp. 54 (IV)

Borg Equipment Div. 49 (III)

Borg-Warner Corp. 46 (III)

Bouras, Inc. 7 (IIII), 52 (IIII), 34 (IV)

Rowmar Instrument Corp. 59 (III), (IVI)

(VI)
Bracke-Selb X-ray Co. 51 (III)
Bradley Semiconductor Corp. 58 (V)
Breasley Semiconductor Corp. 58 (V)
Breese Corps. Inc. 57 (II), 27 (III)
Brooks Corps. Inc. 28 (II)
Brooks & Perkins, Inc. 28 (II)
Brunell & Co., Inc. 12 (II), 51 (VI)
Bruh Inst. Div. 20 (IV)
Bruh Inst. Div. 20 (IV)
By-Buk Co. 69 (IV)

Cable Designs, Inc. 61 (II)
Cannon Electric Co. 48 (V), 49 (V)
Carter Mfg. Corp. 67 (IV)
Carter Bob 33 (I)
CBS Electronics S3 (II), 55 (IV),
(IV)
Centralab Div. 48 (III), 70 (IV)
C68 Laboratories, Inc. 45 (I), 47 (B
C68 (V), 62 (V)
Chassis-Trak, Inc. 56 (II), 78 (IV)
Chassis-Trak, Inc. 56 (II), 78 (IV)
Chatham Controls Corp. 60 (IV)

MILITARY SYSTEMS DESIGN

cemalloy Electronics Corp. 44 (1)
cleage Dynamic Industries, Inc. 51 (I),
54 (III), 59 (V)
dristle Electric Corp. 57 (V)
dristle, C. B. 18 (IV)
coll Corp. 72 (IV), 70 (V)
coll Corp. 84 (V), 51 (V)
coll Corp. 48 (III)
coll Corp. 84 (III), 70 (IV)
coll Corp. 85 (IV)
coll Corp. 85 (IV)
coll Electric Co. 58 (IV), 50 (V), 45
coll Corp. 81 (IV)
coll Corp. 81 (IV)
coll Corp. 81 (IV), 50 (V), 45
coll Corp. 81 (IV), 50 (V), 45
coll Corp. 81 (IV), 50 (V), 45
coll Corp. 81 (IV), 61 (IV)
coll Corp. 81 (IV), 61 (IV)

(III)

(V)

(I)

(III)

V)

27 (1

III) 58 (III 40 (III 52 (I), 4

VI) i0 (I), i (IV), 55 (

I)

(II).

1), 34 (II),

(V) 8 (V) 27 (III

(II) 51 (VI)

. 49 (V)

49 (V)

15 (IV),

(V) 1), 47

(IV)

ESIGN

(VI)
Collins Corp., G. L. 49 (III)
Collins Corp., G. L. 49 (III)
Color-Lite Div. 50 (V)
Columbia Technical Corp. 59 (IV)
Combination Pump Valve Co. 47 (IV)
Components Corp. 43 (III)
Computer Control Co., Inc. 54 (I), 47 (II)
Computer Instruments Corp. 56 (II),
67 (IV)
Con-Elco 81 (IV)
Connector Seals Corp. 45 (V)
Consolidated Controls Corp. 59 (I), 31
(II), 60 (IV)
Consolidated Electrodynamics Corp. 53 Consolidated Electrodynamics (II)
Consolidated Reactive Metals, Inc. 51

(II)
Consolidated Electrodynamics Cosp. 55
(III)
Consolidated Reactive Metals, Inc. 51
(III)
Cons. Resistance Co. of Am., Inc. 58 (V)
Control Dynamics Corp. 71 (V)
Consolidated Systems Corp. 8 (III)
Control Electronics Co., Inc. 50 (I),
7 (II), 47 (III), 57 (IIII), 59 (IV), 41
(VI)
Control Products, Inc. 60 (IV), 29 (VI)
Convair Instruments Div. 67 (IV)
Cook Dr. Neal A. 10 (VI)
Cook Dr. Neal A. 10 (VII)
Corning Glass Works 69 (IV)
Courter Products Div. 56 (II)
Crescent Engineering & Research Co. 13
(IIII)

Crescent Engineering & Researc (III) Crouse-Hinds Co. 49 (V) CTS Corp. 35 (VI) Cubic Corp. 62 (V) Cutis Dev. & Mfg. Co. 80 (IV)

D

Dage Electric Co., Inc. 48 (V)
DataTape Div. 53 (II)
Daystrom, Inc. 36 (II), 56 (IV), 68 (IV),
54 (V)
Deitzler, Richard P. 14 (II)
Delur-Amsco Corp. 72 (IV)
Delco Radio Div. 41 (III)
Delta Design, Inc. 43 (II), 35 (VI)
Deltine Inc. 50 (V)
De Mornay-Bonardi 64 (IV)
Designers for Industry, Inc. 44 (III)
Dialight Corp. 44 (IV)
Dial Service & Mfg. Inc. 11 (III)
Dickens, Wray D. 6 (V)
Don-Lan Electronics Inc. 40 (VI)
Donner Scientific Co. 57 (I)
Dorsett Electronics Labs 38 (VI)
Dressen-Barnes Corp. 57 (IIII), 76 (IV)
Du Mont Labs., Inc., Allen B. 4, 55 (II),
55 (IV), 56 (IV), 37 (V)
Ducan Electronics, Inc. 76 (IV), 52 (V)
Durant Mfg. Co. 53 (IV), 55 (IV), 47 (VI)
Dynamic Devices, Inc. 69 (IV)
Dynamic Gear Co., Inc. 56 (III), 53 (IV), Dynamic Devices, Inc. 69 (IV) Dynamic Gear Co., Inc. 56 (II), 53 (IV), 54 (IV) Dynamic Core.

Dynamics Corp. of America 69 (IV) Dynatron Labs. 62 (IV)

E Eclipse-Pioneer Div. 54 (IV) Edeliff Instruments 52 (III) Edison Industries, Thomas A. 80 (IV), 30 Edison Industries, Thomas A. 80 (IV), 30 (V)

(V)

Edison Industries, Thomas A. 80 (IV), 30 (V)

Elchonauer, Jr., C. J. 4 (I)

El Labs, Div. 64 (V)

Elco Corp. 72 (IV), 44 (V), 49 (V)

Elco Corp. 72 (IV), 44 (V), 49 (V)

Electra Mg. Co. 70 (IV)

Electrie Hotpack Co. The 42 (VI)

Electrie Hotpack Co. The 42 (VI)

Electrie Regulator Corp. 59 (III)

Electrie Regulator Corp. 59 (III)

Electrie Regulator Corp. 58 (IV), 54 (V), 16, 48 (VI)

Electrol Corp. 58 (VI)

Electronie Communications. Inc. 49 (III), 58 (IV)

Electronie Seals, Inc. 73 (IV)

Electronie Seals, Inc. 73 (IV)

Electronie Transistors Corp. 42 (III)

Electron Escals, Inc. 73 (IV), 60 (V)

Electronie Transistors Corp. 42 (III)

Electro Switch Corp. 58 (III), 56 (IV)

Electronie Transistors Corp. 41 (III)

Electro Switch Corp. 58 (III), 56 (IV)

Electronie Corp. 19 (III)

Elgin National Watch Co. 74 (IV)

Empire Devices Products Corp. 44 (III)

EMPIRE Devi

Fairchild Controls Corp. 61 (II), 28 (III), 4 (V)
Fairchild Semiconductor Corp. 64 (V)
Failon, William K. 8 (IV)

Falstrom Co. 58 (II)
Fecker, Inc., J. W. 20 (IV)
Fenwal Electronics, Inc., 28 (VI)
Ferrotec, Inc. 65 (IV)
Fien & Schwerin, Inc. 52 (III)
Filmohn Corp. 52 (III)
Fischer, Herbert L. 18 (II)
Flite-Tronics, Inc. 51 (III)
Flite Begulators, Inc. 65 (V)
Fortini, M. M. 20 (III)
Franklin Systems, Inc. 40 (III)
Freed Transformer Co., Inc. 69 (IV)
FXR, Inc. 62 (V)

Gamah Corp. 80 (IV)
Gamewell Co. 67 (IV)
Garlock Electronic Prod. 35 (VI)
General Communications 38 (VI)
General Devices, Inc. 61 (I)
General Dynamics Corp. 67 (IV)
General Electric Co. 4, 57 (I), 14 (II),
4, 21 (III), 64 (IV), 3 (VI)
General Electronic Laboratories, Inc. 50
(I)

Instrument Corp. 47 (III), 55 69 (IV)
Magnetic Corp. 30 (VI)
Magnetics, Inc. 54 (I)
Motors Corp. 41 (III)
Phones Corp. 52 (II)
Precision Equipment Corp. 29 General Precision.

(III)
General Precision, Inc. 8 (1),
General Precision, Inc. 8 (1),
General Radio Co. 53 (IV)
General Radio Co. 53 (IV)
General Tel. & Electronics Corp. 63
General Tel. & Electronics Corp. 63

General Tel. & Electronics Corp. 63
(IV)
General Time Corp. 51 (I)
General Transistor Corp. 11 (II), 37
(II), 15 (V)
Genisco, Inc. 14 (I), 43 (VI)
Globe Industries, Inc. 59 (I), 60 (III)
Globe-Union, Inc. 48 (III), 70 (IV)
Gore & Associates, Inc., W. L. 52 (III)
Grand Sliding Mechanisms, Inc. 58 (II)
Grant Pulley & Hardware Corp. 78 (IV)
Great Lakes Mfg. Corp. 63 (III), 76 (IV)
Griffin, Sam 8 (III)
Guardian Electric Mfg. Co. 47 (I), 72
(IV)
Guidance Controls Corp. 46 (I), 52 (IV) (IV)
Guidance Controls Corp. 46 (I), 52 (IV),
55 (V)
G-V Controls, Inc. 36 (V)
Gyrex Corp. 67 (I), 52 (V), 55 (V)

Haloid Xerox, Inc. 21 (V)
Hammerton, J. C. 24 (VI)
Handley, Inc. 52 (I), 68 (IV), 34 (VI)
Hardley, Inc. 52 (I), 68 (IV), 34 (VI)
Harvard Industries, Inc. 45 (I)
Harvard Industries, Inc. 45 (II)
Hardles, C. E. 13 (IV)
Harvey-Wells Elex, Inc. 40 (VI)
Hass Instrument Corp. 60 (IV)
Hathaway Instrument, Inc. 46 (II)
Helitz, Inc., Karl 46 (II)
Helitz, Inc., Karl 46 (II)
Herons Electronics Corp. 40 (VI)
Hermes Electronics Corp. 40 (VI)
Herwald, Dr. S. W. 42 (IV)
Hi-G, Inc. 44 (VI)
Hi-Q Div. 38 (I), 33 (II), 8, 48 (III), 62 (V)
Hi-Spec Electronics Corp. 50 (V)
Hoffman Electronics Corp. 30 (III), 40 (III), 18, 65 (V)
Hood, II, Chas. N. 14 (VI)
Houston Fearless Div. 62 (V)
Howell Instruments, Inc. 46 (VI)
Hughes Aircraft Co. 55 (I), 14, 51 (II), 65 (IV)
Humphrey, Paul 38 (III) H 65 (IV)

Humphrey, Inc. 37 (VI)

Hurney, Paul 85 (II)

Hurney, Paul 85 (II)

Hurney, Paul 85 (II)

Hydra-Rore 10, 59 (VI)

Hydra-Rore Corp. 49 (I), 54 (IV)

Hydra-Aire Co. 57 (III)

Hydra-Rore Corp. 51 (III)

Hytech Corp. 55 (VI)

ime Magnetics Corp. 33 (VI)
Inconiz. Inc. 58 (I)
Industrial Electronic Engineers, Inc. 50 (II), 55 (IV)
Industrial Instruments, Inc. 46 (III), 77 (IV)
Industrial Timer Corp. 48 (II)
Industrial Timer Corp. 48 (II)
Intertial Switch, Inc. 35 (VI)
Infrared Standard Lab. 49 (II)
Instrument Corp. 67 Florida 48 (II)
Instrument Development Labs., Inc. 50 (II), 54 (II)
Instrument Industry, Inc. 42 (II)
International Resistance Co. 51 (II), 32 (III), 60 (IV)
Int. Rectifier Co. 20 (III)
International Tel. & Tel. Corp. 49 (III), 12 (IV)
Iron Fireman Mfg. Co. 50 (VI) 1 Iron Fireman Mfg. Co. 50 (VI)

Jack & Heintz, Inc. 48 (IV)
James Electronics Inc. 48 (II), 52 (IV)
James, Pond & Clark, Inc. 48 (II)
Jettron Products, Inc. 63 (IV)
JFD Electronics Corp. 44 (VI)
Johanson Mfg, Corp. 44 (VI)
Johanson Mfg, Corp. 45 (VI)
Jordan Electronics Co. 52 (V)

J

Kaestner, Paul 40 (VI)
Kaufman Glass Co. 54 (I)
Kearfott Div. 8 (I), 56 (II). 52 (IV).
38, 47 (VI)
Kelvin Electric Co. 59 (V)
Kennedy Co. 58 (IV)
Kerstone Electronics Co. 58 (IV)
Kinetic Instrument Corp. 46 (I)
Kinetics Corp. 57 (II), 71 (IV)
King Electronics, Inc. 59 (V)
King Electronics, Inc. 59 (V)
King Electronics, Inc. 59 (V)
King Radio Corp. 49 (III)
Kistler Instrument Corp. 48 (III)
Kooltronic Fan Co. 75 (IV)
Kulka Electric Corp. 56 (I), 84 (IV)

L L. A. B. Corp. 60 (V)
Lab. for Electronics 29 (11)
Lansdale Div. 34 (III), 39 (V), 36 (VI)
Larson, Larry G. 6 (V)
Leach Corp. 61 (V)
Leemath, Inc. 47 (1)
Leonard, Inc. Wallace 34 (VI)
Lerce Electronics, Inc. 59 (V)
Ling.-Altee, Inc. 63 (IV)
Liton Industries 49 (II), 64 (IV)
Lord Mfg. Co. 12 (III)
Lower, Jack W. 4 (VI)
Lundey Associates 52 (I)

Magnetic Amplifiers, Inc. 60 (I)
Magnetic Research Corp. 57 (IV)
Magnetic Shield Div. 52 (III)
Magnetics, Inc. 13, 15 (IV)
Mannets, Inc. 13, 15 (IV)
Mannets, Inc. 13, 15 (IV)
Mannets, Inc. 14 (IV)
Mannets, Inc. 14 (IV)
Mannets, Inc. 16 (II)
Mannets Valve Corp. 48 (I), 57 (III),
72 (IV), 64 (V)
Marstan Electronics Corp. 57 (III)
Martin Sweets Co. 63 (III)
Mason-Neilan Div. 24 (I)
Mast Development Co. 61 (I)
Masterials Electronic Prod. Corp. 24 (II)
Masterials Electronic Prod. Corp. 24 (II)
MBE Electronics 52 (VI)
MBE Electronics 52 (VI)
MBE Electronics 53 (VI)
Mechatrol Div. 34 (III)
Melpar, Inc. 16 (IV)
Memory Memory Inc. 16 (IV)
Memory Memory Inc. 16 (IV)
Merel, Wolf 13 (I)
Merrimac Research & Development, Inc. 63 (IV)
Metalls & Controls Div. 52 (III)
Methods Research Corp. 60 (III)
Metrolab Corp. 77 (IV)
Micro Balancing, Inc. 69 (IV)
Micro-Systems, Inc. 4 (III)
Micro-Systems, Inc. 40 (III)
Microwave Electronics Corp. 49 (VI)
Minneapolis-Honeywell Regulator Co. 54 (III)
Microwave Electronics Corp. 49 (VI)
Microwave Electronics Corp. 49 (VI)
Microwave Electronics Corp. 49 (VI)
Microwave Chemicals Lab., Inc. 44 (III)
Microwave Chemicals Lab., Inc. 44 (III)
Microwave Chemicals Corp. 71 (IV), 53 (V)
Moolay Chemical Co. 22 (V)
Monlor Systems, Inc. 22 (II)
Moutools, Inc. 51 (III), 44 (III), 57 (IV)
Mullenbach Div. 47 (VI)
Mullenbach Div. 47 (VI)
Mullenbach Div. 47 (VI)
Mullenbach Div. 47 (VI)
Muller, Geo. J. 29 (I)

no Products 69 (IV) Controls, Inc. 47 (I) Engineering Co, Inc. 56 (II), 59 Nacime Products 69 (IV)
Nash Controls, Inc. 47 (I)
Natel Engineering Co, Inc. 56 (II), 59
(IV)
National Connector Corp. 48 (VI)
National Semiconductor Corp. 60 (I), 36
(II) (III)
Naugler Engrg., Inc. 54 (IV)
Neff Instrument Corp. 51 (I)
Nems-Clarke Co. 39 (VI)
New Hampshire Ball Bearings, Inc. 54 Neif Instrument Corp. 51 (1)
Nems-Clarke Co. 39 (VI)
New Hampshire Ball Bearings, Inc. 54
(IV)
Norden Div. 52 (V), 54 (V)
Normandy Electric Wire Corp. 48 (IV)
North Atlantic Industries, Inc. 56 (I),
53 (II), 56
Si (II)
North Hills Electronics, Inc. 63 (IV),
60
Si (V)
Northrup Corporation 8 (VI)
Nuclear Electronics Corp. 49 (II)
Nylomatic Corp. 51 (III)
Nylomatic Corp. 61 (III)
Nytronics, Inc. 52 (I), 70 (IV)

Ohmite Mfg. Co. 61 (IV)
Optimized Devices, Inc. 62 (IV), 28 (V)
Orion Electronics Corp. 41 (VI)
Osborne Electronic Sales Corp. 57 (V)
Oster Mfg. Co., John 47 (I), 57 (III),
52 (IV), 54 (V), 34 (VI)
Ott, Paul W. 8 (VI)
Owens, Harry L. 4 (III)

# **BEATTIE-COLEMAN** PROGRAMER OFFERS

# **4 HOUR PROGRAM ON 13 CHANNELS**

Reliability of the Beattie-Coleman MLPR-13 Programer has been thoroughly proved in numerous successful missile applications and in rigorous laboratory tests. This precision instrument offers these important features:

- 13 channels.
- Not affected by magnetic fields.
- Controls programs up to 4 hrs. 42 mins, duration.
- Accommodates 160 ft. of punched 35mm Cronar tape.
- Available in 8 tape speeds. · Tapes quickly changed for varying programs.
- · Compact, light weight.
- Timing accuracy: Repeatability ±0.05%.
- Temperature: 0° to 65°C. Other models to fit your needs. Write for catalogs.



BEATTIE-COLEMAN INC.

1012 N. Olive Street, Anaheim, Calif. • Branch: 437 Fifth Ave., New York, N.Y. CIRCLE 82 ON READER-SERVICE CARD



# FEATURES

- Rated residual SWR under 1.010; rated error in detected signal —
- Several models covering various bands from 50 to 4000 mc.
- Engraved scales and verniers permit one to read the probe position to 0.01 centimeters.
- Optional accessory: a rack and pinion carriage drive than can be engaged or disengaged at will.
- · Precision tapered reducers are available for use in making accurate measurements in a wide range of rigid and flexible coaxial transmission

Write for complete information on AMCI Slotted Lines.



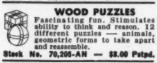
CIRCLE 83 ON READER-SERVICE CARD



ORDER BY STOCK NO. . CHECK-M.O. . SATISFACTION OR MONEY BACK 6X POCKET COMPARATOR 50-150-300X MICROSCOPE Amazing Value!

3 Achromatic objective lenses on revolving turret! Imported, Fine rack and pinion focusing.

Use to check layouts, ma-chining on tools, dies, gauges, threads, chamfers, etc. Measures angles, radii, circles, linear in both deci-mal inches & millimeters. 生毒者 Stock No. 30,081-AN - \$19.50 Petpd.



CRYSTAL GROWING KIT ick No. 70,836-AN - \$9.50 Patpd.

1,000 LB. ROPE HOIST Extra heavy duty — uses 24 ft. long 3/2" rope. Steel swivel hooks, roller bearings and steel rope lock — holds in any position. 1,000 lbs. capacity. Stock No. 70,316-AN-\$5.00 Pstpd.

SCIENCE TREASURE CHESTS For Boys, Girls, Adults! Excellent Science Fair Project Material!



DE LUXE CHEST . . Everything in Chest above plus exciting additional items for more advanced experiments.

Stock No. 78,343-AN — \$10.00 Pstpd.

Stock Nos Stock Nos.

30,349-AN — Earrings ...\$2,75 Ppd.
30,350-AN — Cuff Links ..\$2,75 Ppd.
30,372-AN — Pendant ...\$2,75 Ppd.
30,390-AN — Tie Clasp ...\$2,75 Ppd.

Steek No. 70,008-AN \$14.95 Patpd.

BARGAINI 3" ASTRONOMICAL

TELESCOPE . . . 60 TO 180X
See stars, moon, planets close-up. Famous Mt. Palomar reflecting type. Equatorial mount; finder telescope; hard-wood tripped. "Star Chart", "Hand Book of Heavens" plus directions included free.

Stock No. 85.050-AN - \$29.95 Pstpd.

ANALOG COMPUTER KIT

Used for multiplication, division, powers, roots, logs, trig, physics. Easy screw-driver assembly.

Stock No. 70,341-AN — \$14.95 Pstpd.

GRATING JEWELRY

A dazzling rainbow of color. Just as a prism breaks up light into full range of spec-trum colors, so does Diffrac-tion Grating.

CIRCULAR DIFFRACTION

FREE! Write for Giant 'CATALOG AN 144 pages! Over 1,000 Bargains!
SCIENCE • MATH • OPTICS
For industry, hobbylsts, etc.!

EDMUND SCIENTIFIC CO., Barrington, N. J.

CIRCLE 84 ON READER-SERVICE CARD

# ROTARY SWITCHES

- For Critical Reliability Applications.
- · Quick changing of programs, configurations, circuits.
- Maintenance problems completely eliminated by unique 5-second wafer replacement models.



11/4" x 11/2" Retary Selector Switch, Series RS15.
Manually (illustrated), motor or colenoid



21/2" x 23/2" Rotary Selector Switch, Series RS21.
Solenoid , manually or motor operated.



3" x 2½" Retary Selecter Switch, Series RS30. Manually (illustrated), solenoid or motor operated.



CHICAGO DYNAMIC INDUSTRIES, Inc.

(DI) PRECISION PRODUCTS DIVISION 1725 Diversey Blvd., Chicago 14, Illinois Phone: WEllington 5-4600

CIRCLE 85 ON READER-SERVICE CARD

Pacific Automation Products, Inc. 77

(IV)
Pamar Electronics Co. 61 (IV)
Pamar Electronics Co. 61 (IV)
Pamoranic Radio Products, Inc. 46 (III)
Parker Fittings & Hose Div. 55 (I)
Parker Fittings & Hose Div. 55 (I)
Parker Beal Co. 73 (IV)
Percent Glebra E. 22 (I)
Penne Engr. & Mig. Corp. 61 (III)
Perfection Mics Co. 52 (III)
Performance Measurements Co. 59 (I)
Perdin-Elmer Corp. 61 (III), 80 (IV)
Pittin-Elmer Corp. 61 (III), 80 (IV)
Pittin-Elmer Corp. 61 (III), 83 (IV)
Pittin-Elmer Corp. 74 (III)
Philadelphia Scientific Glass Co. 50 (V)
Philoc Corp. 26 (II)
Philadelphia Scientific Glass Co. 50 (V)
Pittin-Electronics, Inc. 14 (V)
Pitto Design Corp. 61 (IIII), 83 (V)
Pierce, Donald E. 20 (IV)
Polarad Electronics Corp. 72 (IV), 63 (V), 54 (VI)
Power Sources, Inc. 60 (II)
Power Sources, Inc. 60 (II)
Precision Connector Inc. 73 (IV)
Precision Connector Inc. 73 (IV)
Precision Scientific Co. 69 (IV)
Precision Scientific Co. 69 (IV)
Probascope Co., Inc. 50 (I), 48 (VI)
Probascope Co., Inc. 50 (I), 48 (VI)
Profotopy Transformer Co., 31 (IV)
Power Designs, Inc. 79 (IV)
Pyrofuze Corp. 59 (V)

Quan-Tech Labs 45 (II), 47 (III), 45 (VI)

R

Radar Design Corp. 51 (II), 43 (III), 66 (IV)
Radar Relay, Inc. 55 (IV)
Radiation Electronics Co. 42 (III)
Radiation, Inc. 43 (III)
Radio Corp. of America 49 (II), 40 (III) (III)
Ramm Rectifier Co. 42 (VI)
Ramme Rectifier Co. 41 (IV)
Rantec Corp. 65 (IV), 61 (V)
Rapide Electric Co. 41 (I)
Raytheon Mrg. Co. 43 (I), 49 (II),
42 (III), 58 (IV), 69 (V), 38 (VI)
Red Bank Div. 65 (IV)
Reeves Instrument Corp. 59 (IV)
Regulators, Inc. 60 (IV)
Republic Aviation Corp. 53 (I)
Rescon Electronics Corp. 62 (IV)
Resistance Prod. Co. 46 (VI)
Rex Corp. 49 (I)
Rheem Bemiconductor Corp. 49 (III), 40
(III)

Reem Semiconductor Corp.

(IIF)

RLC Electronics, Inc. 66 (IV)

Robinson Technical Products Inc. 53

(III), 77 (IV)

Rose, Leonard J. 30 (II)

Rotary Devices Corp. 45 (I)

Rototest Labs, Inc. 42 (VI)

Rototest Labs, Inc. 42 (VI)

Royal McBee Corp. 9 (II)

Rutherford Electronics Co. 32 (V)

5 Sanders Associates, Inc. 50 (II), 65 (IV) Scientific-Atlanta, Inc. 46 (I), 49 (II), 63 (IV), 33 (VI) Sealectro Corp. 53 (I), 61 (II), 61 (III), 62 (IV), 20, 46, 48 (V) Semi-Alloys, Inc. 60 (III) Servo Corp. of America 44 (II), 65 (V) Seryonochanisms, Inc. 59 (I), 34 (II), 22 (IV) Servomechanisms, Inc. 22 (IV)
Servometer Corp. 59 (I)
Servotronics, Inc. 26 (I)
Servo-Tek Products Co. 34 (VI)
Shepherd Industries, Inc. 84 (IV), 60 Shepherd Industries, Inc. 84 (IV), 60 (V)
Sibley Co., The 37 (VI)
Sickies Div. 55 (IV)
Sierra Electronic Corp. 42 (II)
Signalite, Inc. 56 (IV)
Silipon Transistor Corp. 42 (III)
Skiatron Electronics & Television Corp. 44 (III), 66
Silip Ring Co. of America 58 (II), 56
Sioan Co. 60 (V)
Solid State Electronics Co. 58 (IV), 37 (VI)
Solid State Products Co. 52 (II)
Southwestern Industrial Electronics Co. 61 (II)
Spectracoat, Inc. 54 (VI)

61 (II)
Spectracoat, Inc. 54 (VI)
Spectra Electronics Corp. 56 (V), 58
(V), 35 (VI)
Speidel Corporation 12 (VI)
Sperry Microwave Electronics Co. 40 (VI)
Sperry Rand Corp. 35 (II), 40 (III)
Sperry Semiconductor Div. 35 (II), 40

(III)
Sprague Electric Co. 51 (I)
Sprague Engrg. Corp. 74 (IV)
Statham Dev. Corp. 77 (IV)
Stavid Engineering, Inc. 43 (I)
Sterling Precision Corp. 49 (III), 11

(VI) Stevens Mfg. Co., Inc. 60 (IV) Stoddart, Aircraft Radio Co., Inc. 58 (I), 24 (I), 35 Stoner, R. B. 36 (IV) Stratacon Cepp. 47 (V)

Stromberg-Carlson 36 (IV), 58 (V), 7 (VI) Superior Electric Co. 52 (IV)
Superior Mfg. & Instrument Corp. 52
(IV), 32 (VI)
Swift, Dr. I. H. 14 (III)
Sylvania Electric Products Inc. 59 (I),
41 (III), 13, 63 (IV)
Syntron Co. 76 (IV)
Syntron Co. 76 (IV)
Systron Corp. 52 (II), 45 (III)

T Taber Inst. Corp. 40 (III)
Tally Register Corp. 25 (I)
TA Mfg. Corp. 49 (V)
Tansitor Electronics, Inc. 52 (II)
Taylor Electronics, Inc. 52 (II)
Taylor Electronics Corp. 42 (III)
Technical Appliance Corp. 42 (III)
Technical Material Corp. 54 (III)
Telemeter Magnetics, Inc. 50 (I), 82 (IV)
Tel-Instrument Electronics Corp. 57 (IV)
Tempo Instrument Inc. 42 (III), 59 (IV), 68 (IV), 68 (IV) Tel-Instrument Electronics Corp. 57 (IV)
Tempo Instrument Inc. 42 (III), 59
(IV), 68 (IV)
Tensolite Insulated Wire Co., Inc. 46
(IV), 73 (IV)
Tensor Electric Development Co., Inc. 49
(VI)
Texas Instruments, Inc. 22 (I), 55 (II), 52 (III), 57 (III)
Texas Instruments, Inc. 52 (VI)
Texas Instruments, Inc. 52 (IV), 33, 46
(VI), 57 (III)
Thermo Electronics, Inc. 56 (III)
Their Instrument Corp. 52 (IV), 33, 46
(VI)
Their Instrument Corp. 52 (IV), 33, 46
(VI)
Thompson Industries, Inc. 13 (V)
Thermonia Corp. 66 (IV), 46 (VI)
TRAK Electronics Co. 57 (IV), 26 (V), 62 (V)
Transco Products, Inc. 43 (I), 50 (II), Transco Products, Inc. 43 (I), 50 (II), 62 (V)

Transitron Electronic Corp. 61 (III), 62, 76 (IV) 76 (IV)
Trobovich, Nicholas D. 26 (I)
Tregub, B. 6. 16 (IV)
Triad Transformer Corp. 57 (II)
Triad Transformer Corp. 78 (IV)
Tribut Equipment Corp. 78 (IV)
Tribut Laba, Inc. 69 (IV), 74 (IV), 68
(V), 38 (VI)
Trygon Electronics, Inc. 77 (IV)
Tucor, Inc. 61 (I), 48 (II)
Turbo Machine Co. 46 (III), 61 (V), 39
(VI)

U

Ultronix, Inc. 48 (III)
Union Switch & Signal Div. 55 (I),
51 (V), 45 (VI)
United Aircraft Corp. 52 (V), 54 (V)
United Electronics Co. 63 (IV)
United Transformer Corp. 41 (III), 49 (IV), 70 (IV), 58 (V)
U. S. Industries, Inc. 53 (V)
U. S. Relay Electronics 10 (II)
U. S. Sonics Corp. 60 (IV)
Universal Data Systems, Inc. 40 (III)
Universal Data Systems, Inc. 40 (III)
Universal Match Corp. 63 (I)

Valor Instruments, Inc. 58 (I), 58 (II) Varo Mfg. Co., Inc. 38 (III) Vector Electronics Co. 60 (II), 65 (V) Vector Mfg. Co., Inc. 45 (III) Vernistat Div. 61 (II), 80 (IV) Vernitron Corp. 55 (V) Vickers Inc., 48 (VI) Victoreen Inst. Co. 61 (II), 42 (III), 52 (V) Victor Electronics, Inc. 48 (III), 74 Electronics, Inc. 48 (III), 74 (IV) Victory Eng. Corp. 58 (I), 46 (II) Viking Industries, Inc. 60 (III), 50 (V) Vilms, J. 20 (I) Vincent, Jr., Britton T. 26 (II) Vitramon, Inc. 55 (II)

Wakefield Engrg., Inc. 52 (IV)
Walker, N. K. 32 (IV)
Walker, N. K. 32 (IV)
Wasserman, Reuben 38 (II)
Waterman, Reuben 38 (II)
Waterman Hydraulies Corp. 60 (I)
Waveline, Inc. 65 (IV)
Weboor, Inc. 59 (IV)
Weboor, Inc. 59 (IV)
Wells Electronics Co. 61 (IV)
Wells Industries Corp. 58 (IV)
Wells Industries Corp. 58 (IV)
Western Design Div. 53 (V)
Western Dev. Labs. 7 (V)
Westinghouse Air Brake Co. 55 (I), 51
(V), 45 (VI)
Western Dev. Labs. 7 (V)
Western Instruments Div. 56 (IV)
Wheslock Signals, Inc. 71 (IV)
White Avionics Corp. 58 (I)
William Brand-Ber Div. 30 (IV)
Wollensak Optical Co. 27 (V)
Worthington Corp. 34 (I)

Y Yardney Electric Corp. 60 (II)

RESISTORS FIXED . ADJUSTABLE PRECISION . ULTRA-PRECISION

lmmediate Deliverability: Largest Selection

PRODUCTS
Retehmeters\*: Minute,
Ultra-red Basinson BULLETIN Adjusted Resistors
Plug-Trims\* Plug-in Resistors and Socket Blocks for Divider, Decade or Instruments: .0002% Voltage Dividers .01% Wheatstone Bridges .01% Resistance Decades 000 R-50

Banana-Piugs Resisters\*: Axial, Radial, & One Sided Types, Also Jacks R.Stacks\*: Multi-Tap. 12 R-40 R-SIGERS': Multi-Tap, Fixed and Adjustable Resistors and Dividers Series "200's": Standard design Lug and Wire Lead Resistors "Patents Applied For **—13** 

For abbreviated performance data see specs below or EEM, 1960 edition, page 1263.

### GENERAL RESISTOR SPECIFICATIONS

Type: Range: Absolute accuracy: Relative accuracy: Long term stability: Temp. coefficient: Power dissipation: MIL. Specs:

**DELIVERY:** 

.01 ohms thru 20 Megohms 1% thru .005% (at 25°C) thru .001% thru .001% thru 2 ppm/°C. thru 3 watts at 125°C.

MIL-R-93A and

MIL-R-9444
(applicable sections)

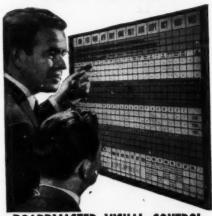
4 weeks regular, 1 week
thru 24 hours—Special

Wire-wound, also carbon and metal film.

CONSOLIDATED RESISTANCE COMPANY OF AMERICA, INC. 44 Prospect St., Yonkers, N.Y. YO 3-5900

CIRCLE 86 ON READER-SERVICE CARD

# **How To Get Things Done Better And Faster**



# BOARDMASTER VISUAL CONTROL

Gives Graphic Picture—Saves Time, Saves

Money, Prevents Errors

Simple to operate—Type or Write on Cards, Snap in Grooves

Ideal for Production, Traffic, Inventory

Scheduling, Sales, Etc.

Over 500,000 in Use Full price \$4950 with cards

FREE

24-PAGE BOOKLET No. MT-40 Without Obligation

Write for Your Copy Today **GRAPHIC SYSTEMS** Yanceyville, North Carolina CIRCLE 87 ON READER-SERVICE CARD MILITARY SYSTEMS DESIGN

60

Babcoc Bausch Beattie Boehm Breeze Bruno-Cedar Chicag Clifton Cohn ( Collins

R-44

R-28

T is

Acoust Airo S Airord Americ Autom

Colum Colvin Consol Contro Digital Dorsett DuMor Durant Dychro Dyna-E

EICO ESCO Eagle Edmun Electro Fairchi Filtors,

Graphi

Haloid Harvey Hi-G Hoffm Semi Hoke Housto Industr Industr

Kearfo Kulka Landis MM E Metho

Nation Optim

Precision Precision Prestos

Secon Servom Stanpa Sterling Stromb Sturtev

Taber Technic Thermo Thomso Times Trak Trinity Trio L. Trygon

Varian Vitrome

Zoc na

# **ADVERTISERS' INDEX**

I is index is published as a service. Every care is taken to n ke it accurate, but MSD assumes no responsibility for errors or omissions.

Airo Service Corporation   52     Airord Manufacturing Company   59     Airord Manufacturing Company   59     Airerican Measurement & Control, Inc.   30     Automatic Timing & Controls, Inc.   50     Babcock Relays, Inc.   34     Bausch & Lomb Incorporated   49     Beattle-Coleman Inc.   59     Boehme, Inc., H. O.   58     Breeze Corporations, Inc.   9     Bruno-New York Industries   50     Cedar Engineering Division of Control Data Corporation   38     Chicago Dynamic Industries, Inc.   60     Ciliton Precision Products Co., Inc.   51     Cohn Corp., Sigmund   58     Collins Corporation, G. L.   22     Columbus Electronics Corp.   13     Consolidated Resistance Company of America, Inc.   60     Conso	Acoustica Associates, Inc.	54
Alford Manufacturing Company 59 Alterican Measurement & Control, Inc. 30 Automatic Timing & Controls, Inc. 50  Babcock Relays, Inc. 34 Bausch & Lomb Incorporated 49 Beattle-Coleman Inc. 59 Boehme, Inc., H. O. 58 Breeze Corporations, Inc. 9 Bruno-New York Industries 50  Cedar Engineering Division of Control Data Corporation 38 Chicago Dynamic Industries, Inc. 60 Clifton Precision Products Co., Inc. 51 Cohn Corp., Sigmund 58 Collins Corporation, G. L. 22 Columbus Electronics Corp. 13 Colvin Laboratories, Inc. 35 Consolidated Resistance Company of America, Inc. 60 Consolidated Resistance Company of America, Inc. 60	A ro Service Corporation	52
Anerican Measurement & Confrol, Inc. 30 Automatic Timing & Controls, Inc. 50  Babcock Relays, Inc. 34 Bausch & Lomb Incorporated 49 Beattle-Coleman Inc. 59 Boehme, Inc., H. O. 58 Breeze Corporations, Inc. 9 Bruno-New York Industries 50  Cedar Engineering Division of Control Data Corporation 38 Chicago Dynamic Industries, Inc. 60 Clifton Precision Products Co., Inc. 51 Cohn Corp., Sigmund 58 Collins Corporation, G. L. 22 Columbus Electronics Corp. 13 Colvin Laboratories, Inc. 35 Consolidated Resistance Company of America, Inc. 60 Consolidated Resistance Company of America, Inc. 66		
Automatic Timing & Controls, Inc. 50  Babcock Relays, Inc. 34  Bausch & Lomb Incorporated 49  Beattie-Coleman Inc. 59  Beattie-Coleman Inc. 59  Breeze Corporations, Inc. 9  Bruno-New York Industries 50  Cedar Engineering Division of Control Data Corporation 38  Chicago Dynamic Industries, Inc. 60  Clifton Precision Products Co., Inc. 51  Cohn Corp., Sigmund 58  Collins Corporation, G. L. 22  Columbus Electronics Corp. 13  Consolidated Resistance Company of America, Inc. 60  Consolidated Resistance Company of America, Inc. 60	Apperican Measurement & Control Inc.	30
Bausch & Lomb Incorporated 49 Beattle-Coleman Inc. 59 Boehme, Inc., H. O. 58 Breeze Corporations, Inc. 9 Bruno-New York Industries 50 Cedar Engineering Division of Control Data Corporation 38 Chicago Dynamic Industries, Inc. 60 Clifton Precision Products Co., Inc. 51 Cohn Corp., Sigmund 58 Collins Corporation, G. L. 22 Columbus Electronics Corp. 13 Colvin Laboratories, Inc. 35 Consolidated Resistance Company of America, Inc. 60	Automatic Timing & Controls, Inc.	50
Beattie-Coleman Inc. 59 Boehme, Inc., H. O. 58 Breeze Corporations, Inc. 9 Bruno-New York Industries 50 Cedar Engineering Division of Control Data Corporation 38 Chicago Dynamic Industries, Inc. 60 Clifton Precision Products Co., Inc. 51 Cohn Corp., Sigmund 58 Collins Corporation, G. L. 22 Columbus Electronics Corp. 13 Colvin Laboratories, Inc. 35 Consolidated Resistance Company of America, Inc. 60		
Boehme, Inc., H. O.  Breeze Corporations, Inc.  Paruno-New York Industries  Cedar Engineering Division of Control Data Corporation  Chicago Dynamic Industries, Inc.  Colifton Precision Products Co., Inc.  Colins Corporation, G. L.  Collins Corporation, G. L.  Columbus Electronics Corp.  Colvin Laboratories, Inc.  Sover Consolidated Resistance Company of America, Inc.  60	Bausch & Lomb Incorporated	49
Breeze Corporations, Inc. 9 Bruno-New York Industries 50  Cedar Engineering Division of Control Data Corporation 38 Chicago Dynamic Industries, Inc. 60 Clifton Precision Products Co., Inc. 51 Cohn Corp., Sigmund 58 Collins Corporation, G. L. 22 Columbus Electronics Corp. 13 Colvin Laboratories, Inc. 35 Consolidated Resistance Company of America, Inc. 660	Beattie-Coleman Inc.	59
Bruno-New York Industries 50  Cedar Engineering Division of Control Data Corporation 38 Chicago Dynamic Industries, Inc. 60 Clifton Precision Products Co., Inc. 51 Cohn Corp., Sigmund 58 Collins Corporation, G. L. 22 Columbus Electronics Corp. 13 Colvin Laboratories, Inc. 35 Consolidated Resistance Company of America, Inc. 650	Boehme, Inc., H. O.	58
Bruno-New York Industries 50  Cedar Engineering Division of Control Data Corporation 38 Chicago Dynamic Industries, Inc. 60 Clifton Precision Products Co., Inc. 51 Cohn Corp., Sigmund 58 Collins Corporation, G. L. 22 Columbus Electronics Corp. 13 Colvin Laboratories, Inc. 35 Consolidated Resistance Company of America, Inc. 650	Breeze Corporations, Inc.	9
Chicago Dynamic Industries, Inc. 60 Clifton Precision Products Co., Inc. 51 Cohn Corp., Sigmund 58 Collins Corporation, G. L. 22 Columbus Electronics Corp. 13 Colvin Laboratories, Inc. 35 Consolidated Resistance Company of America, Inc. 60	Bruno-New York Industries	50
Chicago Dynamic Industries, Inc. 60 Clifton Precision Products Co., Inc. 51 Cohn Corp., Sigmund 58 Collins Corporation, G. L. 22 Columbus Electronics Corp. 13 Colvin Laboratories, Inc. 35 Consolidated Resistance Company of America, Inc. 60		
Clifton Precision Products Co., Inc. 51 Cohn Corp., Sigmund 58 Collins Corporation, G. L. 22 Columbus Electronics Corp. 13 Colvin Laboratories, Inc. 35 Consolidated Resistance Company of America, Inc. 60	Cedar Engineering Division of Control Data Corporation	38
Cohn Corp., Sigmund 58 Collins Corporation, G. L. 22 Columbus Electronics Corp. 13 Colvin Laboratories, Inc. 35 Consolidated Resistance Company of America, Inc. 650	Chicago Dynamic Industries, Inc.	60
Collins Corporation, G. L. 22 Columbus Electronics Corp. 13 Colvin Laboratories, Inc. 35 Consolidated Resistance Company of America, Inc. 60		
Columbus Electronics Corp. 13 Colvin Laboratories, Inc. 35 Consolidated Resistance Company of America, Inc. 60	Cohn Corp., Sigmund	58
Colvin Laboratories, Inc. 35 Consolidated Resistance Company of America, Inc. 60		
Consolidated Resistance Company of America, Inc. 60	Columbus Electronics Corp.	13
Consolidated Resistance Company of America, Inc. 60	Colvin Laboratories, Inc.	35
Control Products Inc	Consolidated Resistance Company of America, Inc.	60
	Control Products, Inc.	31

igital Equipment Corporation	
uMont Laboratories, Inc., Allen B	
urant Manufacturing Company	
ychro Corporation	
yna-Empire, Inc.	-6144
lynamic Gear Co. Inc.	
ICO	
SCO Eng. & Mfg. Corp.	
agle Signal	
dmund Scientific Co.	
lectronic Engineering Company of Ca	lifornia
lectrosolids Corporation	
decirosones corporation	CHARLES OF THE PERSON OF THE P

General Electric Graphic Systems	Company			60
Harvey-Wells Electric	ctronics In	c	Martin Ma	22
Hoffman Electron	nics Corpor Div.	ation,	Inside	

Industrial Electronic Engineers, Inc.	46
Industrial Sapphire Co. Instrument Development Laboratories Incorporated	35
International Telephone and Telegraph Corporation, Federal Division	
Kearfott Division, General Precision, Inc. Kulka Electric Corp.	39
Landis & Gyr, Inc.	3!
MM Enclosures, Inc.	4
Methods Research Corp.	3

Nanmac Corporation National Instrument Laboratories, Inc.	34
Nippon Electric Company Ltd	
Optimized Devices, Inc.	52
Panoramic Radio Products, Inc.	

Precision Resistor Co., Inc	
Rosemount Engineering Company	
Rosemount Engineering Company	
Scam Instrument Corn	
cam Instrument Corp.	***************************************
Secon Metals Corp	44,
econ Metals Corp. ervomechanisms, Inc.	44,
icam Instrument Corp. Secon Metals Corp. Servomechanisms, Inc. Stanpat Co. Sterling Components, Division of Sterling Precis Stromberg-Carlson, Division of General Dynam	ion Corporation

Tabor Instrument Corneration	2
Technic Inc	2
Inermo Electric Co., Inc.	
Illomson industries, inc.	3.
aber Instrument Corporation echnic Inc. hermo Electric Co., Inc. homson Industries, Inc. imes Wire & Cable Division rak Microwave Corporation rinity Equipment Corporation rio Laboratories, Inc.	2
I Irak Microwave Corporation	2
Trinity Equipment Corporation	cetric Co., Inc. (1) dustries, Inc. 33 s & Cable Division 22 wave Corporation 21 ipment Corporation 1 atories, Inc.
Trygon Electronics Inc.	

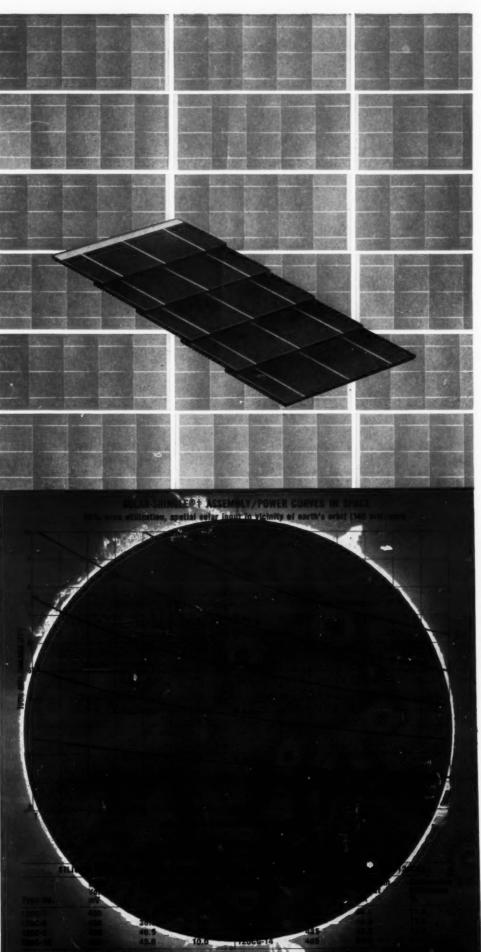
on

tory

T-40

ESIGN

Varian Associates Inside Vitromon Incorporated	Front	Cover 5
Weiham Precision Instrument Company Weiham Electronic Products Co.		.36, 39 .22
Zoc mar, Inc.		57



CIRCLE 88 ON READER-SERVICE CARD

Hoffman solar-power series.

# ONLY HOFFMAN GIVES YOU THIS MUCH DESIGN RANGE IN SILICON SOLAR-POWER ASSEMBLIES

No longer need unconventional solar-power requirements cause procurement problems. Hoffman's broad range of conversion efficiencies — widest in the industry — helps you achieve the optimum solution. Now you can specify size, shape, power output and conversion efficiency in an unprecedented number of combinations. ■ The curves at the left show you how much design flexibility is possible. To determine the minimum assembly efficiency necessary, relate the area available to the desired power output. For details, consult your Hoffman sales engineer or request Data Sheet 126-660\$.

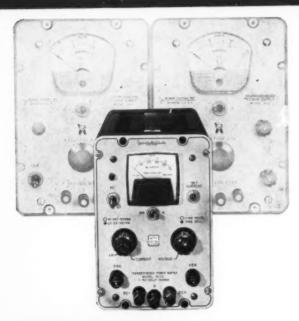
# Hoffman

ELECTRONICS CORPORATION

Semiconductor Division

1001 Arden Drive, El Monte, California TWX: El Monte 9735 Plants: El Monte, California and Evanston, Illinois





# VOLTAGE CURRENT



# FROM THE SAME TERMINALS!

The Power Designs Inc. Model 4005 Power Supply adds a new dimension to the application of d-c sources for laboratory instrumentation. Truly universal, the Model 4005 may be operated as a constant voltage source, a constant current source, a constant voltage source with automatic current limiting or a constant current source with automatic voltage limiting.

The Model 4005 employs semiconductor devices exclusively in a new proprietary circuit 

AMBITROL\* is a dual regulator system permitting continuous control of voltage or current with automatic electronic cross-over to either mode of operation.

The supply also features remote voltage programming, dual concentric controls for both coarse and fine adjustment of voltage or current and the HEATRAN® circuit for electronic control of power transistor dissipation.

MODEL 4005 SPECIFICATIONS
INPUT: 105-125 voits, 55-440 cycles single phase.
TEMPERATURE: Continuous duty at full load 0-50° C, ambient
POLARITY: Positive or negative output terminal may be grounded
DIMENSIONS: 534° W x 836° H x 1134° D.

CONSTANT VOLTAGE Range: 1-40 vdc, 0-0.5 amperes. Regulation: .05% or 10 milli-volts max, for line or load variations,

Ripple: .001% or 500 micro-volts max. Response Time: Less than 50 microseconds.

CONSTANT CURRENJ
Range: 25 to 500 milliamperes.
Voltage compliance: Output
current constant to full
rated output voltage of 40

volts.

Regulation: .05% or 250 microamperes max., for line or
load variations.

Ripple Content: .01% or 25

Source 2: 0.1 ohms to 20 kc, 0.5 ohms to 1 mc. Source impedance: 100,000 ohms annow



\$14350 F.O.B. FACTORY

†Prices subject to change without notice.



1700 SHAMES DRIVE WESTBURY, NEW YORK

EDgewood 3-6200 (Long Distance Area Code 516) CIRCLE 89 ON READER-SERVICE CARD

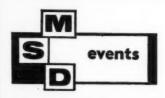


ROBOTEC HEATRAN VOLTRAN









DECEMBER 13-15-1960 Eastern Joint Computer Conference, sponsored by IRE AIEE and ACM, at the New Yorker Hotel, New York, N. Y. Write James L. Lanigan. Sylvania Electric Products Inc., 730 Third Ave., New York 17, N. Y.

INSTRUMENTS PUBLISHING
845 Ridge Avenue, Pittsburgh

Ridge

Pittsburgh

CO.,

JANUARY 8-12—1961 Symposium on Thermoelectric Energy Conversion, Statler-Hilton Hotel, Dallas, Texas. Jointly sponsored by IRE, AIEE, ANS, ARS, and others with the Department of Defense, Write Paul H. Egli, Chairman, Arrangements Committee, Naval Research Laboratory, Anacostia, D. C.

JANUARY 9-11—7th National Symposium on Reliability and Quality Control, Bellevue Stratford Hotel, Philadelphia, Pa. Sponsored by IRE, IEE, and ASQC. Write James H. Goodman, RCA, Building 1-2, Camden 2 N. I.

JANUARY 12-13—Conference on Reliability of Semiconductor Devices, Western Union Auditorium, 60 Hudson St., New York For information write Advisory Group on Electron Tubes, 346 Broadway, 8th Flr., New York 13, N. Y.

JANUARY 16-17—Symposium on Space Instrumentation scheduled to be held in Washington, D. C. has been CANCELLED

FEBRUARY 2-4-Annual ISA North Centra Area Automation Symposium, Radisson Ho tel, Minneapolis, Minn. Write Ray Hoppe Pub. Chairman Minneapplis Honeywel E. Hennepin Ave., Minneapplis Minn. FEBRUARY 14-16—Second annual

posium on Nondastructive Jesting craft and Missile Components Punclas Gunter Hotel, San Antonio, Texas. R. B. Wangler, Gen Chairman, Son Research Institute, Box 2296, San A